

TECHNICAL NOTE

D-132

A GENERAL METHOD FOR AUTOMATIC COMPUTATION OF
EQUILIBRIUM COMPOSITIONS AND THEORETICAL
ROCKET PERFORMANCE OF PROPELLANTS

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Figure 2, page 138: The second term of $\Delta \ln T$ for "Enthalpy" should be $\sum (H_T^O)_i q_i p_i$.

Figure 3, page 139: The terms in the column headings should be (a change in mathematical sign)

$$-\left(\frac{\partial \ln p_Z}{\partial \ln T}\right)_P, -\left(\frac{\partial \ln p_Y}{\partial \ln T}\right)_P, -\left(\frac{\partial \ln p_X}{\partial \ln T}\right)_P, -\left(\frac{\partial n_M}{\partial \ln T}\right)_P, -\left(\frac{\partial n_N}{\partial \ln T}\right)_P, \text{ and } +\left(\frac{\partial \ln A}{\partial \ln T}\right)_P.$$

Page 71, cards 464, 470, 471, and 474: TEMPO and 9059 should be TEM 1 and 9049, respectively.

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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SUMMARY

A general computer program for chemical equilibrium and rocket performance calculations was written for the IBM 650 computer with 2000 words of drum storage, 60 words of high-speed core storage, indexing registers, and floating point attachments. The program is capable of carrying out combustion and isentropic expansion calculations on a chemical system that may include as many as 10 different chemical elements, 30 reaction products, and 25 pressure ratios. In addition to the equilibrium composition, temperature, and pressure, the program calculates specific impulse, specific impulse in vacuum, characteristic velocity, thrust coefficient, area ratio, molecular weight, Mach number, specific heat, isentropic exponent, enthalpy, entropy, and several thermodynamic first derivatives.

INTRODUCTION

Almost the entire work involved in the calculation of theoretical performance of propellants is in the determination of the equilibrium composition and temperature of the reaction products. The difficulty in determining equilibrium compositions, especially where many reaction products are involved, is due to the fact that the necessary equations for their solution are not simultaneously linear; and hence, in general, a direct solution is not feasible.

In recent years, a number of articles have appeared in the literature dealing with equilibrium calculations for complex mixtures that describe various systematic iterative techniques for obtaining equilibrium compositions (e.g., refs. 1 to 22). With the increasing availability of high-speed digital computers, a number of programs have been prepared to solve for equilibrium compositions automatically (e.g., refs. 13, 16, and 19 to 22).

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The present report presents a completely general method programmed for the IBM 650 data processing system with 2000 words of drum storage, 60 words of high-speed core storage, index registers, floating decimal-point attachment, and alphabetic device. This program can handle any chemical system within certain limitations set by the storage capacity of the IBM 650. The program is based essentially on the method described in reference 9; however, some modifications have been made. The program was prepared during 1957 and has been in operation since January 1958.

EQUATIONS DEFINING ADIABATIC COMBUSTION

AND ISENTROPIC EXPANSION

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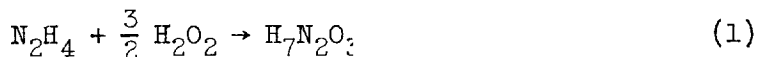
The computer program described in this report is primarily concerned with the calculation of theoretical rocket performance of chemical propellants. This calculation is simple and straightforward once the temperature and composition of the reaction products are known at combustion and exit points in the nozzle. The temperature and composition following a process such as adiabatic combustion at constant pressure or isentropic expansion to an assigned pressure can be determined from an appropriate combination of equations describing the conservation of atomic species, chemical equilibrium, Dalton's law of partial pressures, and the conservation of enthalpy or entropy. Since these equations do not constitute a set of linear equations, they must usually be solved by some iterative technique.

Combustion at Constant Pressure

For given initial conditions, the temperature and composition following a combustion process are to be found. The substances entering into the reaction may be represented by an equivalent formula

$$Z_{a_0} Y_{b_0} X_{c_0} \dots$$

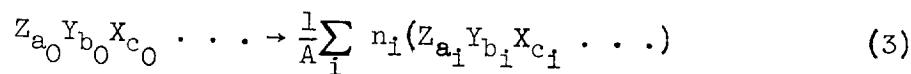
where a_0, b_0, c_0, \dots are proportional to the total number of gram atoms of the elements Z, Y, X, \dots in the reaction mixture. (A complete list of symbols is given in appendix A.) For example,



The reaction at equilibrium may be written as

$$A(Z_{a_0} Y_{b_0} X_{c_0} \dots) \rightarrow \sum_i n_i (Z_{a_i} Y_{b_i} X_{c_i} \dots) \quad (2)$$

or



where A is the number of formula weights of the equivalent reactant, and n_i is the number of moles of the i^{th} molecule or atom.

With this representation of the reaction, the equations involving mass conservation, chemical equilibria, pressure, and enthalpy may be written as follows.

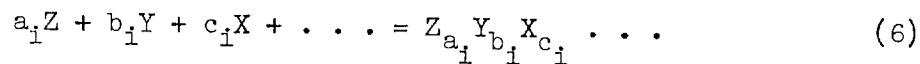
Conservation of mass. - Equations defining the relative amounts of each element in the reaction products may be written as follows:

$$\left. \begin{aligned} a &= \frac{1}{A} \sum_i a_i n_i \\ b &= \frac{1}{A} \sum_i b_i n_i \\ c &= \frac{1}{A} \sum_i c_i n_i \\ . &= \end{aligned} \right\} \quad (4)$$

where a, b, c, \dots are the number of gram atoms of substance Z, Y, X, \dots per equivalent formula required to form the reaction products. For the reaction of equation (3), conservation of mass is defined by the following relations:

$$\left. \begin{aligned} a &= a_0 \\ b &= b_0 \\ c &= c_0 \\ . . . &= . . . \end{aligned} \right\} \quad (5)$$

Chemical-equilibrium equations. - For convenience in handling the equations, each reaction product can be considered as being formed from the gaseous atoms as follows:



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The change in free energy across reaction (6), $(\Delta F)_i$, in terms of activities α is given by the relation

$$(\Delta F)_i = (\Delta F^0)_i + RT(\ln \alpha_i - a_i \ln \alpha_Z - b_i \ln \alpha_Y - c_i \ln \alpha_X - \dots) \quad (7)$$

where $(\Delta F^0)_i$ is the standard-state free-energy change across the reaction.

For gaseous reaction products, the standard state, or the state of unit activity, is usually taken to be the ideal gas at 1-atmosphere pressure. This choice of standard state makes the activity and the fugacity numerically equal. If, furthermore, all the gaseous reaction products are assumed to behave ideally, then the fugacity and partial pressure are identical. In this case, dividing by RT and using the symbol δ for $\Delta F/RT$, equation (7) may be written as

$$\delta_i = \left(\frac{\Delta F^0}{RT} \right)_i + \ln p_i - (a_i \ln p_Z + b_i \ln p_Y + c_i \ln p_X + \dots) \quad (8)$$

The criterion for equilibrium for a reaction at constant temperature and pressure is that ΔF (or δ_i) be equal to zero; that is,

$$\left(\frac{\Delta F^0}{RT} \right)_i + \ln p_i - (a_i \ln p_Z + b_i \ln p_Y + c_i \ln p_X + \dots) = 0 \quad (9)$$

In this report, a condensed phase is assumed to be a pure solid or liquid, excluding the possibility of solid or liquid solutions. The activity for a condensed phase is conventionally taken to be unity for the pure solid or liquid at 1-atmosphere pressure. At moderate pressures the activity of the condensed phase is essentially the same as in the standard state, and hence the equilibrium relation for the formation of the condensed product $Z_{a_N} Y_{b_N} X_{c_N} \dots$ from the gaseous atoms may be written as

$$\delta_N = \left(\frac{\Delta F^0}{RT} \right)_N - (a_N \ln p_Z + b_N \ln p_Y + c_N \ln p_X + \dots) \quad (10)$$

Similar expressions may be written for other condensed products, $Z_{a_M} Y_{b_M} X_{c_M} \dots$, and so forth. At equilibrium conditions $\delta_N, \delta_M, \dots$ are equal to zero; that is,

$$\left. \begin{aligned} \left(\frac{\Delta F^0}{RT} \right)_N - (a_N \ln p_Z + b_N \ln p_Y + c_N \ln p_X + \dots) &= 0 \\ \dots &= 0 \end{aligned} \right\} \quad (11)$$

Dalton's law of partial pressures. - The static pressure of the system is the sum of the partial pressures of the gaseous products:

$$P = \sum_i P_i \quad (12)$$

If a process has an assigned pressure P_0 , then

$$P = P_0 \quad (13)$$

In this report, it is assumed that the gases at combustion conditions have zero velocity; and hence, in the combustion chamber, static pressure is equal to the total pressure.

Conservation of enthalpy. - Adiabatic combustion is a constant-enthalpy process; and hence, if chemical energy is included in the enthalpy of each substance, the enthalpy of the products of reactions must equal the enthalpy of the reactants.

Since only differences in enthalpy are involved, an arbitrary base may be adopted for assigning absolute values to the enthalpy of various substances. The molar enthalpy of a substance is defined as

$$(H_T^O)_i = \int_0^T (C_P^O)_i dT + (H_O^O)_i \quad (14)$$

where $(C_P^O)_i$ is the molar specific heat at constant pressure, and $(H_O^O)_i$ is the assigned reference enthalpy at 0° K of the i^{th} substance.

If the enthalpy of the reactants per formula weight of the equivalent formula $Z_{a_0} Y_{b_0} X_{c_0} \dots$ is H_0 , then

$$H_0 = \sum_i n_{f_i} (H_T^O)_{f_i} + \sum_i n_{x_i} (H_T^O)_{x_i} \quad (15)$$

where n_{f_i} and n_{x_i} are the moles of the i^{th} fuel and i^{th} oxidant corresponding to equivalent formula $Z_{a_0} Y_{b_0} X_{c_0} \dots$, and $(H_T^O)_{f_i}$ and $(H_T^O)_{x_i}$ are the molar enthalpies of the i^{th} fuel and i^{th} oxidant, respectively.

The enthalpy of the combustion products per equivalent formula of reactants may be written as

$$H = \frac{1}{A} \sum_i (H_T^O)_i n_i \quad (16)$$

If the H_O^O values for all substances are consistently assigned (taking into account heats of reaction and transition), then for adiabatic combustion,

$$H = H_O \quad (17)$$

Isentropic Expansion to Assigned Pressure

The temperature and composition following an isentropic expansion of the combustion gases to an assigned pressure may be determined by equations for (1) conservation of atomic species, (2) chemical equilibrium, (3) the law of partial pressures, and (4) the conservation of entropy. The first three types of equations ((5), (9), (11), and (13)) have been discussed in the previous section and again apply. The fourth type is discussed herein.

The entropy of the reaction products per formula weight of the equivalent reactant is given by

$$S = \frac{1}{A} \sum_i (S_T)_i n_i \quad (18)$$

where

$$(S_T)_i = \begin{cases} (S_T^O)_i - R \ln p_i & \text{for gases} \\ (S_T^O)_i & \text{for condensed phases} \end{cases} \quad (19)$$

and $(S_T^O)_i$ is the absolute molar entropy of the i^{th} product at temperature T in the standard state.

For an isentropic expansion following a combustion process, the entropy at any point in the expansion S_e must be equal to the value of entropy at combustion conditions S_c . If S_e is considered to be an assigned value S_O , then

$$S_e = S_c = S_O \quad (20)$$

Summary of Equations for Adiabatic Combustion

and Isentropic Expansion

Equations (5), (9), (11), and (13), together with equation (17) for adiabatic combustion or equation (20) for isentropic expansion, are sufficient to solve the problem of equilibrium calculations completely. However, these equations involve both the moles n_i and the partial pressures p_i . The equations can be expressed in the same variables by letting A be that number of formula weights of equivalent reactant such that, for ideal gases,

$$p_i = n_i \quad (21)$$

This is the same as saying that the reaction takes place in a volume V numerically equal to RT . Each condensed phase is considered to occupy a negligible volume with respect to the volume occupied by the gases, even when finely divided and suspended in the gas. Condensed phases are further discussed in the subsequent section on "Condensation phenomena."

ITERATION TECHNIQUE

The two sets of equations ((5), (9), (11), (13), and (17), and (5), (9), (11), (13), and (20)) are sets of nonlinear equations, and therefore it is usually not feasible to find a direct solution. The Newton-Raphson method for solving nonlinear equations (ref. 23) is well suited to this type of calculation. In this method the finite-difference approximation to the total differential serves as a basis for the iteration procedure. This method will be illustrated by a simple example.

Let Q_1 and Q_2 be two nonlinear functions of x and y :

$$\left. \begin{aligned} Q_1 &= Q_1(x, y) = 0 \\ Q_2 &= Q_2(x, y) = 0 \end{aligned} \right\} \quad (22)$$

and let their simultaneous solution be \bar{x}, \bar{y} . For any other values of x and y , say x_i, y_i ,

$$\left. \begin{aligned} Q_1(x_i, y_i) &\neq Q_1(\bar{x}, \bar{y}) \\ Q_2(x_i, y_i) &\neq Q_2(\bar{x}, \bar{y}) \end{aligned} \right\} \quad (23)$$

or

$$\left. \begin{aligned} \Delta Q_1 &= Q_1(\bar{x}, \bar{y}) - Q_1(x_i, y_i) \\ \Delta Q_2 &= Q_2(\bar{x}, \bar{y}) - Q_2(x_i, y_i) \end{aligned} \right\} \quad (24)$$

The total differentials of (22) are

$$\left. \begin{aligned} dQ_1 &= \frac{\partial Q_1}{\partial x} dx + \frac{\partial Q_1}{\partial y} dy \\ dQ_2 &= \frac{\partial Q_2}{\partial x} dx + \frac{\partial Q_2}{\partial y} dy \end{aligned} \right\} \quad (25)$$

In finite-difference form, these become

$$\left. \begin{aligned} \Delta Q_1 &= \left(\frac{\partial Q_1}{\partial x} \right) \Delta x + \left(\frac{\partial Q_1}{\partial y} \right) \Delta y \\ \Delta Q_2 &= \left(\frac{\partial Q_2}{\partial x} \right) \Delta x + \left(\frac{\partial Q_2}{\partial y} \right) \Delta y \end{aligned} \right\} \quad (26)$$

If the difference terms ΔQ_1 and ΔQ_2 and the analytic expressions for the partial derivatives are evaluated numerically at the point x_i, y_i , the correction variables Δx and Δy can be solved for simply, since equation (26) is a simultaneous linear set of equations in the correction variables.

Because equation (26) is not exact,

$$\left. \begin{aligned} x_{i+1} &= x_i + \Delta x \neq \bar{x} \\ y_{i+1} &= y_i + \Delta y \neq \bar{y} \end{aligned} \right\} \quad (27)$$

but rather x_{i+1} and y_{i+1} will in general be a closer approximation to \bar{x} and \bar{y} than are x_i and y_i . The process of solving for corrections Δx and Δy is repeated until Δx and Δy (or ΔQ_1 and ΔQ_2) are sufficiently small.

Linear Correction Equations

Equations. - The finite-difference form of the total differential of equations (5), (9), (11), (13), (17), and (20) in terms of logarithmic correction variables is

$$\left. \begin{aligned}
 A \Delta a &= A(a_0 - a) = \sum_i a_i n_i \Delta \ln n_i - \sum_i a_i n_i \Delta \ln A \\
 A \Delta b &= A(b_0 - b) = \sum_i b_i n_i \Delta \ln n_i - \sum_i b_i n_i \Delta \ln A \\
 A \Delta c &= A(c_0 - c) = \sum_i c_i n_i \Delta \ln n_i - \sum_i c_i n_i \Delta \ln A \\
 \dots &= \dots = \dots
 \end{aligned} \right\} (28)$$

$$-\delta_i = \Delta \ln p_i - (a_i \Delta \ln p_Z + b_i \Delta \ln p_Y + c_i \Delta \ln p_X + \dots) - q_i \Delta \ln T \quad (29)$$

$$\left. \begin{aligned}
 -\delta_N &= -(a_N \Delta \ln p_Z + b_N \Delta \ln p_Y + c_N \Delta \ln p_X + \dots) - q_N \Delta \ln T \\
 \dots &= \dots
 \end{aligned} \right\} (30)$$

$$\text{where } q = \frac{\Delta H_T^0}{RT} = \frac{\partial \left(-\frac{\Delta F_T^0}{RT} \right)}{\partial \ln T};$$

$$\Delta P = (P_0 - P) = \sum_i p_i \Delta \ln p_i \quad (31)$$

$$\begin{aligned}
 A \Delta H &= A(H_0 - H) = \sum_i (H_T^0)_i n_i \Delta \ln n_i - \sum_i (H_T^0)_i n_i \Delta \ln A \\
 &\quad + T \sum_i (C_P^0)_i n_i \Delta \ln T \quad (32)
 \end{aligned}$$

$$\begin{aligned}
 A \Delta S &= A(S_0 - S) = \sum_i (S_T)_i n_i \Delta \ln n_i - \sum_i (S_T)_i n_i \Delta \ln A \\
 &\quad + \sum_i (C_P^0)_i n_i \Delta \ln T \quad (33)
 \end{aligned}$$

where

$$(S_T)_i' \begin{cases} = (S_T^O)_i - R(1 + \ln p_i) = (S_T)_i - R & \text{for gases} \\ = (S_T^O)_i & \text{for condensed phases} \end{cases} \quad (34)$$

The values for $\Delta a, \Delta b, \Delta c, \dots, (-\delta_i), (-\delta_N), \dots, \Delta P, \Delta H$, and ΔS serve to indicate the error still left in the system of equations with the estimates n_i, A , and T .

Relation between δ_i and q_i . - For purposes of machine computation, it was found more convenient to write equations (8) and (10) in a different form. The relation

$$\left(\frac{\Delta F_T^O}{RT}\right)_i = \left(\frac{\Delta H_T^O}{RT}\right)_i - \left(\frac{\Delta S_T^O}{R}\right)_i = q_i - \left(\frac{\Delta S_T^O}{R}\right)_i \quad (35)$$

is used to eliminate $(\Delta F_T^O/RT)_i$ in equations (8) and (10), which become

$$\delta_i = q_i - \left[\left(\frac{S_T^O}{R}\right)_i - \ln p_i \right] + a_i \left[\left(\frac{S_T^O}{R}\right)_Z - \ln p_Z \right] + b_i \left[\left(\frac{S_T^O}{R}\right)_Y - \ln p_Y \right] + c_i \left[\left(\frac{S_T^O}{R}\right)_X - \ln p_X \right] + \dots \quad (36)$$

$$\delta_N = q_N - \left[\left(\frac{S_T^O}{R}\right)_N \right] + a_N \left[\left(\frac{S_T^O}{R}\right)_Z - \ln p_Z \right] + b_N \left[\left(\frac{S_T^O}{R}\right)_Y - \ln p_Y \right] + c_N \left[\left(\frac{S_T^O}{R}\right)_X - \ln p_X \right] + \dots \quad (37)$$

Matrix Representation of Correction Equations

Matrix. - The augmented matrix for the combustion problem (eqs. (28) to (32)) is given in figure 1. The augmented matrix for the expansion problem is identical to that for combustion, except that equation (32) is replaced by equation (33), as indicated in the footnote in figure 1. A direct elimination of the correction variables pertaining to the gaseous molecules gives a new matrix whose order is equal to the sum of the different chemical elements and condensed phases plus 2. This reduced matrix is presented as figure 2, where the correction variables for the condensed phases are linear rather than logarithmic to permit a greater symmetry in the coefficient matrix.

In figure 2 and elsewhere in this report, the symbol p_i is used in summations that include only gaseous reaction products, whereas the symbol n_i is used in summations that include condensed as well as gaseous reaction products.

Condensation phenomena. - In this report, a molecular species which appears in a condensed phase is considered to be independent of the same species in the gaseous phase. The vapor pressure is assigned completely to the gas phase, and a zero vapor pressure is assigned to the condensed phase. Two separate equilibrium equations (eqs. (8) and (10)) are written for this species, one for the gaseous phase and one for the condensed. The vapor-condensed-phase equilibrium is implicit in these two equations.

The present program is capable of considering several situations when the chemical system is such that condensed reaction products are possible. In the first situation, a condensed product is assumed to be present. After the equilibrium compositions have been determined, the assumption is checked. If correct, the program continues; if incorrect (a negative value for the amount of the condensed product), the program automatically restarts the calculations with this condensed phase excluded. In a second situation, a condensed phase is assumed to be not present. After equilibrium compositions have been determined, if the assumption is correct the program continues. If the assumption is incorrect (the partial pressure of the condensable gas exceeds the vapor pressure), the program automatically restarts the calculations with the condensed phase included.

The criterion for condensation is easily obtained from the equilibrium constant. Thus, for the reaction

$$(Z_{a_1} Y_{b_1} X_{c_1} \dots)_g = (Z_{a_N} Y_{b_N} X_{c_N} \dots)_c \quad (38)$$

where $a_1 = a_N$, $b_1 = b_N$, $c_1 = c_N \dots$, the equilibrium constant is

$$K = \frac{K_N}{K_1} = \frac{1}{p_{\text{vap}}} = e^{-\left[\frac{(F_T^0)_c - (F_T^0)_g}{RT} \right]} \quad (39)$$

Condensation occurs when

$$p_i \geq p_{\text{vap}} = \frac{1}{K}$$

or

$$p_i K \geq 1$$

which can be written as

$$\frac{(F_T^O)_c - (F_T^O)_g}{RT} - \ln p_i \leq 0 \quad (40)$$

THERMODYNAMIC FIRST PARTIAL DERIVATIVES

From the many thermodynamic first partial derivatives, it is possible arbitrarily to select three independent derivatives and then to express all the other possible thermodynamic first partial derivatives in terms of these three. The three thermodynamic derivatives selected for calculation in this report are $(\partial H/\partial T)_P$, $(\partial \ln \mathcal{M}/\partial \ln T)_P$, and $(\partial \ln \mathcal{M}/\partial \ln P)_T$, where \mathcal{M} is the molecular weight of the reaction products as defined in equation (45).

Heat Capacity at Constant Pressure

The enthalpy of the products of reaction per equivalent formula of reactant is given by (16). Since the heat capacity per equivalent formula of reactant is $(\partial H/\partial T)_P$, then the heat capacity of the reaction products per mole of reaction product is

$$\frac{A}{n} \left(\frac{\partial H}{\partial T} \right)_P = C_P^O \quad (41)$$

where

$$n = \sum_i n_i$$

Differentiation of equation (16) gives an expression for $(\partial H/\partial T)_P$ that may be used to obtain C_P^O in equation (41):

$$\begin{aligned} \left(\frac{\partial H}{\partial T} \right)_P = \frac{1}{AT} \left[\sum_i (H_T^O)_i p_i \left(\frac{\partial \ln p_i}{\partial \ln T} \right)_P + (H_T^O)_N \left(\frac{\partial n_N}{\partial \ln T} \right)_P + (H_T^O)_M \left(\frac{\partial n_M}{\partial \ln T} \right)_P + \right. \\ \left. \dots + T \sum_i (C_P^O)_i n_i - \sum_i (H_T^O)_i n_i \left(\frac{\partial \ln A}{\partial \ln T} \right)_P \right] \quad (42) \end{aligned}$$

Equation (42) may be written in another form that was found more convenient with the calculation method of this report. Differentiation of (9) gives the identity

$$\left(\frac{\partial \ln p_i}{\partial \ln T}\right)_P = a_i \left(\frac{\partial \ln p_Z}{\partial \ln T}\right)_P + b_i \left(\frac{\partial \ln p_Y}{\partial \ln T}\right)_P + \dots + q_i \quad (43)$$

Combining equations (41), (42), and (43) gives the following expression for C_P^O :

$$\begin{aligned} C_P^O = \frac{1}{nT} & \left[\sum_i (H_T^O)_i a_i p_i \left(\frac{\partial \ln p_Z}{\partial \ln T}\right)_P + \sum_i (H_T^O)_i b_i p_i \left(\frac{\partial \ln p_Y}{\partial \ln T}\right)_P + \dots \right. \\ & + (H_T^O)_N \left(\frac{\partial n_N}{\partial \ln T}\right)_P + (H_T^O)_M \left(\frac{\partial n_M}{\partial \ln T}\right)_P + \dots - \sum_i (H_T^O)_i n_i \left(\frac{\partial \ln A}{\partial \ln T}\right)_P \\ & \left. + T \sum_i (C_P^O)_i n_i + (H_T^O)_i q_i p_i \right] \quad (44) \end{aligned}$$

A comparison of equation (44) with the last row in figure 2 shows that the coefficients of the derivatives are the elements of the enthalpy row. The solution of the partials $(\partial \ln p_Z / \partial \ln T)_P$, $(\partial \ln p_Y / \partial \ln T)_P$, \dots , is discussed in the section on "Derivative Matrices."

Molecular-Weight Derivatives

Each condensed phase is considered to occupy a negligible volume with respect to the volume occupied by the gases, even when finely divided and suspended in the gas. An average molecular weight is then defined to be the weight of the reaction products divided by the number of moles of gaseous products:

$$\mathcal{M} = \frac{\sum_i n_i \mathcal{M}_i}{\sum_i p_i} = \frac{A \mathcal{M}_r}{P} \quad (45)$$

where \mathcal{M}_r is the formula weight of the equivalent formula of equation (3). When only gaseous products are formed in the reaction, this definition is identical to the usual definition of an average molecular weight. With the definition of equation (45), the molecular weight is suitable for use in the ideal gas law even when solids are present:

$$\left. \begin{aligned} P &= \frac{\rho RT}{\mathcal{M}} \\ \text{or} \\ P v &= \frac{RT}{\mathcal{M}} \end{aligned} \right\} \quad (46)$$

The density ρ or specific volume v in equation (46) is the average value of the mixture of gases and condensed phases. Taking logarithms of equation (45),

$$\ln \mathcal{M} = \ln A + \ln \mathcal{M}_r - \ln P \quad (47)$$

Differentiation of equation (47) with respect to $\ln T$ at constant P gives

$$\left(\frac{\partial \ln \mathcal{M}}{\partial \ln T} \right)_P = \left(\frac{\partial \ln A}{\partial \ln T} \right)_P \quad (48)$$

Differentiation of equation (47) with respect to $\ln P$ at constant T gives

$$\left(\frac{\partial \ln \mathcal{M}}{\partial \ln P} \right)_T = \left(\frac{\partial \ln A}{\partial \ln P} \right)_T - 1 \quad (49)$$

Differentiation of equation (12) with respect to $\ln A$ at constant T gives

$$\left(\frac{\partial \ln P}{\partial \ln A} \right)_T = \frac{1}{\left(\frac{\partial \ln A}{\partial \ln P} \right)_T} = \frac{1}{P} \sum_i P_i \left(\frac{\partial \ln p_i}{\partial \ln A} \right)_T \quad (50)$$

which may be used in equation (49) to give

$$\left(\frac{\partial \ln \mathcal{M}}{\partial \ln P} \right)_T = \left[\frac{P}{\sum_i P_i \left(\frac{\partial \ln p_i}{\partial \ln A} \right)_T} - 1 \right] \quad (51)$$

Differentiation of equation (9) gives

$$\left(\frac{\partial \ln p_i}{\partial \ln A} \right)_T = a_i \left(\frac{\partial \ln p_Z}{\partial \ln A} \right)_T = b_i \left(\frac{\partial \ln p_Y}{\partial \ln A} \right)_T + \dots \quad (52)$$

Equations (51) and (52) may be combined to give

$$\left(\frac{\partial \ln \mathcal{M}}{\partial \ln P} \right)_T = \left[\frac{P}{\sum_i a_i P_i \left(\frac{\partial \ln p_Z}{\partial \ln A} \right)_T + \sum_i b_i P_i \left(\frac{\partial \ln p_Y}{\partial \ln A} \right)_T + \dots} - 1 \right] \quad (53)$$

Comparison of equation (53) and the pressure row in figure 2 shows that the coefficients of the derivatives in equation (53) are the elements of the pressure row.

Other First Partial Derivatives (γ and C_V^O)

Bridgman (ref. 24) presents a convenient scheme for expressing all first partial derivatives in terms of three first partial derivatives, one of which is the same as selected in this report, $(\partial H/\partial T)_P = C_P^O$, and two of which are different, $(\partial v/\partial T)_P$ and $(\partial v/\partial P)_T$. In order to make use of the tables of reference 24, $(\partial v/\partial T)_P$ and $(\partial v/\partial P)_T$ can be obtained from the derivatives given in this report by means of the following equations, which have been derived from the equation of state for ideal gases with variable molecular weight (eq. (46)):

$$\left(\frac{\partial v}{\partial T}\right)_P = \frac{v}{T} \left[1 - \left(\frac{\partial \ln \mathcal{M}}{\partial \ln T}\right)_P \right] \quad (54)$$

$$\left(\frac{\partial v}{\partial P}\right)_T = -\frac{v}{P} \left[1 + \left(\frac{\partial \ln \mathcal{M}}{\partial \ln P}\right)_T \right] \quad (55)$$

With the aid of the tables in reference 24 and equations (46), (54), and (55), other first partial derivatives can be expressed in terms of C_P^O , $(\partial \ln \mathcal{M}/\partial \ln T)_P$, and $(\partial \ln \mathcal{M}/\partial \ln P)_T$. As examples, expressions are derived for the isentropic exponent γ , which is used to calculate velocity of sound, and specific heat at constant volume C_V^O .

By definition,

$$\gamma = \left(\frac{\partial \ln P}{\partial \ln \rho}\right)_s = -\left(\frac{\partial \ln P}{\partial \ln v}\right)_s = -\frac{v}{P} \left(\frac{\partial P}{\partial v}\right)_s \quad (56)$$

From Bridgman's tables (ref. 24),

$$\left(\frac{\partial P}{\partial v}\right)_s = \frac{C_P^O/\mathcal{M}}{\left(\frac{C_P^O}{\mathcal{M}}\right)\left(\frac{\partial v}{\partial P}\right)_T + T\left(\frac{\partial v}{\partial T}\right)_P^2} \quad (57)$$

Substituting equations (46), (54), (55), and (57) into equation (56) yields

$$\gamma = \frac{C_P^O/R}{\frac{C_P^O}{R} \left[1 + \left(\frac{\partial \ln \mathcal{M}}{\partial \ln P}\right)_T \right] - \left[1 - \left(\frac{\partial \ln \mathcal{M}}{\partial \ln T}\right)_P \right]^2} \quad (58)$$

For nonreacting gases ("frozen" composition), \mathcal{M} is a constant, and equation (58) reduces to

$$\gamma = \frac{C_P^0/R}{\frac{C_P^0}{R} - 1} \quad (59)$$

By definition and from Bridgman's tables (ref. 24),

$$\frac{C_V^0}{\mathcal{M}} = \frac{1}{\mathcal{M}} \left(\frac{\partial E}{\partial T} \right)_V = \frac{\left(\frac{C_P^0}{\mathcal{M}} \right) \left(\frac{\partial v}{\partial P} \right)_T + T \left(\frac{\partial v}{\partial T} \right)_P^2}{\left(\frac{\partial v}{\partial P} \right)_T} \quad (60)$$

Substituting equations (46), (54), and (55) into equation (60) gives

$$C_V^0 = C_P^0 - R \frac{\left[1 - \left(\frac{\partial \ln \mathcal{M}}{\partial \ln T} \right)_P \right]^2}{\left[1 + \left(\frac{\partial \ln \mathcal{M}}{\partial \ln P} \right)_T \right]} \quad (61)$$

For nonreacting gases, \mathcal{M} is constant, and equation (61) reduces to

$$C_V^0 = C_P^0 - R \quad (62)$$

Derivative Matrices

The evaluation of the three independent thermodynamic first partial derivatives is possible if the quantities $(\partial \ln p_Z / \partial \ln T)_P$, $(\partial \ln p_Y / \partial \ln T)_P \dots (\partial n_N / \partial \ln T)_P \dots (\partial \ln A / \partial \ln T)_P$ and $(\partial \ln p_Z / \partial \ln A)_T$, $(\partial \ln p_Y / \partial \ln A)_T, \dots$ are known. These quantities may be calculated for equilibrium conditions by the solution of a set of simultaneous equations involving the preceding derivatives. The necessary equations for the temperature derivatives may be obtained from equations (5), (9), (11), and (13). Differentiation of these equations with respect to $\ln T$ at constant P gives

$$\left. \begin{aligned} \sum_i a_i p_i \left(\frac{\partial \ln p_i}{\partial \ln T} \right)_P + a_N \left(\frac{\partial n_N}{\partial \ln T} \right)_P + \dots - \sum_i a_i n_i \left(\frac{\partial \ln A}{\partial \ln T} \right)_P &= 0 \\ \sum_i b_i p_i \left(\frac{\partial \ln p_i}{\partial \ln T} \right)_P + b_N \left(\frac{\partial n_N}{\partial \ln T} \right)_P + \dots - \sum_i b_i n_i \left(\frac{\partial \ln A}{\partial \ln T} \right)_P &= 0 \\ \dots \dots \dots \dots \dots \dots \dots \dots \dots \dots \dots \dots \dots &= 0 \end{aligned} \right\} \quad (63)$$

$$\left(\frac{\partial \ln p_i}{\partial \ln T}\right)_P - \left[a_i \left(\frac{\partial \ln p_Z}{\partial \ln T}\right)_P + b_i \left(\frac{\partial \ln p_Y}{\partial \ln T}\right)_P + \dots \right] - q_i = 0 \quad (64)$$

$$\left. \begin{aligned} a_N \left(\frac{\partial \ln p_Z}{\partial \ln T}\right)_P + b_N \left(\frac{\partial \ln p_Y}{\partial \ln T}\right)_P + \dots + q_N &= 0 \\ \dots &= 0 \end{aligned} \right\} \quad (65)$$

$$\sum_i p_i \left(\frac{\partial \ln p_i}{\partial \ln T}\right)_P = 0 \quad (66)$$

If equation (64) is used to eliminate $(\partial \ln p_i / \partial \ln T)_P$ from equations (63) and (66), then the resulting augmented matrix is identical to the matrix of figure 2 with the last row and column deleted, as shown in figure 3.

The derivatives with respect to $\ln A$ at constant T are obtained in a similar fashion. Differentiation of equations (5), (9), and (11) yields:

$$\left. \begin{aligned} \sum_i a_i p_i \left(\frac{\partial \ln p_i}{\partial \ln A}\right)_T + a_N \left(\frac{\partial n_N}{\partial \ln A}\right)_T + \dots - \sum_i a_i n_i &= 0 \\ \sum_i b_i p_i \left(\frac{\partial \ln p_i}{\partial \ln A}\right)_T + b_N \left(\frac{\partial n_N}{\partial \ln A}\right)_T + \dots - \sum_i b_i n_i &= 0 \\ \dots &= 0 \end{aligned} \right\} \quad (67)$$

$$\left(\frac{\partial \ln p_i}{\partial \ln A}\right)_T - \left[a_i \left(\frac{\partial \ln p_Z}{\partial \ln A}\right)_T + b_i \left(\frac{\partial \ln p_Y}{\partial \ln A}\right)_T + \dots \right] = 0 \quad (68)$$

$$\left. \begin{aligned} a_N \left(\frac{\partial \ln p_Z}{\partial \ln A}\right)_T + b_N \left(\frac{\partial \ln p_Y}{\partial \ln A}\right)_T + \dots &= 0 \\ \dots &= 0 \end{aligned} \right\} \quad (69)$$

If equation (68) is used to eliminate $(\partial \ln p_i / \partial \ln A)_T$ from equation (67), then the resulting augmented matrix is identical to the matrix of figure 2 with the last two rows and columns deleted, as shown in figure 4.

ROCKET PERFORMANCE PARAMETERS

Calculation

The evaluation of rocket performance parameters for a propellant is simple once the temperature and composition are known at combustion and exit points of a nozzle. The following formulas used in computing the various performance parameters were derived from the one-dimensional forms of continuity, energy, and momentum equations and the following assumptions: zero velocity in the combustion chamber, perfect gas law, complete combustion, homogeneous mixing, adiabatic combustion, and isentropic expansion. (The units used were $h = \text{cal/g}$, $T = ^\circ\text{K}$, $P = \text{lb force/sq in.}$, $A = \text{sq in.}$, $w = \text{lb mass/sec}$, and $g_c = 32.174 (\text{lb mass/lb force})(\text{ft/sec}^2)$.)

Specific impulse with ambient and exit pressures equal, $(\text{lb force})(\text{sec})/\text{lb mass}$:

$$I = 294.98 \sqrt{\frac{h_c - h}{1000}} \quad (70)$$

Specific impulse in vacuum (ambient pressure zero), $(\text{lb force})(\text{sec})/\text{lb mass}$:

$$I_{\text{vac}} = I + P \left(\frac{A}{w} \right) \quad (71)$$

Nozzle area per unit mass-flow rate, $(\text{sq in.})(\text{sec})/\text{lb}$:

$$\frac{A}{w} = \frac{86.4554 T}{P M I} \quad (72)$$

Characteristic velocity, ft/sec :

$$c^* = g_c P_c \frac{A_t}{w} = 32.174 P_c \frac{A_t}{w} \quad (73)$$

Coefficient of thrust:

$$C_F = \frac{g_c I}{c^*} = 32.174 \frac{I}{c^*} \quad (74)$$

Mach number:

$$M = \frac{U}{a} = \frac{I}{\sqrt{86.4554 \gamma T}} \quad (75)$$

Effect of Chamber Pressure on Performance Parameters

For a given pressure ratio P_c/P , the logarithms of the performance parameters given in equations (70) to (74) are very nearly linear in the logarithm of the combustion-chamber pressure P_c . Thus, if any one of the performance parameters is denoted by λ , then, to a good approximation,

$$\left(\frac{\partial \ln \lambda}{\partial \ln P_c} \right)_{P_c/P} = \pi_\lambda \cong \frac{\ln \lambda_2 - \ln \lambda_1}{\ln (P_c)_2 - \ln (P_c)_1} \quad (76)$$

or

$$\frac{\lambda_2}{\lambda_1} \cong \left[\frac{(P_c)_2}{(P_c)_1} \right]^{\pi_\lambda} \quad (77)$$

Analytical expressions are readily obtained for the partial derivatives π_λ by the method indicated in reference 25. Using this technique it is possible to derive the following identities:

$$\pi_I = \frac{RT}{I^2} \left[\frac{1}{\mathcal{M}_c} - \frac{1}{\mathcal{M}} \right] \quad (78)$$

$$\pi_{A/w} = - \left\{ \frac{R}{C_P^0 \frac{\mathcal{M}_c}{\mathcal{M}}} \left[1 - \left(\frac{\partial \ln \mathcal{M}}{\partial \ln T} \right)_P \right] + \frac{1}{\gamma} + \pi_I \right\} \quad (79)$$

$$\pi_\epsilon = \pi_{A/w} - (\pi_{A/w})_t \quad (80)$$

$$\pi_{c*} = 1 + (\pi_{A/w})_t \quad (81)$$

$$\pi_T = \frac{R}{C_P^0} \left[1 - \left(\frac{\partial \ln \mathcal{M}}{\partial \ln T} \right)_P \right] - \frac{R}{C_P^0 \left(\frac{\mathcal{M}_c}{\mathcal{M}} \right)} \quad (82)$$

$$\pi_{C_F} = \pi_I - \pi_{c*} \quad (83)$$

$$\pi_{I_{vac}} = \frac{I(\pi_I) + (I_{vac} - I)(\pi_\epsilon + \pi_{c*})}{I_{vac}} \quad (84)$$

ITERATION TO AN ASSIGNED MACH NUMBER

It may sometimes be desired to calculate conditions following an isentropic expansion to an assigned Mach number rather than to an assigned pressure. For example, one might wish to find the conditions at the throat of a nozzle where the Mach number is 1. The procedure used in this report for calculating conditions at an assigned Mach number is as follows:

(1) An estimate of pressure corresponding to the assigned Mach number is made.

(2) After equilibrium composition and temperature have been obtained in a manner identical to isentropic expansion to assigned pressure, the Mach number is then calculated.

(3) The error between the desired Mach number and the calculated Mach number is used to obtain a new estimate for pressure.

(4) Steps (2) and (3) are repeated until the desired degree of accuracy is obtained.

The correction to the assumed pressure ratio can be obtained by using a parameter h^* , defined as

$$h^* = h + \frac{M_0^2}{2} \frac{\gamma R T}{\mathcal{M}} \quad (85)$$

where h , γ , T , and \mathcal{M} are values corresponding to the assumed pressure, and M_0 is the assigned Mach number. When the correct pressure (or pressure ratio) is used, h^* will equal the initial enthalpy of the propellants h_c . The estimate for the pressure ratio is corrected on the basis of the difference between h^* and h_c . Since h^* is a function of P ,

$$\Delta h^* = \left(\frac{\partial h^*}{\partial \ln P} \right)_s \Delta \ln P \quad (86)$$

where

$$\Delta h^* = h_c - h_k^*$$

and

$$\Delta \ln P = \frac{P_{k+1} - P_k}{P_k}$$

with the subscript k referring to the k^{th} estimate. Equation (86) then gives

$$\frac{P_c}{P_{k+1}} = \frac{P_c/P_k}{\left[1 + \frac{h_c - h_k^*}{\left(\frac{\partial h^*}{\partial \ln P} \right)_s} \right]} \quad (87)$$

The $(k+1)^{\text{th}}$ estimate can be obtained from the k^{th} estimate for the pressure ratio by means of equation (87), provided that $(\partial h^*/\partial \ln P)_s$ can be evaluated. Since γ is essentially constant for a small change in pressure ratio, then from equation (85),

$$\left(\frac{\partial h^*}{\partial \ln P} \right)_s \cong P \left\{ \left(\frac{\partial h}{\partial P} \right)_s + \frac{\gamma R M_0^2}{2} \left[\frac{\partial (T/\mathcal{M})}{\partial P} \right]_s \right\} \quad (88)$$

From equation (46) for an ideal gas,

$$\left[\frac{\partial (T/\mathcal{M})}{\partial P} \right]_s = \frac{1}{R\rho} \left[1 - \left(\frac{\partial \ln \rho}{\partial \ln P} \right)_s \right] = \frac{1}{R\rho} \left(\frac{\gamma - 1}{\gamma} \right) \quad (89)$$

Using the thermodynamic relation $(\partial h/\partial P)_s = 1/\rho$ and equation (89) in equation (88) yields

$$\left(\frac{\partial h^*}{\partial \ln P} \right)_s \cong \frac{RT}{\mathcal{M}} \left[1 + \frac{M_0^2}{2} (\gamma - 1) \right] \quad (90)$$

In particular, at the throat $M_0 = 1$ and equation (90) becomes

$$\left(\frac{\partial h^*}{\partial \ln P} \right)_s \cong \frac{RT}{2\mathcal{M}} (\gamma + 1) \quad (91)$$

COMPUTER PROGRAM

A computer program for performing the calculations previously discussed has been made for an IBM 650 Magnetic Drum Data-Processing Machine with 2000 words of drum storage, 60 words of high-speed core storage, indexing registers, floating point attachments, and an alphabetic device. When additional attachments such as tapes and RAMAC are available, the program may be modified to make use of these attachments. A wiring diagram for the IBM type 533 Read-Punch Unit is given in appendix I. In the description of the program, a familiarity with the symbolic coding for the IBM 650 computer (SOAP II) is assumed, as described in IBM Form 32-7646-1, "Soap Programmer's Reference Manual." References to storage

locations will be made with symbolic addresses given in upper case and enclosed by quotes. For the absolute equivalents of the symbolic addresses, the program listing given in appendixes F, G, and H can be consulted.

Because of computer storage limitations, it was necessary to divide the program into two sections, (1) The "Vector and Propellant Program," which prepares most of the input data and requires an alphabetic device on the IBM 650, and (2) The "Main Calculating Program," which solves for the equilibrium compositions and temperatures and the performance parameters. The Main Calculating Program may be used without using the Vector and Propellant Program if the necessary input data are prepared manually. The primary use of the Vector and Propellant Program is to simplify the preparation of input data and to minimize the possibility of errors. However, since the use of the Vector and Propellant Program is optional, the Main Calculating Program will be described first.

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MAIN CALCULATING PROGRAM

General Description

Figure 5 gives a schematic outline of the Main Calculating Program. Individual portions of the program will be discussed in more detail in later sections. A SOAP listing of the Main Program is given in appendix F, and operating instructions are given in appendix C.

The program as written is capable of performing thermodynamic equilibrium calculations for both combustion and isentropic expansion conditions for a chemical system that may include as many as 10 different chemical elements (if no condensed phases appear as reaction products). When condensed phases are present as reaction products, then the sum of the different chemical elements and different condensed phases must not exceed 10. This restriction implies that the size of the reduced augmented matrix (fig. 2) is limited to 12×13 . It should be emphasized that this restriction is imposed solely by machine storage limitations.

The program will handle as many as 30 reaction products and 25 pressure ratios including the combustion chamber and the throat. The restriction on the number of products and pressure ratios is also the result of storage limitations. The program calculates the equilibrium composition, temperature, pressure, enthalpy, and entropy of the reaction products, and the following performance parameters: specific impulse, specific impulse in vacuum, thrust coefficient, characteristic velocity, area ratio, specific heat, isentropic exponent γ , and Mach number. The program also calculates the derivatives $\left(\frac{\partial \ln \mathcal{M}}{\partial \ln P}\right)_P$, $\left(\frac{\partial \ln \mathcal{M}}{\partial \ln P}\right)_T$, and the chamber-pressure derivatives π_I , π_c , π_T , and π_{c*} .

Normally the program calculates combustion conditions ($P_c/P = 1$), then throat conditions, and finally other exit conditions corresponding to assigned pressure ratios. The program is easily modified to operate for assigned temperatures and pressures or to work a series of constant-enthalpy calculations at various pressures. The necessary changes in the program are given in the section "Program Modifications."

The following input data are required by the Main Calculating Program for the solution of equilibrium compositions and temperature following an adiabatic combustion process:

- (1) The reaction products to be considered
- (2) Gram atoms of elements in 1 gram of fuel and 1 gram of oxidant
- (3) Enthalpies of fuel and oxidant per gram of fuel and oxidant
- (4) Oxidant to fuel weight ratio O/F (or percent fuel or equivalence ratio r)
- (5) Thermodynamic data for products considered
- (6) Chamber pressure
- (7) Initial estimate of temperature, composition, and number of formula weights A . (A set of estimates is already provided by the program and therefore need not be supplied unless a better set is desired.)

Reaction products (the composition vector). - The composition of any product of reaction in terms of the elements may be represented as a chemical vector whose components are determined by the chemical formula for the reaction product. Thus, the molecule $Z_{a_i}Y_{b_i}X_{c_i} \dots$ may be associated with the vector

$$C = \{a_i, b_i, c_i \dots\}$$

The number of components associated with each composition vector is known once it is decided how many chemical elements are to be considered in any particular problem. For example, if hydrogen and oxygen were the only two elements appearing, then any reaction product could be specified with two components. If hydrogen, oxygen, and nitrogen were the elements under consideration, then each reaction product would have three components. This is illustrated in the following table for four possible products of reaction involving hydrogen, oxygen, and nitrogen:

Product	Component		
	H	N	O
N	0	1	0
OH	1	0	1
H ₂ O	2	0	1
NO	0	1	1

A considerable portion of the matrix of figure 2 may be constructed in a reasonably systematic manner with the aid of the composition vector. This is described in the section "Vector multiplication routine."

Packed chemical vector. - The total number of components of all the chemical vectors is directly related to the size of the chemical system and to the number of possible reaction products. Thus, for a 10-element system in which 30 different products of reaction are to be considered, a total of 300 components requiring 300 storage locations would have to be specified. Since these numbers would be placed in the storage area of a computer with limited storage capacity, the storage area available for programming would be seriously reduced. It has been found that with a few suitable restrictions all the components of a vector may be packed into one 10-digit word, and thus only 30 storages would be required for 30 products. The following restrictions have been set forth:

- (1) All the chemical vector components that are not specified are assumed to be zero.
- (2) No reaction product may be formed from more than five different chemical elements; that is, the chemical vector may have no more than five nonzero components.
- (3) Each subscript in the chemical formula for the reaction product must be less than 10; that is, no vector component may be greater than 9.

The packed chemical vector may now be generated from the chemical formula of a reaction product in the following manner:

- (1) Each element in the chemical system is assigned a number equal to one less than its column assignment in the reduced augmented matrix (fig. 2). This number is used to specify the component.
- (2) The magnitude of any component is equal to the subscript associated with the chemical element in the chemical formula for the reaction product under consideration.
- (3) The packed vector consists of five pairs of numbers. In each pair of numbers (where both numbers are not zero) the number designating the component precedes the number that gives the magnitude of the component.

(4) The nonzero vector components and their associated magnitudes are arranged in the packed vector in the order of their appearance in the chemical formula of the reaction product, the entire packed vector being shifted as far to the right as possible.

(5) The sign of the packed composition vector is positive for a gaseous reaction product and negative for a condensed-phase reaction product.

An example of how components might be designated in an H-N-O system is as follows:

Element	H	N	O
Column of matrix in fig. 2	1	2	3
Number designating component (column number - 1)	0	1	2

The assignment of numbers designating the elements is completely arbitrary. However, once an assignment has been made for some problem, then all product vectors must be consistent with this assignment.

Examples of packed vectors for four reaction products using the numbers designating components given in the previous table are as follows:

Reaction product	Packed vector
N	00 00 00 00 11+
OH	00 00 00 21 01+
H ₂ O	00 00 00 02 21+
NO	00 00 00 11 21+

To read the preceding packed vectors, proceed as follows:

- (1) Pair the digits into groups of two.
- (2) The first digit of a pair designates the atom.
- (3) The second digit of the pair tells how many of these atoms there are.

the fuel ($O/F = W_X/W_F$), then the number of gram atoms of each element in 1 gram of equivalent reactant $Z_{a_O} Y_{b_O} X_{c_O} \dots$ is

$$\left. \begin{aligned} a_O &= \frac{W_X a_X + W_F a_F}{W_X + W_F} = \frac{(O/F) a_X + a_F}{(O/F) + 1} \\ b_O &= \frac{W_X b_X + W_F b_F}{W_X + W_F} = \frac{(O/F) b_X + b_F}{(O/F) + 1} \\ \dots &= \dots = \dots \end{aligned} \right\} \quad (92)$$

Equation (92) may be illustrated by considering the example of equation (1):



The formulas per gram of equivalent fuel and oxidant are

$$\left. \begin{aligned} N(2/32.048) \quad H(4/32.048) &= N_{0.062406390} \quad H_{0.12481278} \\ H(2/34.016) \quad O(2/34.016) &= H_{0.058795860} \quad O_{0.058795860} \end{aligned} \right\} \quad (93)$$

(Eight significant figures are kept in this example, since the IBM 650 floating point attachment keeps eight significant figures.) For equation (1),

$$O/F = \frac{1.5(34.016)}{32.048} = 1.5921118 \quad (94)$$

and therefore

$$\left. \begin{aligned} (H) \quad a_O &= \frac{1.5921118(0.058795860) + 0.12481278}{1.5921118 + 1} = 0.084264252 \\ (N) \quad b_O &= \frac{1.5921118(0) + 0.062406390}{1.5921118 + 1} = 0.024075501 \\ (O) \quad c_O &= \frac{1.5921118(0.058795860) + 0}{1.5921118 + 1} = 0.036113250 \end{aligned} \right\} \quad (95)$$

Calculation of enthalpy of fuel and oxidant or of propellant. - Let h_F and h_X be the enthalpy per gram of equivalent fuel and per gram of equivalent oxidant, respectively. Then the enthalpy per gram of equivalent reactant $Z_{a_O} Y_{b_O} X_{c_O} \dots$ is

$$H_O = h_O = \frac{(O/F)h_x + h_o}{(O/F) + 1} \quad (96)$$

Equation (96) may be illustrated by again considering the reaction of equation (1). Using values similar to those on page 19 of reference 9 and the O/F value from equation (94),

$$\left. \begin{aligned} h_{N_2H_4} = h_f &= \frac{154,702.97}{32.048} = 4827.2269 \text{ cal/g} \\ h_{H_2O_2} = h_x &= \frac{28,681.626}{34.016} = 843.18043 \text{ cal/g} \end{aligned} \right\} \quad (97)$$

$$h_O = \frac{1.5921118 (843.18043) + 4827.2269}{1.5921118 + 1} = 2380.1691 \text{ cal/g} \quad (98)$$

Optional specification of O/F. - In addition to the oxidant to fuel weight ratio O/F, two other quantities may be used to give the relative amounts of oxidant and fuel. One of these is the weight percent of fuel in the propellant %F and the other is the equivalence ratio r.

(1) %F: The relation between O/F and %F is given by

$$\%F = \frac{100}{(O/F) + 1} \quad (99)$$

(2) Equivalence ratio r: The equivalence ratio is defined in terms of arbitrary, permanently assigned oxidation states for each element in a compound. This practice produces no difficulty so long as all the elements have the assigned oxidation state in all their compounds (e.g., H = +1, Na = +1, F = -1). Some elements have various oxidation states; for example, sulfur, which has the oxidation numbers -2, +4, +6 in the compounds H₂S, SO₂, and H₂SO₄, respectively. In cases such as this the assigned oxidation states are taken to be those considered as occurring commonly in products. For this reason it is possible that some components of the propellant combination may show a net positive or negative oxidation state, contrary to the usual practice of having the sum of the oxidation numbers of a compound add up to zero.

Let V_Z^+ , V_Y^+ , V_X^+ . . . be the positive oxidation states and V_Z^- , V_Y^- , V_X^- . . . be the negative oxidation states of the elements Z, Y, X . . . in the reactant. Let V_x^+ and V_x^- be the total positive oxidation state and total negative oxidation state, respectively, per gram of equivalent oxidant, and let V_f^+ and V_f^- be the total positive and negative oxidation states, respectively, per gram of equivalent fuel. Then,

$$\left. \begin{aligned} V_x^+ &= \left[a_x V_Z^+ + b_x V_Y^+ + c_x V_X^+ + \dots \right] \\ V_x^- &= \left[a_x V_Z^- + b_x V_Y^- + c_x V_X^- + \dots \right] \\ V_f^+ &= \left[a_f V_Z^+ + b_f V_Y^+ + c_f V_X^+ + \dots \right] \\ V_f^- &= \left[a_f V_Z^- + b_f V_Y^- + c_f V_X^- + \dots \right] \end{aligned} \right\} \quad (100)$$

The total positive oxidation state V^+ and total negative oxidation state V^- per gram of propellant are

$$\left. \begin{aligned} V^+ &= \frac{(O/F)V_x^+ + V_f^+}{(O/F) + 1} \\ V^- &= \frac{(O/F)V_x^- + V_f^-}{(O/F) + 1} \end{aligned} \right\} \quad (101)$$

The equivalence ratio may now be defined as

$$r \equiv \left| \frac{V^-}{V^+} \right| = \left| \frac{V_f^- + (O/F)V_x^-}{V_f^+ + (O/F)V_x^+} \right| \quad (102)$$

This definition of r gives $r = 1$ for stoichiometric conditions, $r > 1$ for oxidant-rich conditions, and $r < 1$ for fuel-rich conditions. For those who prefer to consider $r > 1$ for fuel-rich conditions and $r < 1$ for oxidant-rich conditions, the reciprocal of r in equation (102) may be taken as the definition of equivalence ratio, provided that the computing program be correspondingly modified.

The reaction of equation (1) may be again taken to illustrate equations (100) and (102). Let a, b, c refer to H, N, O, respectively. Then, from equation (100),

$$\left. \begin{aligned} \text{H}_2\text{O}_2 \quad & \left\{ \begin{aligned} V_x^+ &= [2(1) + (0)(0) + 2(0)]/34.016 = 0.058795860 \\ V_x^- &= [2(0) + (0)(0) + 2(-2)]/34.016 = -0.11759172 \end{aligned} \right. \\ \text{N}_2\text{H}_4 \quad & \left\{ \begin{aligned} V_f^+ &= [4(1) + 2(0) + 0(0)]/32.048 = 0.12481278 \\ V_f^- &= [4(0) + 2(0) + 0(0)]/32.048 = 0 \end{aligned} \right. \end{aligned} \right\} \quad (103)$$

From equation (102), and using the $O/F = 1.5921118$ of equation (94),

$$r = \left| \frac{(1.5921118)(-0.11759172) + 0}{(1.5921118)(0.058795860) + 0.12481278} \right| = 0.85714286 \quad (104)$$

For any problem it is sufficient to specify any one of the three quantities O/F , $\%F$, or r , since any two may be expressed in terms of the third. (See eqs. (99) and (102), e.g.)

Thermodynamic data. - Since the computer program solves for temperature simultaneously with composition, it was found convenient to represent the thermodynamic data for each product as a function of temperature as follows:

$$C_P^O/R = A + BT + CT^2 + DT^3 \quad (105)$$

$$H_T^O/RT = A + \frac{BT}{2} + \frac{CT^2}{3} + \frac{DT^3}{4} + \frac{E}{T} \quad (106)$$

$$S_T^O/R = A \ln T + BT + \frac{CT^2}{2} + \frac{DT^3}{3} + F \quad (107)$$

where T is in degrees Kelvin. The function H_T^O/RT must include H_O^O/RT , where H_O^O is the reference enthalpy at $0^\circ K$ (see eq. (14)).

In order to minimize the errors resulting from a functional representation of the thermodynamic data, the six coefficients A , B , C , D , E , and F for each product were obtained from a simultaneous least-squares fit of the thermodynamic functions C_P^O/R , H_T^O/RT , and S_T^O/R for several selected temperature intervals with continuity from one interval to the next. Coefficients for several substances in the C , H , O , N , F , and Cl chemical system are given in table I.

Calculating Routines

The Main Calculating Program consists of ten major routines and several auxiliary routines with suitable connecting links. These routines are described in the following sections.

Packed vector loading routine. - The flow chart for the packed vector loading routine is given in figure 6. This short program permits direct loading of the packed vectors from the Vector and Propellant Program. The packed vectors are in the form of load hub cards on which the second word gives the permanent code number associated with the reaction product, and the fourth word gives the packed vector for the same product. The permanent code and the packed vector are loaded into sequential locations in

the P region; that is, the code and packed vector from the first card are placed into "P0001" and "P0002," respectively; the code and vector from the next card are placed into "P0003" and "P0004," and so forth.

When the program encounters a condensed phase, it examines the contents of the word "OASIS" to determine whether or not this product is to be considered in the first iteration. Thereafter, the decision to use or not to use a condensed phase is made internally. All positions of "OASIS" must be either zero or one, a zero indicating use and one indicating nonuse of a condensed phase. Each position of "OASIS" corresponds to a different condensed phase; thus position 1 (right-most position) is associated with the first condensed phase encountered, position 2 with the second, and so forth. For example, if "OASIS" contained

00 0000 1101 +

the program would not initially consider the first, third, and fourth condensed phases encountered. Should only two condensed-phase packed vectors be present, the program will ignore all positions beyond the first two. If the operator does not specify the contents of "OASIS," the program puts ones in all positions, thus initially considering only the gas phase.

The packed vector loading routine requires a transfer card to precede the first packed vector. The transfer card is a load hub card on which the first word is

NOP 0000 V0001 + (or numerical equivalent, 000000 1599+)

The last packed vector must be followed by another load hub card on which the first word is

00 0000 0000+

The packed vectors themselves must be arranged so that all the gaseous atoms enter storage before any gaseous molecules or condensed phases. If this condition is not met, a programmed stop will halt the loading. (The vectors for gaseous atoms may be loaded in any order followed by the remainder of the vectors in any order. However, the thermal data coefficients must be loaded in the same order as the vectors.) As each gaseous atom and each condensed-phase vector considered by "OASIS" is placed into storage, it is counted so that the two constants "ATOM1" and "SYS," used to specify the size of the reduced augmented matrix, may be obtained. Both of these are fixed point numbers in the low-order positions. "ATOM1" gives the number of different elements in the chemical system, and "SYS" gives the number of elements plus the condensed phases currently being considered. During the course of loading packed vectors, any load card with word 2 blank or zero will be bypassed.

Input data routine. - The flow chart for the input data routine is given in figure 7. The routine converts the input data as specified by the operator into suitable form for use in the computer. Thus, using equations (99) and (102), it calculates any two of the quantities O/F , r , and $\%F$ from the one which is supplied by the operator. The numbers $a_0, b_0, c_0, \dots, h_0$ are calculated from $a_f, a_x, b_f, b_x, \dots, h_x, h_f$ using equations (92) and (96). Also, the combustion-chamber pressure in pounds per square inch absolute is converted to atmospheres.

The input data for this routine and, hence, for the general program consist of the following:

(1) A 4-digit identification number for the problem (case no.) is loaded into "FO039" as

0000 Case no. 00+

(2) The chamber pressure P_c in pounds per square inch absolute is loaded into "FO000."

(3) The numbers $a_x, b_x, \dots, j_x; h_x, V_x^+$, and V_x^- are loaded into locations 0537, 0538, \dots ; 0547, 0548, and 0549, respectively, and the numbers $a_f, b_f, \dots, j_f; h_f, V_f^+$, and V_f^- are loaded into locations 0587, 0588, \dots ; 0597, 0598, and 0599, respectively. If the Vector and Propellant Program is used, these numbers will be prepared automatically.

(4) Any one of the three quantities O/F , r , and $\%F$ is loaded into "O/F," "EQRAT," or "PCT F," respectively, while the other two are loaded as zero.

(5) A schedule of up to 25 pressure ratios is loaded into the region R(1075-1099).

A set of estimates for $\ln p_i, n_N, \ln T$, and $\ln A$ is already provided by the program and need not be supplied unless one wishes to use a better set of estimates. Convergence usually occurs without good estimates.

The output from this routine is seven Bell format cards (see discussion in section on "Auxiliary routines" and also appendix B). The first Bell card contains the following six words: $r, O/F, \%F, P_c$ (atm), h_0 (cal/g), and the identification number for the problem. The identification number is a composite of the equivalence ratio, the case number, and the chamber pressure in pounds per square inch absolute. The input data $a_f, b_f, \dots, j_f; h_f, V_f^+, V_f^-, a_x, b_x, \dots, j_x; h_x, V_x^+$, and V_x^- are punched out on the next six Bell cards. A console-controlled punch can be used to obtain the calculated numbers $a_0, b_0, \dots, (h_0/R)$.

Load thermal data routine. - The thermodynamic data for each reaction product are represented by six coefficients A, B, C, D, E, and F, which were discussed in the section on "Thermodynamic data." The routine requires the coefficients to be on a load hub card in columns 21 through 80 (the last six words). The first word on the card is actually the first instruction in the routine following the read command for a basic load card and is

RAL 9051 RDB

The second word is the identification for the card, being a composite of the permanent code for the molecule and the low temperature (divided by 10) and high temperature (divided by 10) of the interval for which the coefficients were obtained. Thus, if the code for the molecule is 0121 and the temperature range is from 2600° to 3200° K, word 2 would be

Code	T _{low}	T _{high}
0121	260	320

With this scheme no molecule may have a code greater than four digits in length or a temperature interval higher than 9990° K.

The information from a thermodynamic coefficient card appears on the drum in a block of ten consecutive storages in the T region. The first word of the block contains the permanent code for the molecule in the instruction address position. For the previous example this would be

00 0000 0121

The following six storage positions contain the thermal coefficients. The eighth word is reserved for the composition estimate $\ln p_i$ or n_N , while the last two words of the block are reserved for q_i and $-\delta_i$. Since the sequential blocks of ten storages are assigned to reaction products on the basis of their order of appearance, within any temperature interval the order of the thermal data cards must match the order of the packed vectors. If this is not so, a programmed stop will halt the loading of the thermal coefficients.

Each set of basic load cards corresponding to some temperature interval must be followed by a Bell format card that is filled with zeros except for words 1 (columns 11 to 21) and 2 (columns 22 to 32). Word 1 is the floating point number for the low temperature, and word 2 is the floating point number for the high temperature of the interval covered by the preceding cards.

The flow chart for the load thermal data routine is given in figure 8.

Unpacking routine and thermal routine. - The purpose of the unpacking and thermal routines is to construct a "row vector." This row vector is a set of consecutive core storage locations representing a convenient arrangement of quantities that will eventually be used to construct the elements of the reduced augmented matrix. The row vector and its contents are as follows:

Symbolic location	Absolute location	Contents
RV000	9004	$(H_T^0/R)_i$ During expansion, zero during combustion
RV001	9005	$\left. \begin{matrix} a_i \\ b_i \\ c_i \\ d_i \\ e_i \\ f_i \\ g_i \\ h_i \\ i_i \\ j_i \end{matrix} \right\}$ Composition vector components as floating point numbers
RV002	9006	
RV003	9007	
RV004	9008	
RV005	9009	
RV006	9010	
RV007	9011	
RV008	9012	
RV009	9013	
RV010	9014	
RV011	9015	1 For gas, 0 for condensed
RV012	9016	q_i
RV013	9017	δ_i
RV014	9018	$(H_T^0/R)_i$ For combustion, $(S'/R)_i$ for expansion

Storage space has been provided for ten subscripts or ten components of the composition vector. If the chemical system being used does not require ten components, then the first component appears in the location "RV011" minus "SYS" and is followed by the remaining components. The locations from "RV001" to "RV010" minus "SYS" inclusive remain zero. The unpacking routine fills in the locations "RV001" through "RV011" inclusive, the thermal routine completing the remaining quantities. The flow chart for the unpacking routine is given in figure 9, while the thermal routine is given in figure 10.

Vector multiplication routine. - The vector multiplication routine calculates the elements of the reduced augmented matrix by multiplication of vectors. The gaseous-product contributions to the matrix elements of the mass-balance equations in figure 2 are generated by the following operation:

$$\begin{bmatrix} a_i p_i \\ b_i p_i \\ \cdot \cdot \cdot \\ \cdot \cdot \cdot \\ j_i p_i \end{bmatrix} \quad \begin{bmatrix} a_i, b_i, \cdot \cdot \cdot j_i, l, q_i, \delta_i \end{bmatrix} \quad (108)$$

Only those terms that are on or to the right of the principal diagonal are filled in. The gaseous-product contributions to the pressure-row elements are obtained from

$$p_i \begin{bmatrix} a_i, b_i, \cdot \cdot \cdot j_i, 0, q_i, \delta_i \end{bmatrix} \quad (109)$$

The gaseous-product contributions to the enthalpy-row elements are obtained from

$$\frac{p_i (H_T^O)_i}{R} \begin{bmatrix} a_i, b_i, \cdot \cdot \cdot j_i, l, q_i, \delta_i \end{bmatrix} \quad (110)$$

An entropy row is used in place of the enthalpy row during expansion, and the gaseous-product contributions to the entropy-row elements are given by

$$\frac{p_i S'_i}{R} \begin{bmatrix} a_i, b_i, \cdot \cdot \cdot j_i, l, q_i, \delta_i \end{bmatrix} \quad (111)$$

The condensed products each contribute a row to the reduced augmented matrix, which, for $Z_{a_N} Y_{b_N} X_{c_N} \cdot \cdot \cdot$, is

$$\begin{bmatrix} a_N, b_N, \cdot \cdot \cdot j_N, 0, q_N, \delta_N \end{bmatrix} \quad (112)$$

and, in addition, the contribution of this condensed product to the column $(-\Delta \ln A)$ is

$$\begin{bmatrix} a_N^{n_N} \\ b_N^{n_N} \\ \cdot \cdot \cdot \\ \cdot \cdot \cdot \\ \cdot \cdot \cdot \\ j_N^{n_N} \\ 0 \\ (H_T^O)_N^{n_N} \end{bmatrix} \quad (113)$$

The flow chart for this routine is given in figure 11.

Matrix completion routine. - This routine completes the matrix by calculating and adding to the appropriate matrix elements the quantities $A \Delta a, A \Delta b, \dots, A \Delta p, A \Delta h, \sum_i (C_P^O)_i n_i / R$ or $T \sum_i (C_P^O)_i n_i / R$, and reflecting the symmetric portions of the matrix about the diagonal. During expansion, $\sum_i (S_T)_i n_i / R$ replaces the term in the entropy row and $-\Delta \ln A$ column. When this has been completed, the routine examines all the error terms, requiring them to be smaller than some preassigned value before the iteration process is halted. After convergence is complete, the program checks to make sure that the thermal data for the correct temperature interval were used and examines the partial pressures of the condensable materials to ascertain whether or not condensed-phase products should have been considered. The flow chart for this routine is given in figure 12.

Matrix solution routine. - The correction variables for the gaseous atoms and condensed phases are obtained from the reduced augmented matrix (fig. 2) by the matrix solution routine presented in figure 13. The corrections to the gaseous molecules are obtained from the correction equations for the gaseous atoms using equation (29). When the iteration process has converged to the equilibrium values, this same routine is used to solve the two sets of equations discussed in the section on "Derivative Matrices."

The solution routine carries out a Gauss reduction on the linear set; that is, it eliminates the first variable from all equations following the first equation, the second variable from all equations following the second equation, and so on. The solution routine assumes that the equations appear in consecutive bands of storage, the n^{th} equation in band one, the $(n - 1)^{\text{th}}$ equation in band two, and so forth. Thus, the energy equation appears in band one and the pressure equation in band two. Within each band the coefficients of the variables are placed in consecutive storage locations with the constant term appearing in the last storage location of the band.

The number of equations to be solved must appear as an integer in the low-order positions of the upper accumulator when entering the routine. For the correction equations, this is specified by the constant "SYS + 2." The results of the solution appear in the first band with the first variable appearing in location 0043-"(SYS + 1)" as shown in the following table:

Storage location	Variable
0049 - "(SYS + 1)"	$\Delta \ln n_Z$
0049 - "(SYS)"	$\Delta \ln n_Y$
0049 - "(SYS - 1)"	$\Delta \ln n_X$
-----	-----
-----	-----
0046	Δn_M
0047	Δn_N
0048	$-\Delta \ln A$
0049	$\Delta \ln T$

Two entries to the routine are provided. The first is at location "SOLVE," and the second is at location "BACK." The first entry is used when the Gauss reduction must be performed, while the second is used when the reduction has already been accomplished and only the back solution is needed.

The solution routine can run into difficulty in several situations while carrying out the Gauss reduction. The first happens when the machine attempts to perform a floating multiplication of two numbers that are so small that the resulting product would be less than 10^{-51} , and an underflow occurs. This has been taken care of for several operations by using branch on overflow commands and replacing the result of the multiplication by a zero if underflow occurs.

A second difficulty occurs when the coefficient matrix of figure 2 is singular or nearly singular; that is, its determinant is zero or very nearly so. In this case, because of the way in which the reduction is performed, the machine attempts division by zero. This problem arises when the system is such that within the precision of the calculations only one reaction product exists, as may occur for stoichiometric conditions at low temperatures. For example, in the chemical system hydrogen and oxygen at low temperatures and stoichiometric conditions, gaseous water is the only reaction product of any significance. This type of difficulty may be handled by changing the relative amounts of oxidant and fuel slightly from stoichiometric conditions (perhaps 1 to 10 parts per million) and repeating the calculation.

A third, and perhaps the most difficult, situation occurs when the coefficient matrix is poorly conditioned. For example, if the coefficient of the k^{th} variable in the k^{th} equation is small relative to the coefficients of the $(k + 1)^{\text{th}}$, $(k + 2)^{\text{th}}$, . . . variables in the same equation, and if the k^{th} equation is then used to eliminate the k^{th}

variable from the $(k + 1)^{\text{th}}$, $(k + 2)^{\text{th}}$, . . . equations at an early stage of the calculations, then large rounding errors may occur. This situation occurs more often when condensed phases are present in the calculation than when only gaseous products are considered. In particular, if one chemical element appears almost exclusively in the condensed phase, the matrix element for this chemical element, which appears on the diagonal, will be very small. Should the row containing this small element be used to eliminate its variable at an early stage of the solution, then large rounding errors may occur, causing the solution vector obtained to bear little resemblance to the true solution vector.

To take care of this situation, a modified pivot method has been incorporated into the solution routine. This feature may be used at the operator's discretion, since it is console-controlled. An 8 in position one of the console (right-most position) causes pivoting. Prior to each elimination, the program examines the remaining equations and selects the best one for eliminating the next variable. The program selects the best equation to be that equation in which the coefficients differ by the smallest amount after division by the coefficient of the variable to be eliminated.

For the usual problems involving only gaseous products and those for which graphite is the only condensed phase, adequate solutions can be obtained without use of the modified pivoting routine. If no difficulty is expected, it is recommended that the pivot feature not be used, since each iteration will require more time.

Correction routine and performance-parameter routine. - The correction routine (fig. 14) applies the corrections to the estimates during the course of iteration. Once the iteration procedure has converged to a solution, the performance-parameter routine (fig. 15) calculates the performance parameters.

Auxiliary routines. - During the course of calculations it is necessary to use subroutines for exponentiation, taking square roots, and for punching the results of the calculations on Bell format cards. The subroutines that have been incorporated into the program for this purpose were taken from a collection of closed subroutines in reference 26. The three subroutines have been assembled in the locations 1833 to 1999, and a listing is given in appendix F. The arrangement of the words in the punch band by the punching subroutine, just prior to punching, and the corresponding card columns in which they are to appear are given in appendix B.

Because of the iterative nature of the calculation, it is at times desirable to have information on the progress of the calculations. This has been provided in the form of four console-controlled punches that

may be used individually or in any combination to give intermediate answers during the iterative process. However, because of storage limitations it was necessary to consider these intermediate answer-punching routines as expendable. For this reason they were assembled in the lower portions of the P and T regions and hence can only be used at the expense of a number of reaction products. The output of the punches is on Bell format cards. The punches are as follows:

(1) Console position 2: To be used only when there are 28 or less reaction products. An 8 in position 2 of the console causes punching, in order, of $(1 - P/P_0)$, $(1 - h/h_0)$, or $(1 - s/s_0)$ depending upon whether it is a combustion or expansion process, $(1 - a/a_0)$, $(1 - b/b_0)$, These are followed by the code and $-\delta_i$ for each reaction product.

(2) Console position 3: To be used only when there are 26 or less reaction products. An 8 in position 3 of the console causes punching of P, T, and A, followed by the code and n_i for each reaction product.

(3) Console position 4: To be used only when there are 26 or less reaction products. An 8 in position 4 of the console causes punching of the entire reduced matrix, one equation at a time.

(4) Console sign: To be used only when there are 28 or less reaction products. A minus sign on the console causes punching of the solution to the reduced augmented matrix.

Convergence

Because of the complexity and variability of the problem, no exact analysis can be made of the rate of convergence of the iteration. It is possible, however, to obtain useful information on the rate of convergence by studying a few representative chemical systems. A function E is defined that will be used to indicate the error left in the system by the current estimates:

$$E = \left(1 - \frac{P}{P_0}\right)^2 + \left(1 - \frac{h}{h_0}\right)^2 + \left(1 - \frac{a}{a_0}\right)^2 + \dots + \sum \delta_i^2 \quad (114)$$

where the summation includes all reaction products. The first group of terms will be called the mass balance errors, and the last group will be referred to as the equilibrium errors. Using identical initial estimates in all cases - namely, $p_i = 1$ atm, $n_N = 1 \times 10^{-11}$ mole, $T = 3800^\circ$ K, and $A = 148.4$ formula weights - it was possible to construct the curves given in figures 16 to 18.

From figure 16 it is seen that $\ln\sqrt{E}$ decreases linearly in the initial stages of the calculation, the slope increasing quite rapidly once E has been reduced to approximately 1. In other words, as convergence is approached, the rate of convergence increases. The erratic behavior of the curves for small E is due to loss of significance when convergence is essentially complete. Although the total error of the system is exponentially reduced in a rather systematic fashion, no such trend has been observed in the mass balance or equilibrium errors taken separately.

For the three cases shown in figure 16, 10 to 18 iterations were required to reduce the error to an acceptable limit when starting with poor estimates. The number of iterations may be even higher in some cases, in particular, if the temperature interval for the thermodynamic data that was selected on the basis of the initial estimate for the temperature is not the correct interval, or if there are any additions to or subtractions from the list of reaction products when the program checks for condensation of condensable materials.

The number of iterations can usually be significantly reduced if the correct assumption on the existence or nonexistence of condensed phases is made and if a good estimate for the reaction temperature and composition is available. A large number of iterations is unusual for pressure ratios other than the first, because the program uses the answers from the preceding calculation as estimates for the following point. These are generally good estimates, and therefore fewer iterations are required. This is illustrated in figure 17, where $\ln\sqrt{E}$ is plotted as a function of the iteration number. The data in figure 17 were obtained for the reaction of equation (1) using the same initial estimates as for figure 16. As shown by figure 17, convergence to combustion and throat conditions each required 11 iterations, while the following three exit points needed only 8, 6, and 5 iterations, respectively. The performance results of this example are given in table IV.

For the problem shown in figure 17, it was assumed that the iteration procedure had converged to a solution when each of the mass balance errors, such as $(1 - a/a_0)$, had a magnitude less than 5×10^{-7} and each of the equilibrium errors δ_i had a magnitude less than 5×10^{-6} :

$$\left. \begin{array}{l} \left| 1 - \frac{P}{P_0} \right| \\ \left| 1 - \frac{h}{h_0} \right| \\ \left| 1 - \frac{a}{a_0} \right| \\ \left| \dots \right| \end{array} \right\} < 5 \times 10^{-7}; \quad |\delta_i| < 5 \times 10^{-6}$$

These convergence criteria result in more accuracy than may be desired in some cases. For the example in figure 17, relaxing the convergence criteria by a factor of 10 permitted the total number of iterations to be reduced from 41 to 34 while still retaining five or more figures of accuracy in the final result.

When a poor set of estimates is made for the variables, the first iteration usually overcorrects the estimates and results in an increase in the value of E , as may be seen from figure 16. A solution to this problem is to restrict the size of the applied corrections. This technique is often used in iterative calculations; however, an increased number of iterations is generally required to converge. One procedure is to multiply each correction by some constant factor less than 1 (see ref. 19, e.g.). With such a technique it is often possible to induce convergence in what would normally be a divergent case, although an increased number of iterations is required. An alternative procedure has been developed that not only prevents overcorrection and produces convergence in all divergent cases that have occurred so far in this laboratory, but also often decreases the number of iterations required to reach convergence. In this procedure, the magnitude of each component of the solution vector of figure 2 must be less than a specified maximum value. If one or more components are larger than this specified maximum, the largest component is reduced to the specified maximum, and all the other components, including all $\Delta \ln p_i$, are reduced proportionally.

Figure 18 shows the effect of various maximum magnitudes imposed on the solution vector. Restricting the magnitudes of the components to 5 results in the fewest number of iterations for this case. In other cases a maximum component magnitude of 3 appeared to be best, particularly in systems with fewer chemical elements and reaction products.

The restriction of magnitude of the solution vector is given as an optional program and is discussed in the next section.

Program Modifications

The standard program is considered to be the program that first calculates combustion conditions for assigned enthalpy and pressure and then throat and other exit conditions assuming equilibrium composition of the reaction products during isentropic expansion. However, several modifications to the standard program are available.

The limitations to be discussed apply only to the particular assembly given in appendix F. If the program were assembled in some other fashion, then these limitations would no longer apply.

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Assigned enthalpy for series of pressures. - The first modification permits the calculation of an assigned enthalpy problem for a series of pressures. This is accomplished by changing one instruction of the program and can be done at no sacrifice in the number of permitted reaction products.

Restriction on magnitude of solution vector. - A second modification places a size restriction on the maximum magnitude of the solution vector of the matrix of figure 2. If any component is larger than this maximum value, then all the corrections, including $\Delta \ln P_1$, are multiplied a number less than 1 so that the maximum component of the solution vector of figure 2 becomes equal to the maximum permitted value. This program modification may be used only if no more than 26 reaction products are being considered. In addition, only the intermediate punches controlled by console position 2 and sign may be used.

Assigned temperature and pressure. - The third program modification permits calculations for an assigned temperature and pressure. This is done at a sacrifice of five reaction products; however, the intermediate punches controlled by console position 2 and sign may be used in addition to the program change that controls the size of the solution vector. The modified program for calculations at assigned temperature and pressure is not very efficient, since the program performs many unnecessary calculations. However, a more efficient program for this type of calculation can be made with more extensive modifications. The modified pivoting routine may not be used for assigned temperature and pressure calculations. To perform calculations at an assigned temperature for a series of pressures, the program modifications for an assigned enthalpy and a series of pressures must also be included.

Calculations for Assumption of Frozen

Composition During Expansion

Rocket performance parameters are generally calculated either with the assumption of complete chemical equilibrium among the combustion products during the expansion process (equilibrium expansion) or with composition remaining fixed at combustion-chamber composition during the expansion process (frozen composition). The method for calculating performance for the first assumption has been described in the previous sections. Performance calculations for the second assumption are the same with respect to determining combustion conditions; however, determination of exit conditions, which is described in the next section, is far simpler, since the composition of reaction products is already known.

Equations for frozen-composition isentropic expansion to assigned pressure. - Since composition during expansion is fixed as the combustion-chamber composition, the following relations are obtained:

$$\frac{(p_i)_c}{(p_i)_e} = \frac{(n_i)_c}{(n_i)_e} = \frac{A_c}{A_e} = \frac{P_c}{P_e} \quad (115)$$

Substituting equation (115) into equations (18), (19), and (20) and rearranging terms give, as the condition for frozen isentropic expansion,

$$\sum_i (n_i)_c (S_{T,i}^O)_{i_e} + R P_c \ln \frac{P_c}{P_e} = \left[\sum_i n_i (S_{T,i}^O) \right]_c \quad (116)$$

Equation (116) can be written in a form analogous to equation (20) if the following definitions are used:

$$S_e^f = \sum_i (n_i)_c (S_{T,i}^O)_{i_e} + R P_c \ln \frac{P_c}{P_e} \quad (117)$$

$$S_c^f = \left[\sum_i n_i (S_{T,i}^O) \right]_c \quad (118)$$

for then,

$$S_e^f = S_c^f \quad (119)$$

For an assigned exit pressure, equation (117) is a function of temperature only. For any guess of exit temperature T , equation (119) will not be satisfied identically, and hence an iteration scheme again is employed to converge to correct temperature. The total differential of equation (119) in finite-difference form is

$$\Delta S^f = (S_c^f - S_e^f) = \sum_i (n_i)_c (C_P^O)_i \Delta \ln T \quad (120)$$

or

$$\Delta \ln T = \frac{\Delta S^f}{\sum_i (n_i)_c (C_P^O)_i} \quad (121)$$

Equation (121) may be used to obtain new values of T until the value of ΔS^f is less than some assigned small value.

After convergence has been reached, the calculation of the rocket performance parameters is similar to that described for equilibrium composition during expansion.

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Description of program. - Because of storage limitations, the program for the calculation of rocket performance assuming frozen composition during expansion could not be incorporated as part of the standard program for equilibrium-composition calculations. Equilibrium composition in the combustion chamber is first calculated with the standard deck. The program for frozen-composition calculations is then read into storage and calculations for frozen composition are begun. Operating instructions for this program are given in appendix D, a flow diagram in figure 19, and a SOAP listing in appendix G.

VECTOR AND PROPELLANT PROGRAM

The Vector and Propellant Program was prepared in order to have a simple and almost automatic method of preparing the packed vectors and the quantities (henceforth referred to as packed propellants) a_f , b_f , c_f , . . . , a_x , b_x , c_x , . . . , V_f^+ , V_f^- , V_x^+ , V_x^- , h_f , and h_x . The output of this program serves as part of the input data for the Main Calculating Program (see input data routine). The storage locations for the packed propellants are a_x , b_x , c_x , . . . , 537 to 546; h_x , V_x^+ , V_x^- , 547, 548, 549; a_f , b_f , c_f , . . . , 587 to 596; h_f , V_f^+ , V_f^- , 597, 598, 599.

The flow diagrams for this program are given in figures 20 to 25 and are discussed in the section on "Calculating Routines." Operating instructions are given in appendix E, and a SOAP listing is given in appendix H. Included in the SOAP listing are two punch subroutines taken from reference 26. The format of the output of these two routines (Bell and Random) is given in appendix B. Also given in appendix B is the output format of the packed vectors.

There are ten types of input cards to the Vector and Propellant Program. The type of card is indicated by a symbol of two or three alphabetic or numerical characters appearing in columns 48, 49, and 50 of the IBM card. The data (if any) corresponding to the type of card follow in columns 51 through 72 of the card. The ten types and their functions are listed in the following table and will be discussed more fully in the following sections:

Symbol for type of input	Function	Comment
ATM	Specifies an alphabetic chemical vector for the gaseous atom; e.g., H, AL, or CL	No subscripts permitted for chemical symbol
BOP	Begins program by clearing and initializing	
END	Begins calculations (end of input data)	Begins calculation of a_f , a_x , b_f , b_x , etc.
EFn	Specifies enthalpy of n^{th} fuel in cal/g-mol	$0 \leq n \leq 9^*$
EXn	Specifies enthalpy of n^{th} oxidant in cal/g-mol	$0 \leq n \leq 9^*$
Fn	Specifies n^{th} fuel	$0 \leq n \leq 9^*$
MOL	Specifies all reaction products that are not atoms; e.g., H ₂ FL, NH ₃ , H ₂ CL	All subscripts must be given explicitly
PFn	Gives the weight percent or weight fraction of n^{th} fuel in combined fuel	Weight percent or weight fraction in floating point $0 \leq n \leq 9^*$
PXn	Gives weight percent or weight fraction of n^{th} oxidant in combined oxidant	Weight percent or weight fraction in floating point $0 \leq n \leq 9^*$
Xn	Specifies n^{th} oxidant	$0 \leq n \leq 9^*$

*n = 1 through 9 specifies fuel or oxidant 1 through 9, but n = 0 specifies the tenth fuel or oxidant.

Only two types of cards in the preceding table are general for every problem. These are BOP and END.

Transfer Cards

BOP - Initialize card. - The BOP card serves to initialize the program, preparing it to process a new collection of vector and propellant cards. BOP precedes all other input cards:

Input		Output
Card column		
3	+ Sign (12 punch)	
48-50	BOP	No output

END - Start calculations. - The END card follows at the end of all other input cards and serves as a transfer card to begin calculation of the packed propellants:

Input		Output
Card column		
3	+ Sign (12 punch)	
48-50	END	No output

Input for Packed Vectors

The preparation of the packed vectors requires only two types of input cards, ATM and MOL. These two types specify the products of reaction to be considered. For bookkeeping purposes each product of reaction is given a permanent 4-digit numerical code. This permanent code also appears on the thermodynamic data cards for the same product and serves as a check during calculations in the Main Calculating Program.

ATM - Atom cards. - The ATM cards are used to specify which chemical elements will be considered in the equilibrium calculations. They are to be used only for the gaseous atoms. The reduced matrix column assignments are based on the order of appearance of the ATM cards. ATM cards must precede all the other type cards with the exception of BOP cards. The output of an ATM card is a packed vector for the gaseous atom:

Input		Output	
Card column		Card column	
3	+ Sign (12 punch)	17-20	4-Digit code for gaseous element (same as 44-47 of input)
44-47	4-Digit permanent code for gaseous element	31-40	Packed chemical vector
48-50	ATM	41-80	Input reproduced
51-52	Chemical symbol for element, e.g., AL, CL, H (no numerical subscripts)		
53-80	Blank		

MOL - Molecule cards. - The MOL cards are used for the composition vectors of all reaction products that are not gaseous atoms. Thus, condensed elements such as graphite would be on MOL cards. The output of a MOL card is a packed vector for the corresponding product:

Input		Output	
Card column		Card column	
3	+ Sign (12 punch)	17-20	4-Digit code for reaction product
42	Sign (- for condensed phase, + or blank for gaseous phase)	31-40	Packed chemical vector
44-47	4-Digit permanent code for reaction product	41-80	Input reproduced
48-50	MOL		
51-65	Chemical symbol for reaction product. All subscripts must be explicitly given; e.g., CH_4 is ClH_4 H_2O is $\text{H}2\bar{0}1$ Al_2O_3 is $\text{AL}2\bar{0}3$ ($\bar{0}$ is an alphabetic character)		
66-80	Blank		

Input for Packed Propellants

A number of propellants consist of more than one fuel or one oxidant. The Vector and Propellant Program can accommodate a propellant consisting of a mixture of up to 10 fuels and up to 10 oxidants. Each fuel and each oxidant in the propellant is characterized by three cards. For the fuel, the three cards are Fn, PFn, and EFn; and for the oxidant, Xn, PXn, and EXn.

Fn - Fuel cards. - The Fn cards are used to specify the chemical formula of the n^{th} fuel, where n is any one of the integers 1, 2, 3, 4, 5, 6, 7, 8, 9, 0 (0 is used for the tenth fuel). The subscripts for elements on the fuel cards may either be integers less than 9 digits in length or floating point numbers. Either one or both forms may be used in the same Fn card. Should the chemical formula for the n^{th} fuel be too long to fit on one card (more than 22 columns) it may be continued on the next card providing that (1) the same Fn symbol is used, and (2) the complete numerical subscript for an element is on the same card as the alphabetic symbol for the element:

Input		Output	
Card column		Card column	
3	+ Sign (12 punch)	0-80	Input reproduced
43-47	Anything - never used in program		
48-49	Fn where $n = 1, 2, 3, 4, 5, 6, 7, 8, 9, 0$		
50	Blank		
51-72	Chemical formula for the fuel		

Three examples are given to illustrate Fn cards:

Fuel	Columns 48-49	Columns 51-72
N_2H_4	F1	N_2H_4
C_8H_{18}	F1	C_8H_{18} (or $\text{C}_8\text{H}_{18000000052}$)
Mixture of NH_3 and H_2	F1 F2	NH_3 H_2

Xn - Oxidant cards. - The Xn cards are identical to the fuel cards except that these cards are used for the n^{th} oxidant, and Fn in card columns 48 and 49 is replaced by Xn. Two examples are given to illustrate Xn cards:

Oxidant	Columns 48-49	*Columns 51-72
H ₂ O ₂	X1	H2O2
HN _{1.0529061} O _{3.0344255} (Red fuming nitric acid)	X1 X1	H1N1052906151 O3034425551

*O is an alphabetic character.

PFn - Percent fuel cards. - The percent fuel card PFn gives the weight percent of the n^{th} fuel in the fuel mixture. The percent or weight fractions must be expressed as floating point numbers. There must be a PFn card corresponding to each Fn card:

Input		Output	
Card column		Card column	
3	+ Sign (12 punch)	0-80	Input reproduced
48-50	PFn ($n = 1, 2, 3, 4, 5, 6, 7, 8, 9, 0$)		
51-60	Weight percent of n^{th} fuel in fuel mixture (a floating point number)		

Two examples are given to illustrate PFn cards:

	Columns 48-50	Columns 51-60
One fuel only	PF1	1000000053
Mixture of fuels (20 percent fuel 1, 80 percent fuel 2 by weight)	PF1 PF2	2000000052 8000000052

PXn - Percent oxidant cards. - The PXn cards are identical to the PFn cards except that they refer to the n^{th} oxidant.

EFn - Fuel enthalpy cards. - The EFn card format is identical to that of PFn and PXn, except that instead of weight percentages this type of card gives the enthalpy of the n^{th} fuel in calories per formula weight as a floating point number. An example is given to illustrate an EFn card:

	Columns 48-50	Columns 51-72
Enthalpy of N_2H_4 (l) at 298.16°K (see eq. (97))	EF1	1547029756

EXn - Oxidant enthalpy cards. - The EXn cards are the same as the EFn card except that they refer to oxidant rather than fuel.

Calculating Routines

Flow charts and tables. - Figure 20 gives a general flow chart for the Vector and Propellant Program and includes the BOP routine. Flow charts for the other routines are given in figures 21 to 25.

For the calculation of the packed propellants, the program requires a table of atomic weights and assigned oxidation states. The atomic weight table for 101 elements is located in the M region, while the corresponding table for the oxidation states is in the V region. The atomic weight table is complete, while oxidation-state assignments have been made only for several elements. Additions or alterations to the tables of atomic weights and oxidations states may be made as needed.

Formulas for propellants containing several fuels or several oxidants. - The program can prepare "packed propellant cards" for propellants containing as many as 10 fuels and 10 oxidants. The combination of all fuels is referred to as the equivalent fuel, while the combination of all oxidants is referred to as the equivalent oxidant. The necessary equations are given as follows:

According to the definitions given in previous sections, $Z_{a_f} Y_{b_f} X_{c_f} \dots$ and $Z_{a_x} Y_{b_x} X_{c_x} \dots$ refer to 1 gram of equivalent fuel and 1 gram of equivalent oxidant having enthalpies h_f and h_x , respectively, where $a_f, b_f, c_f \dots$ and $a_x, b_x, c_x \dots$ are the number of gram atoms of elements Z, Y, X, \dots in the gram of equivalent fuel and the gram of equivalent oxidant, respectively. Let the i^{th} oxidant have the formula $Z_{a_{x_i}} Y_{b_{x_i}} X_{c_{x_i}} \dots$, its mass W_{x_i} , and its

enthalpy $(H_T^O)_{x_i}$, while the i^{th} fuel has the formula $Z_{a_{f_i}} Y_{b_{f_i}} X_{c_{f_i}} \dots$, its mass W_{f_i} , and its enthalpy $(H_T^O)_{f_i}$. The total weight of oxidant is W_x and the total weight of fuel is W_f :

$$\left. \begin{aligned} W_f &= \sum_i W_{f_i} \\ W_x &= \sum_i W_{x_i} \end{aligned} \right\} \quad (122)$$

Therefore, the oxidant-to-fuel weight ratio is

$$\frac{O}{F} = \frac{W_x}{W_f} \quad (123)$$

The gram atoms of elements per gram of equivalent oxidant or fuel are

$$\left. \begin{aligned} a_x &= \frac{1}{W_x} \sum \frac{a_{x_i} W_{x_i}}{\mathcal{M}_{x_i}}, \quad b_x = \frac{1}{W_x} \sum \frac{b_{x_i} W_{x_i}}{\mathcal{M}_{x_i}}, \quad \dots \\ a_f &= \frac{1}{W_f} \sum \frac{a_{f_i} W_{f_i}}{\mathcal{M}_{f_i}}, \quad b_f = \frac{1}{W_f} \sum \frac{b_{f_i} W_{f_i}}{\mathcal{M}_{f_i}}, \quad \dots \end{aligned} \right\} \quad (124)$$

and the enthalpies are

$$\left. \begin{aligned} h_x &= \frac{1}{W_x} \sum \frac{(H_T^O)_{x_i} W_{x_i}}{\mathcal{M}_{x_i}} \\ h_f &= \frac{1}{W_f} \sum \frac{(H_T^O)_{f_i} W_{f_i}}{\mathcal{M}_{f_i}} \end{aligned} \right\} \quad (125)$$

Equation (124) may be used in equations (92) and (100) to obtain a_0 , b_0 , c_0 , \dots and V_x^+ , V_x^- , V_f^+ , and V_f^- , while equation (125) may be used in equation (96) to obtain h_0 .

Example

The propellant $\text{N}_2\text{H}_4 + \frac{3}{2} \text{H}_2\text{O}_2$ has been used in this report for purposes of illustration (see eqs. (1), (93), (94), (95), (97), and (98)). This same problem will be used to illustrate the input and output of the Vector and Propellant Program and the Main Calculating Program.

The products considered, which are all gaseous, are H, N, O, H_2 , H_2O , N_2 , NO, O_2 , and OH. The values of enthalpy for the propellants are similar to those on page 19 of reference 9:

$$(\text{H}_{298.16}^{\circ})_{\text{N}_2\text{H}_4(l)} = 154,702.97 \text{ cal/mol}$$

$$(\text{H}_{298.16}^{\circ})_{\text{H}_2\text{O}_2(l)} = 28,681.626 \text{ cal/mol}$$

The input and output of the Vector and Propellant Deck and the Main Operating Deck are given in tables II to V.

Lewis Research Center

National Aeronautics and Space Administration

Cleveland, Ohio, July 2, 1959

APPENDIX A

SYMBOLS

A	number of formula weights of equivalent reactant; also, cross-sectional area of a nozzle, sq in.
a	velocity of sound, $\sqrt{\left(\frac{\partial P}{\partial \rho}\right)_s}$, ft/sec
a,b,c, . . .	number of gram atoms of the elements Z,Y,X, . . .
C_F	thrust coefficient
C_P^o	molar heat capacity at constant pressure, cal/(mole)(°K)
C_V^o	heat capacity at constant volume, cal/(mole)(°K)
c^*	characteristic velocity, ft/sec
E	internal energy per unit mass, cal/mole; also error function defined by eq. (114)
F	free energy per mole of formula weight of material, cal/mole
%F	weight or mass percent fuel
g_c	gravitational conversion factor, 32.174 (lb mass/lb force)(ft/sec ²)
H	sum of sensible enthalpy and chemical energy per mole or formula weight of material, cal/mole
h	sum of sensible enthalpy and chemical energy per unit mass of material, cal/g
h^*	iteration parameter defined by eq. (85)
I	specific impulse with ambient and exit pressures equal, (lb force)(sec)/(lb mass)
I_{vac}	specific impulse in vacuum (ambient pressure equal to zero), (lb force)(sec)/(lb mass)

K	thermodynamic equilibrium constant
M	Mach number
\mathcal{M}	molecular weight, formula weight or atomic weight
N	number
n	number of moles or formula weights of material
O/F	oxidant-to-fuel weight or mass ratio
P	static pressure (sum of partial pressures), consistent units
p	partial pressure, consistent units
P _{vap}	equilibrium vapor pressure of gas
Q	any function
q	symbol for $\partial(-\Delta F_T^0/RT)/\partial \ln T = \Delta H_T^0/RT$
R	universal gas constant, consistent units
r	equivalence ratio defined by eq. (102)
S	entropy per mole, or formula weight of material
s	entropy per unit mass of material, cal/(g)(°K)
T	temperature, °K
U	velocity
V	oxidation state or volume
v	volume per unit mass
W	mass
w	mass-flow rate, (lb mass)/sec; also, weight or mass fraction
x,y	independent variables
Z,Y,X, . . .	symbols for the chemical elements

α	activity of a material
γ	isentropic exponent, $(\partial \ln P / \partial \ln \rho)_s$
δ	error in equilibrium equation, $\Delta F/RT$
ϵ	area ratio
π	with a subscript, a chamber-pressure exponent defined by eq. (76)
ρ	mass density, consistent units
Subscripts:	
c	combustion chamber or condensed phase
e	exit points of a nozzle
f_i	i^{th} fuel
g	gaseous phase
i	i^{th} product of reaction, i^{th} function, i^{th} variable
M,N	M^{th} , N^{th} , . . . condensed reaction products
P	constant pressure
r	equivalent reactant
s	constant entropy
T	at temperature T; also, constant temperature
t	throat of a nozzle
V	constant volume
x_i	i^{th} oxidant
Z,Y,X, . . .	refers to chemical elements
0	an assigned value, equivalent reactant, or absolute zero of temperature

Superscripts:

f	frozen composition during expansion
o	thermodynamic standard state
+	positive oxidation state
-	negative oxidation state

APPENDIX B

CARD FORMATS

Following are word arrangements for Bell, Random, and SOAP II output cards:

Word arrangement for Bell card:

Punch band	Card column
Word 1	11-21 (sign in 11)
Word 2	22-32 (sign in 22)
Word 3	33-43 (sign in 33)
Word 4	44-54 (sign in 44)
Word 5	55-65 (sign in 55)
Word 6	66-76 (sign in 66)
Word 7 (positions 8-5)	6-9 (location of word 1)
Word 8 (positions 8-5)	5, 77-79 (prob. no.)
Word 9 (position 5)	10 (word count)
Word 10 (positions 9-5)	80 (tab. space control)
	1-4 (card number)

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Word arrangement for Random card:

Punch band	Card column
Word 1	5-15 (sign in 15)
Word 2	20-30 (sign in 30)
Word 3	35-45 (sign in 45)
Word 4	50-60 (sign in 60)
Word 5	65-75 (sign in 75)
Word 6 (positions 8-5)	1-4 (location of word 1)
Word 7 (positions 8-5)	16-19 (location of word 2)
Word 8 (positions 8-5)	31-34 (location of word 3)
Word 9 (positions 8-5)	46-49 (location of word 4)
Word 10 (positions 8-5)	61-64 (location of word 5)
	76-80 (not used)

Word arrangement for SOAP II output (packed vectors):

Punch band	Card column	Comments
Word 9	1-10 (sign in 10), emitted	Not used in program
	11-20 (sign in 20)	Columns 17-20 are product code
	21-30 (sign in 30), emitted	Not used in program
Word 7	31-40 (sign in 40)	Packed vectors
Word 8 (position 1)	41	Reproduce input
Sign of word 7	42	
Word 1 (positions 5 to 1)	43-47	
Word 4 (positions 5 to 3)	48-50	
Word 1 (positions 5 to 1)	51-55	
Word 4 (position 2)	56	
Word 3 (positions 5 to 1)	57-61	
Word 4 (position 1)	62	
Word 5 (positions 5 to 1)	63-67	
Word 6 (positions 5 to 1)	68-72	

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APPENDIX C

OPERATING INSTRUCTIONS FOR MAIN CALCULATING PROGRAM

Normally the computer program will not be loaded as one instruction per card, SOAP cards, but will be subjected to some shrinking procedure that will permit loading of five or six instructions per card. (See appendix B for formats of Bell and Random cards.) Assuming this to be the case and also assuming that all input data which must be loaded are in the same card format, the following operating instructions apply for the Main Calculating Program:

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(1) Set console:

- (a) Storage entry switches (70 1951 9/8 9/8 9/8 9/8±):
 - An 8 in position 1 - pivoting during solution
 - An 8 in position 2 - punching of current errors
 - An 8 in position 3 - punching of current values for variables
 - An 8 in position 4 - punching of reduced augmented matrix
 - Minus sign - punching of solution vector for reduced augmented matrix

When the program has been loaded, the 9 in the position 7 of the console may be changed to an 8 if the operator does not wish the program to check for condensation.

- (b) Set programmed switch to STOP.
- (c) Set half-cycle switch to RUN.
- (d) Set control switch to RUN.
- (e) Set display switch to PROGRAM REGISTER.
- (f) Set overflow switch to SENSE.
- (g) Set error switch to STOP.

(2) Place cards in the read feed so that they will be read in the following order:

- (a) Loading routine for program
- (b) Computer program
 - Equilibrium program
 - Rocket package excerpt

(c) Input data to be loaded:

Case card

r card: O/F, %F, or r (any one of the three may be used)

Chamber-pressure card in lb/sq in. abs

Pressure-ratio schedule, as many as 25 pressure ratios

Atoms cards ($a_F, b_F, c_F, \dots j_F$;

$h_F, V_F^+, V_F^-, a_X, b_X, c_X, \dots j_X; h_X, V_X^+, V_X^-$)

(d) Packed vectors

(e) Thermodynamic data as coefficients

Items (a), (b), and (c) are loaded by a loading routine, while (d) and (e) are read into storage by program read commands.

(3) Ready the punch feed with blank cards.

(4) Press computer reset key.

(5) Press program start key.

To aid in detecting errors, programmed stops have been incorporated into the program. The following list gives the card number of the instruction, in the SOAP listing, which produced the stop; the contents of the program register at the time of the stop; and the significance of the stop:

Card number	Instruction	Significance
198	HLT 0000 7766	Thermal data out of order
229	HLT 0000 7777	Elements plus condensed phases greater than 10
325	HLT 0000 8855	Trying to process a molecule or condensed phase before all atoms done
378	HLT 0000 8866	Picked up wrong thermal data for the product
635	NZU XXXX 8877	Trying to process too many condensed phases
1702	HLT 0000 9955	Overflow occurred during construction of matrix
1740	HLT 0000 9966	Overflow occurred in back solution
1827	HLT 0000 9988	Some molecules ahead of some atoms
1570	NZU XXXX 9999	End of program

APPENDIX D

OPERATING INSTRUCTIONS FOR FROZEN COMPOSITION

E-417 To carry out frozen-composition calculations it is necessary first to perform an equilibrium-combustion calculation. Thus, the initial operating instructions are identical to those of the Main Calculating Program (appendix C), with the exception that an additional instruction is included (with the input data (2)(c)) that causes the program to stop when combustion calculations are complete. The instruction loads into storage location "FROZ" (1362) and is HLT 9999 9999 (01 9999 9999).

The following instructions apply after combustion calculations are complete:

- (1) Run out any cards remaining in the read hopper.
- (2) Place cards in the read feed hopper so that they will be read in the following order:
 - (a) Loading routine for program
 - (b) Frozen-composition program
 - (c) A transfer card to start program at "START"
 - (d) Thermodynamic data as coefficients
- (3) Press computer reset key.
- (4) Press program start key.

APPENDIX E

OPERATING INSTRUCTIONS FOR VECTOR AND PROPELLANT PROGRAM

The following operating instructions are for the Vector and Propellant Program, which may be used to prepare input data for the Main Calculating Program:

(1) Prepare the appropriate alphabetic ATM and MOL cards. There must be one ATM card for each chemical element and one MOL card for each other product of reaction.

(2) Prepare F_n , PF_n , and EF_n cards for each fuel, and X_n , PX_n , and EX_n cards for each oxidant in the equivalent reactant.

(3) Set console:

(a) Storage entry switches (70 1951 19 9/8 8^{\pm}); an 8 in position 2 - punching of fuels, oxidants, and percents and enthalpies of fuels and oxidants.

(b) Set programmed switch to STOP.

(c) Set half-cycle switch to RUN.

(d) Set control switch to RUN.

(e) Set display switch to PROGRAM REGISTER.

(f) Set overflow switch to STOP.

(g) Set error switch to STOP.

(4) Place cards in read feed so that they will be read in the following order:

(a) Loading routine for program

(b) Vector and Propellant Program

(c) Input data to be read:

BOP card (if desired)

ATM cards

MOL cards

F_n , PF_n , EF_n , X_n , PX_n , EX_n in any order

END card

(5) Ready punch feed with blank cards.

(6) Press computer reset key.

(7) Press program start key.

As an aid in the detection of errors, the following programmed stops have been included in the program:

Card number	Instruction	Significance
337	HLT 9999 1111	Wrong symbol in ATM program
342	HLT 9999 2222	Wrong symbol in BOP program
351	HLT 9999 3333	Wrong symbol in EFn program
364	HLT 9999 4444	Wrong symbol in END program
378	HLT 9999 5555	Wrong symbol in EXn program
388	HLT 9999 6666	Wrong symbol in Fn program
395	HLT 9999 7777	Wrong symbol in MOL program
404	HLT 9999 8888	Wrong symbol in PFn program
414	HLT 9999 9999	Wrong symbol in PXn program
424	HLT 9999 0000	Wrong symbol in Xn program
460	HLT 2222 8888	Trying to process ATM card after MOL, Fn, or Xn cards
466	HLT 3333 7777	Symbol for atom has more than two letters
491	HLT 4444 6666	More than 10 atoms processed
500	HLT 5555 5555	Trying to process more condensed phases than are permitted
506	HLT 6666 4444	Formula for reaction product has more than 15 letters and digits
509	HLT 7777 3333	No chemical formula on MOL card
551	HLT 8888 2222	An element on a MOL card that did not appear on an ATM card
616	HLT 9988 9988	More than 10 ATM cards
665	HLT 4321 4321	Column equivalent for element not in table
680	HLT 2233 4455	Subscript for element greater than 10 digits
684	HLT 5544 3322	Subscript for element is 9 digits
713	HLT 8888 1111	Enthalpy or percent greater than 10 digits
784	HLT 1111 1111	Sum of percents not close enough to 100

APPENDIX F
MAIN OPERATING PROGRAM (CHEMICAL EQUILIBRIUM)

CHEMICAL EQUILIBRIUM PROGRAM

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1 1      PROTECT ROCKET PACKAGE EXCERPT
2 1      BY LOADING AVAILABILITY TABLE
3 1
4 1
5 1
6      SYN FROZ      1362
7      SYN CHEK      0499
8      SYN PROR      1904
9      SYN EXP F      1850
10     SYN SORT      1900
11     SYN PUNCH      1950
12     SYN CARDN      1852
13     SYN LINK      1855
14     SYN TEMP1      1048      LOW TEMP
15     SYN TEMP2      1049      HIGH TEMP
16     REG A0961      0980      ATOM DATA
17     REG B1247      1249      TWO 3 FOU
18     REG C9050      9050
19     REG D0001      0001
20     PLA 0001      0001
21     RLR 0037      0049
22     RLR 0087      0099
23     RLR 0137      0149
24     RLR 0187      0199
25     RLR 0237      0249
26     RLR 0287      0299
27     RLR 0337      0349
28     RLR 0387      0399
29     RLR 0437      0449
30     RLR 0487      0499
31     RLR 0537      0549
32     RLR 0587      0599
33     REG F1110      1149
34     REG G0001      0015
35     REG H0987      0999      EXTRA H F
36     REG I1001      1005
37     REG J1006      1012
38     REG K1013      1019
39     REG M9000      9000
40     REG N9015      9015
41     REG P1599      1659      PROD DATA
42     REG Q1020      1027
43     REG R1075      1099      PRES RATIO
44     REG T0660      0959      HEAT DATA
45     REG U0050      0058
46     REG Y0059      0065
47     REG Z1340      1349      PRESS ROV
48     EQU PCP      F0001
49     EQU TEE      F0002
50     EQU P      F0003
51     EQU H      F0004
52     EQU I      F0005
53     EQU M      F0006
54     EQU CF      F0007
55     EQU FPSIL      F0008
56     EQU MACH      F0009
57     EQU I VAC      F0010
58     EQU CP      F0011
59     EQU GAMMA      F0012
60     EQU LMPT      F0013
61     EQU LMTP      F0014
62     EQU S      F0015
63     EQU NI      F0016
64     EQU NT      F0017
65     EQU NEPS      F0018
66     EQU NCSTR      F0019
67     EQU CSTAR      F0020
68     EQU AW      F0021
69     EQU NAW      F0022
70     EQU HSTR      F0023
71     EQU AAY      F0024
72     EQU HC      F0025
73     EQU PECMC      F0026
74     EQU NAKT      F0027
75     EQU AKT      F0028
76     EQU HSTR2      F0029
77     EQU P1      F0030
78     EQU CONS1      F0031
79     EQU CONS2      F0032
80     EQU CONS3      F0033
81     EQU CONS4      F0034
82     EQU CONS5      F0035
83     EQU S2      F0036
84     EQU R      F0037
85     EQU GC      F0038
86     EQU IDENT      F0039

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87      EQU ONE      F0040
88      EQU LNAAV     G0001
89      EQU LNT        G0002
90      EQU SGR        G0003
91      EQU HGR        G0004
92      EQU AQMOL      G0005
93      EQU BQMOL      G0006
94      EQU COMOL      G0007
95      EQU DOMOL      G0008
96      EQU EQMOL      G0009
97      EQU FQMOL      G0010
98      EQU GQMOL      G0011
99      EQU HQMOL      G0012
100     EQU IQMOL      G0013
101     EQU JQMOL      G0014
102     EQU P3          G0015
103     EQU CODE        9000
104     EQU SIR         9001
105     EQU ATOM2       9002
106     EQU T           9003
107     EQU RV000       9004
108     EQU RV001       9005
109     EQU RV002       9006
110     EQU RV003       9007
111     EQU RV004       9008
112     EQU RV005       9009
113     EQU RV006       9010
114     EQU RV007       9011
115     EQU RV008       9012
116     EQU RV009       9013
117     EQU RV010       9014
118     EQU RV011       9015
119     EQU RV012       9016
120     EQU RV013       9017
121     EQU RV014       9018
122     EQU NI          9019
123     EQU A           9021
124     EQU B           9022
125     EQU C           9023
126     EQU D           9024
127     EQU E           9025
128     EQU F           9026
129     EQU LN NI       9027
130     EQU IA          9011
131     EQU IB          9012
132     EQU IC          9013
133     EQU ID          9014
134     EQU IE          9015
135     EQU IF          9016
136     EQU LN NI       9017
137     EQU TWO         9028
138     EQU THREE       9029
139     EQU FOUR        9030
140     EQU CPR         9031
141     EQU S CPR       9032
142     EQU HRT         9033
143     EQU S HRT       9034
144     EQU SR          9035
145     EQU S SR        9036
146     EQU MINFX       9045
147     EQU MINCO       9046
148     EQU MAXCO       9047
149     EQU VARRL       9048
150     EQU TEM 1       9049
151     EQU TEMPO       9059
152     EQU MOVE1       9058
153     EQU MOVE2       9059
154     EQU BASIC       9050
155     EQU INDXA       THREE
156     EQU INDXC       FOUR
157     EQU S1          C0001
158     EQU ELMIN       C0001
159     EQU NOROW       C0000
160     SYN RDR         1193
161     SYN PC          F0000
162 1
163 1
164      BEGIN      RAU LNT      SET TO      0000 60 0002 0107
165      STL COMEX   COMBUSTION 0107 20 0111 0114
166      STD PCPCT   FIRST PC   0114 24 0017 0020
167      LDD         EXP E      OVER P     0020 69 0023 1850
168      STU T       T FROM LNT 0023 21 9003 0031
169      LDD TDATA   PCP 1      0031 69 0034 0637
170 1
171 1      IF COMEX IS ZERO WE ARE DOING
172 1      COMBUSTION OTHERWISE EXPANSION
173 1      COMEX EQUALS MINUS UNITY FOR
174 1      THROAT AND PLUS UNITY FOR
175 1      EXPANSION
176 1
177 1

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178 1      READ THERMAL DATA ROUTINE FOR
179 1      GENERAL ROCKET PERFORMANCE
180 1      CALCULATION
181 1      TDATA  RAA 0000      0034 80 0000 0640
182 1      RAC 0000      TD001 0640 88 0000 0646
183 1      RCD BASIC  BELL      READ CARD 0646 70 9050 1046
184 1      RAL 9051      RDB      ARE WE 9050 65 9051 1193
185 1      RDB      SLT 0004      GOING TO 1193 35 0004 0103
186 1      STU 9051      STORE IN 0103 21 9051 0161
187 1      RAU P0001 A      COPRECT 0161 60 3599 0153
188 1      SLT 0001      PLACE 0153 35 0001 0109
189 1      SRT 0001      0109 30 0001 0115
190 1      SUP 9051      0115 11 9051 0073
191 1      NZU TD005      0073 44 0027 0028
192 1      LDD TD008 C      YES STORE 0028 69 6667 0070
193 1      STD 9058      THERMAL 0070 24 9058 0026
194 1      SET 9051      DATA 0026 27 9051 0081
195 1      SBB TD001 C      0081 28 6660 0113
196 1      AXA 0002      0113 50 0002 0019
197 1      AXC 0010      TD001 0019 58 0010 0646
198 1      HLT 0000      7766 0027 21 0000 7766
199 1      RAU 9051      WAS THE 1046 60 9051 0203
200 1      FSB T      DATA JUST 0203 33 9003 0033
201 1      BMI TDATA      READ IN 0033 46 0034 1037
202 1      RAU T      FOR THE 1037 60 9003 0645
203 1      FSB 9050      CORRECT 0645 33 9050 0025
204 1      BMI TDATA      INTERVAL 0025 46 0034 0029
205 1      SET 9050      0029 27 9050 0084
206 1      SBB TEMP1      UNPAK 0084 28 1048 0101
207 1
208 1
209 1      UNPACKING ROUTINE FOR GENERAL
210 1      ROCKET PERFORMANCE CALCULATION
211 1
212 1      ATOM1 IS THE NUMBER OF THE
213 1      ELEMENTS IN THE SYSTEM AND IS
214 1      IN THE I ADDRESS POSITION
215 1
216 1      SYS IS THE SUM OF ELEMENTS
217 1      AND CONDENSED PHASES IN THE
218 1      I ADDRESS POSITION AND MUST
219 1      BE LESS THAN OR EQUAL TO TEN
220 1
221 1      SYSTM IS GENERATED FROM SYS
222 1      BY SHIFTING TO THE D ADDRESS
223 1      POSITION
224 1
225 1      UNPAK  RAU UNITY      IS SYS 0101 60 0104 0159
226 1      SLT 0001      GREATER 0159 35 0001 0165
227 1      SUP SYS      THAN TEN 0165 11 0018 0123
228 1      BMI      UP000 0123 46 0076 0077
229 1      HLT 0000      7777 0076 01 0000 7777
230 1      UP000  RAU SYS      GENERATE 0077 60 0018 0173
231 1      SLT 0004      I ADDRESS 0173 35 0004 0083
232 1      CONSTANTS
233 1      STU SYSTM      SYS+1 AND 0083 21 0638 0641
234 1      RAL SYS      SYS+2 AND 0641 65 0018 0223
235 1      ALO UNITY      ATM-1 ALSO 0223 15 0104 0209
236 1      AUP 8001      D ADDRESS 0209 10 8001 0067
237 1      AUP 8002      CONSTANT 0067 10 8002 0075
238 1      STL SYS+1      SYSTM FROM 0075 20 0079 0032
239 1      STU SYS+2      SYS AND 0032 21 0036 0639
240 1      RAU ATOM1      ATOM1 0639 60 0642 0647
241 1      SUP UNITY      0647 11 0104 0259
242 1      STU ATM-1      0259 21 0164 0117
243 1      STL S CPR      CLEAR THE 0117 20 9032 0024
244 1      STD S HRT      SUMMATION 0024 24 9034 0030
245 1      STD S SR      STORAGES 0030 24 9036 0086
246 1      STD P      0086 24 1112 0215
247 1      RAL STORE      SET STORE 0215 65 0068 0273
248 1      SLO SYSTM      ORDER FOR 0273 16 0638 0643
249 1      LDD UP033      SUBSCRIPT 0643 69 1196 0649
250 1      SDA UP033      0649 22 1196 1199
251 1      LDD TH024      SET DATA 1199 69 0102 0105
252 1      SDA TH024      ADDRESS OF 0105 22 0102 0155
253 1      LDD TH035      TH024 AND 0155 69 0108 0211
254 1      SDA TH035      TH035 0211 22 0108 0261
255 1      RAU SYS      SET SOLIDS 0261 60 0018 0323
256 1      SUP ATOM1      COUNTER 0323 11 0642 1047
257 1      STU COUNT      1047 21 0152 0205
258 1      STD SOLID      0205 24 0158 0311
259 1      SLT 0004      SET 0311 35 0004 0021
260 1      RSL 8003      DATA 0021 66 8003 0129
261 1      ALO STORE      ADDRESS OF 0129 15 0068 0373
262 1      LDD VM007      VM007 AND 0373 69 0176 0179
263 1      SDA VM007      VM048 TO 0179 22 0176 0229
264 1      LDD VM048      RV011R 0229 69 0082 0035
265 1      SDA VM048      LESS SOLID 0035 22 0082 0085
266 1      RAU LNT      GET T FROM 0085 60 0002 0157
267 1      LDD UP001      EXP E      LNT 0157 69 0110 1850

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268 UP001 STU T 0110 21 9003 0167
269 LDD ATOM1 SET ATOM 0167 39 0642 1045
270 STD ATOM2 COUNTER 1045 24 9002 0151
271 1
272 1 INDEX ACCUMULATOR C WILL BE
273 1 USED FOR PICKING UP THE
274 1 THERMAL DATA IN THE FUTURE
275 1
276 RAC 0000 0151 88 0000 0207
277 RAA 0012 0207 80 0012 0163
278 PAU WIPE1 8003 0163 60 0016 8003
279 8003 STL 9007 A UP003 CLEAR THE 8003 20 9207 0078
280 UP003 NZA UP005 UP007 LAST 13 0078 40 0131 0132
281 UP005 SXA 0001 8003 POSITIONS 0131 51 0001 8003
282 UP007 RAB 0011 UP009 OF FIRST 0132 82 0011 1038
283 UP009 SET 9007 1038 27 9007 1043
284 STS 0037 A FOR MATRIX 1043 29 2037 1040
285 NZR 0012 1040 42 1243 0644
286 SXB 0001 1243 53 0001 1299
287 AXA 0050 UP009 1299 50 0050 1038
288 UP012 SET 9007 CLEAR THE 0644 27 9007 1399
289 STR H0001 H REGION 1399 29 0987 1190
290 RAA 0000 UP013 1190 80 0000 1246
291 UP013 PAR 0013 CLEAR 14 1246 82 0013 0207
292 PAU WIPE2 8003 CORE LOCA 0207 60 0255 8003
293 8003 STL RV001 R UP015 FOR ROW 8003 20 9405 0066
294 UP015 NZR UP017 UP019 VECTOR 0066 42 0069 0170
295 UP017 SXB 0001 8003 0069 53 0001 8003
296 1
297 1 INDEX ACCUMULATOR A WILL BE
298 1 USED FOR PICKING UP THE
299 1 CURRENT PRODUCT CODE IN FUTURE
300 1
301 1 DATA ADDRESS OF UP033 HAS BEEN
302 1 SET TO RV011R MINUS SYSTEM AT
303 1 START OF UNPAK ROUTINE
304 1
305 UP019 RAL P0001 A STORE PRGD 0120 65 3599 0253
306 NZE 0001 MATRX CODE IF 0253 45 0106 0257
307 SLT 0001 HERE IF NO 0106 35 0001 0213
308 NZU UP021 GO CLEAN 0213 44 0217 0118
309 SRT 0001 UP MATRIX 0118 30 0001 0125
310 STL CODE UP024 0125 20 9000 0182
311 UP021 SRT 0001 PASS UP 0217 30 0001 0423
312 STU T0008 C SOLID AND 0423 21 6667 0170
313 STD T0010 C SET NI AND 0170 24 6669 0027
314 AXA 0002 DELTA1 TO 0022 50 0002 0128
315 AXC 0010 UP019 ZERO 0128 58 0010 0120
316 UP024 RAU P0002 A GAS OR 0182 60 3600 0305
317 STL CHECK CONDENSED 0305 20 0309 0112
318 HVI UP037 SET ONE OR 0112 46 0265 0116
319 RSU 8003 UP029 LEAVE ZERO 0265 61 8003 0473
320 UP029 SRT 0002 UP030 IN RV011 0473 30 0002 0279
321 UP030 SUP 8003 0279 11 8003 1187
322 STD TEMPO 1187 24 9059 1293
323 AUP ATOM2 CHECK ATOM 1293 10 9002 0201
324 NZU UP031 0201 44 0355 0156
325 HLT 0000 8855 0355 01 0000 8855
326 UP031 SLT 0001 0156 35 0001 0263
327 ALO 51 0263 15 0166 0071
328 RAB 8003 UP033 STORE THE 0071 82 8003 1196
329 UP033 STL RV011 R SUBSCRIPT 1196 20 9415 0154
330 RAU TEMPO GET NEXT 0154 60 9059 0361
331 NZU UP029 SUBSCRIPT 0361 44 0473 0216
332 AXA 0002 THERM 0216 50 0002 0072
333 1
334 1 PREPARE FOR NEXT PRODUCT THEN
335 1 GO TO THE THERMAL ROUTINE
336 1
337 UP037 LDD ONE SET ONE IN 0116 69 1149 0252
338 STD RV011 RV011 0252 24 9018 0208
339 SRT 0002 IS IT ONE 0208 30 0002 0315
340 NZU UP030 ELEMENT 0315 44 0279 0220
341 STL TEMPO YES IT WAS 0220 20 9059 0178
342 SLT 0001 IS IT AN 0178 35 0001 0135
343 RAU 8002 ATOM 0135 60 8002 1393
344 SUP ONE 1393 11 1296 0251
345 NZU UP038 IT WAS A 0251 44 0405 0206
346 RAL TEMPO UP030 MOLECULE 0405 65 9059 0279
347 UP038 PAU ATOM2 IT WAS AN 0206 30 9002 0313
348 SUP UNITY ATOM 0313 11 0104 0359
349 STD CHECK 0359 24 0309 0162
350 STU ATOM2 0162 21 9002 0119
351 RAL TEMPO 0119 65 9059 0127
352 STU TEMPO UP031 0127 21 9059 0156
353 1
354 1 CONSTANTS FOR UNPACKING
355 STORE GO RV011 R 0000 0068 00 9415 0000
356 WIPE1 STL 9007 A UP003 0016 20 9207 0078
357 WIPE2 STL RV001 R UP015 0255 20 9405 0066
358 ONE 10 0000 0051 1149 10 0000 0051

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359 UNITY 00 0000 0001 0104 00 0000 0001
360 51 00 0000 0051 0156 00 0000 0051
361 UNF 10 0000 0000 1296 10 0000 0000
362 1
363 1
364 1 THERMAL ROUTINE FOR GENERAL
365 1 ROCKET PERFORMANCE CALCULATION
366 1
367 1 THE DATA ADDRESSES OF TH024
368 1 AND TH035 SHOULD BE SET TO
369 1 RV0118 MINUS SYSTEM AT START OF
370 1 UNPACKING ROUTINE
371 1
372 THERM SET 9020 PICK UP 0072 27 9020 0177
373 LRR T0001 C THERMAL 0177 08 6660 0363
374 1 DATA
375 RAU 9020 IS THIS 0353 60 9020 0121
376 SUP CODE THE RIGHT 0171 11 9000 0329
377 NZU TH003 DATA 0329 44 0133 0134
378 HLT 0000 8866 0133 01 0000 8866
379 TH003 RAU P0000 A 0134 30 3598 0303
380 RMI TH007 0303 46 0256 0307
381 1
382 1 IF DEALING WITH CONDENSED
383 1 PRODUCT SET LN NI TO ZERO
384 1
385 RAU LN NI LN NI IS 0206 60 9027 0413
386 STL LN NI REALLY NI 0403 20 9027 0270
387 STU NI TH009 0270 21 9019 0227
388 TH007 RAU LN NI GET NI 0307 60 9027 0365
389 LDD EXP E 0355 69 0168 1850
390 STU NI TH009 0158 21 9019 0227
391 TH009 SET TWO TWO 3 FOUR 0277 27 9028 0232
392 LDR R0001 ON CORE 0232 09 1247 0100
393 RAU D CALCULATE 0100 60 9024 0357
394 FMP T CPR 0357 39 9003 0160
395 FAD C 0150 32 9022 1039
396 FMP T 1009 39 9003 1042
397 FAD B 1002 32 9022 0171
398 FMP T 0171 39 9003 0074
399 FAD A 0074 32 9021 0353
400 1
401 1 S CPR S HRT S SR MUST BE
402 1 CLEARED AT MATRIX CLEARING
403 1
404 STU CPR 0303 21 9031 0411
405 FMP NI SUM CPRXNI 0401 39 9019 0214
406 FAD S CPR IN CORE 0204 32 9032 1442
407 STU S CPR 1443 21 9032 0301
408 RAU D CALCULATE 0301 60 9024 0409
409 FDV FOUR HRT 0409 34 9030 0212
410 FMP T 0202 39 9003 0415
411 STU TEMPO 0405 21 9059 0523
412 RAU C 0503 60 9023 0181
413 FDV THREE 0181 34 9029 0184
414 FAD TEMPO 0184 32 9059 0463
415 FMP T 0463 39 9003 0266
416 STU TEMPO 0266 21 9059 0573
417 RAU B 0503 60 9022 0231
418 FDV TWO 0201 34 9028 0234
419 FAD TEMPO 0204 32 9059 0513
420 FMP T 0503 39 9003 0316
421 STU TEMPO 0306 21 9059 0623
422 RAU F 0603 60 9025 0281
423 FDV T 0281 34 9003 0284
424 FAD TEMPO 0284 32 9059 0563
425 FAD A 0563 32 9021 1493
426 STU HRT 1493 21 9033 0351
427 FMP NI SUM HRTXNI 0351 39 9019 0204
428 FAD S HRT IN CORE 0204 32 9034 0183
429 STU S HRT 0183 21 9034 1041
430 RAU D CALCULATE 1041 60 9024 1449
431 FDV THREE SR 1449 34 9029 0302
432 FMP T 0302 39 9003 0455
433 STU TEMPO 0455 21 9059 0613
434 RAU C 0613 60 9023 0221
435 FDV TWO 0221 34 9028 0124
436 FAD TEMPO 0124 32 9059 0403
437 FMP T 0403 39 9003 0306
438 FAD B 0306 32 9022 0185
439 FMP T 0185 39 9003 1188
440 STU TEMPO 1188 21 9059 1195
441 RAU A 1195 60 9021 0453
442 FMP LNT 0453 39 0002 0352
443 FAD TEMPO 0352 32 9059 0331
444 FAD F 0331 32 9026 0461
445 FSR LN NI SR MINUS 0461 33 9027 1191
446 STU SR LN PI 1191 21 9035 1499
447 FMP NI SUM SR 1499 39 9019 0402
448 FAD S SR LESS LN PI 0402 32 9036 0381
449 STU S SR X NI CORE 0381 21 9036 1189
450 RAU CHECK IS IT ATOM 1189 60 0309 1063

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451 NZU TH023 1063 44 0267 0218
452 1
453 1 REGION A IS PERMANENT STORAGE
454 1 OF ATOM GAS THERMAL PROPERTIES
455 1
456 RAU HRT PERMANENT 0267 60 9033 0175
457 STU A0001 R STORAGE OF 0175 21 4961 0264
458 PAL SR HRT AND SR 0264 65 9035 0271
459 STL A0011 R LESS LN PI 0271 20 4971 0174
460 STU T0009 C OF GASEOUS 0174 21 6668 0321
461 STD T0010 C TH044 ATOMS 0321 24 6669 0122
462 TH023 RAU ATM-1 SET MULT 0218 60 0164 0169
463 RAB 8003 FREQUENCY 0169 82 8003 0228
464 STL TEMPO FOR CI 0228 20 9059 0136
465 SET 9050 0136 27 9059 1241
466 LRB A0001 TH024 1241 08 0961 0102
467 TH024 RAU RV011 R TH027 0102 60 9415 0459
468 NZU TH027 0459 44 1162 0314
469 FMP 9050 R 1163 39 9450 0366
470 FAD TEMPO 0366 32 9059 1245
471 STU TEMPO TH027 1245 21 9059 0314
472 TH027 NZB TH031 0314 42 0317 0268
473 SXB 0001 TH024 0317 53 0001 0102
474 TH031 RSU TEMPO 0268 61 9059 0225
475 FAD HRT 0225 32 9033 0505
476 STU RV012 CI IN 9016 0505 21 9016 1213
477 STD TEM 1 AND TEM 1 1213 24 9049 0219
478 STD T0009 C AND T REGN 0219 24 6669 0371
479 RAU ATM-1 SET MULT 0371 60 0164 0269
480 RAB 8003 FREQUENCY 0269 82 8003 0278
481 SET 9050 0278 27 9050 0233
482 LRB A0011 TH035 0233 08 0971 0108
483 TH035 RAU RV011 B 0108 60 9415 0465
484 NZU TH039 0465 44 0319 0320
485 FMP 9050 B 0319 39 9450 0172
486 FAD TEM 1 0172 32 9049 0401
487 STU TEM 1 TH039 0401 21 9049 0320
488 TH039 NZB TH043 0320 42 1073 0224
489 SXB 0001 TH035 1073 53 0001 0108
490 TH043 RAU TEM 1 0224 60 9049 0431
491 FSR SR DELTA I IN 0431 33 9035 0511
492 STU RV013 9017 0511 21 9017 0369
493 RSU 8003 STORE NEG 0369 61 8003 0277
494 STU T0010 C TH044 DELTA I IN 0277 21 6669 0122
495 TH044 AXC 0010 T REGION 0122 58 0010 0328
496 RAU HRT H OVER R 0328 60 9033 0235
497 FMP T IN HR 0235 39 9003 1238
498 STU HR 1238 21 1192 1295
499 RAU P0000 A 1295 60 3598 0503
500 RMI TH045 S PRIMED 0503 46 0356 0407
501 RAU SR OVER R 0407 60 9035 0515
502 FSB ONE TH050 0515 33 1149 0275
503 TH045 RAU SP TH050 0356 60 9035 0275
504 TH050 STU S1R TH051 IN S1R 0275 21 9001 0283
505 TH051 RAU COMEX 0283 60 0111 0565
506 NZU EXPAN COMB 0565 44 0419 0370
507 COMB RAU HR 0370 60 1192 1197
508 STL RV000 TH047 1197 20 9004 0254
509 EXPAN RAU S1R 0419 60 9001 0327
510 LDD HR 0327 69 1192 1395
511 STD RV000 TH047 1395 24 9004 0254
512 TH047 STU RV014 MULT 0254 21 9018 0561
513 1
514 1
515 ONE 10 0000 0051 1149 10 0000 0051
516 UNITY 00 0000 0001 0104 00 0000 0001
517 R0001 20 0000 0051 TWO 1247 20 0000 0051
518 R0002 30 0000 0051 THREE 1248 30 0000 0051
519 R0003 40 0000 0051 FOUR 1249 40 0000 0051
520 1
521 1
522 1 VECTOR MULTIPLICATION ROUTINE
523 1 FOR GENERAL ROCKET PERFORMANCE
524 1 CALCULATION
525 1
526 1 WHEN THERE ARE N EQUATIONS THE
527 1 NTH APPEARS IN BAND 1 AND THE
528 1 1ST APPEARS IN BAND N
529 1
530 1 IN THIS ROUTINE INDEX A WILL
531 1 TRACK THE CURRENT EQUATION B
532 1 WILL TRACK THE CURRENT
533 1 SUBSCRIPT C WILL TRACK THE
534 1 NUMBER OF MULTIPLICATIONS
535 1
536 1 THE SOLIDS COUNTER SHOULD BE
537 1 SET TO ITS MAXIMUM VALUE PRIOR
538 1 TO CLEARING MATRIX LOCATIONS
539 1

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540 1      THE DATA ADDRESSES OF VM007
541 1      AND VM048 SHOULD BE SET TO
542 1      RV011B MINUS SOLID AT THE
543 1      START OF THE UNPACKING ROUTINE
544 1
545 1
546 1      MULT      LDD 8005      VM001      STORE INDX 0561 69 8005 0367
547 1      VM001     STD INDXA      A AND C    0367 24 9029 1173
548 1      LDD 8007      FOP THE    1173 69 8007 0379
549 1      STD INDXC      TIME BEING 0379 24 9030 0285
550 1      RAU P0000 A    IS PRODUCT 0285 60 3598 0553
551 1      BMI VM042     CONDENSED 0553 46 0406 0457
552 1
553 1      GASEOUS PRODUCT PROCESSING
554 1
555 1      RAU SYS+1      SET INDXA 0457 60 0079 0333
556 1      MPY 50         TO SYS+1  0333 19 0186 0456
557 1      RAA 8002      TIMES 50   0456 80 8002 0615
558 1      RSU ATOM1     SET INDEXB 0615 61 0642 1297
559 1      RAB 8003      VM002      TO ATOM 1297 82 8003 0506
560 1
561 1      VM002      RAC 8003      SET INDEXC 0506 88 8003 0364
562 1      LDD SOLID    TO INDEXB  0364 69 0158 0611
563 1      SXC 8001     LESS SOLID 0611 59 8001 0417
564 1      SXC 0002     VM007      LESS TWO 0417 59 0002 0126
565 1      VM007      RAU RV011 B  IS IT ZERO 0126 60 9415 0383
566 1      NZU         VM023      SUBSCRIPT 0383 44 1237 1288
567 1      FMP NI      SUBSCRIPT 1237 39 9019 1240
568 1      STU TEMPO   TIMES NI    1240 21 9059 1397
569 1      SET 9037     BRING IN    1397 27 9037 0452
570 1      LDB 0037 A VM013      EQUATION 0452 09 2037 1290
571 1      VM013      RAU RV013 C  1290 60 9617 1447
572 1      NZU         VM017      1447 44 0451 0502
573 1      FMP TEMPO   PERFORM A    0451 39 9059 0304
574 1      FAD 9049 C  MULTIPLY     0304 32 9649 0433
575 1      STU 9049 C VM017      AND ADD  0433 21 9649 0502
576 1      VM017      NZC         VM021  ANY MORE 0502 48 0555 0556
577 1      AXC 0001     VM013      TO MULTIPLY 0555 58 0001 1290
578 1      VM021      SET 9037     0556 27 9037 1061
579 1      STB 0037 A VM023      1061 29 2037 1288
580 1      VM023      AXB 0001     ANY MORE 1288 52 0001 1044
581 1      NZB         VM027      EQUATIONS 1044 42 1497 0648
582 1      RAU 8006     VM002      1497 60 8006 0605
583 1      SXA 0050     0605 51 0050 0506
584 1      RAA 0000     COMPLETE    0648 80 0000 0354
585 1      RAB 0001     BOTH THE    0354 82 0001 0210
586 1      RAU RV014   ENTROPY     0210 60 9018 0467
587 1      VM101      NZU         VM104  AND THE  0467 44 0421 0222
588 1      FMP NI      ENTHALPY    0421 39 9019 0274
589 1      STU TEMPO   DURING THE  0274 21 9059 0481
590 1      RAU SYS+2   EXPANSION    0481 60 0036 1291
591 1      RSC 8003     SET INDXC   1291 89 8003 0150
592 1      SET 9037     0150 27 9037 0655
593 1      LDB 0037 A VM028      0655 09 2037 1390
594 1      VM028      RAU RV013 C  DO THE  1390 60 9617 1547
595 1      NZU         VM031      LAST      1547 44 0501 0552
596 1      FMP TEMPO   EQUATION    0501 39 9059 0404
597 1      FAD 9049 C  WHICH IS    0404 32 9649 0483
598 1      STU 9049 C VM031      ENTHALPY 0483 21 9649 0552
599 1      VM031      NZC         VM035  OR ENTROPY 0552 48 1055 0606
600 1      AXC 0001     VM028      1055 58 0001 1390
601 1      VM035      SET 9037     0606 27 9037 1161
602 1      STB 0037 A VM104      1161 29 2037 0222
603 1      VM104      NZB         VM036  0222 42 0325 0176
604 1      SXB 0001     DURING     0325 53 0001 0531
605 1      RAA 0950     EXPANSION   0531 80 0950 1287
606 1      RAU RV000   ENTHALPY    1287 60 9004 0467
607 1
608 1
609 1
610 1
611 1      VM036      RAU SYS+2     IS IN 0950
612 1      STL RV011    BAND        ALSO FILL 0176 60 0036 1391
613 1      RSC 8003     IN THE      PRESSURE 1391 20 9015 1198
614 1      SET 9037     EQUATION    1198 89 8003 0656
615 1      LDB 0087     0656 27 9037 1211
616 1      VM037      RAU RV013 C  1211 09 0087 1440
617 1      NZU         VM039      1440 60 9617 1597
618 1      FMP NI      1597 44 0551 0602
619 1      FAD 9049 C  0551 39 9019 0454
620 1      STU 9049 C VM039      0454 32 9649 0533
621 1      VM039      NZC         VM041  0533 21 9649 0602
622 1      AXC 0001     VM037      0602 48 1105 1056
623 1      VM041      SET 9037     1105 58 0001 1440
624 1      STR 0087     1056 27 9037 1261
625 1      RAU NI      SUM PI      1261 29 0087 1490
626 1      FAD P       1490 60 9019 1697
627 1      STU P       1697 32 1112 1239
628 1      VM061      1239 21 1112 1065

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629 1          CONDENSED PRODUCT PROCESSING
630 1
631 1          COUNT IS NUMBER OF UNPROCESSED
632 1          CONDENSED PRODUCTS
633 1
634   VM042   RAU COUNT          0406 60 0152 0507
635           NZU                0507 44 1311 8877
636 1
637 1          ARE WE TRYING TO PROCESS TOO
638 1          MANY CONDENSED PHASES
639 1
640           RSR 8003          SET THE      1311 83 8003 0420
641           ALO 8003          INDICES TO   0420 15 8003 0377
642           SUP UNITY        STORE         0377 11 0104 0509
643           ALO 8001          CONDENSED    0509 15 8001 0517
644           STU COUNT        PHASE         0517 21 0152 1155
645           RAU 8002          EQUATION      1155 60 8002 1263
646           MPY 50           AND ITS       1263 19 0186 1106
647           RAA 8002          ENTHALPY     1106 80 8002 1165
648 1
649           SET RV001         OR ENTROPY
650           STB 0037 A       STORE THE     1165 27 9005 0470
651           RAU RV014        EQUATION      0470 29 2037 1540
652           STU 0047 P       STORE THE     1540 60 9018 1747
653 1           ENTHALPY      1747 21 4047 0200
654           OR ENTROPY
655           FMP NI          COMPLETE      0200 39 9019 0603
656           FAD 0047        ENTHALPY      0603 32 0047 1223
657           STU 0047        ROW           1223 21 0047 0250
658           RAU COMEX       VM111
659           NZU              0250 60 0111 1215
660           RAU RV000       1215 44 0469 0520
661           STU H0011 B     0469 60 9004 0427
662           FMP NI          0427 21 4997 0300
663           FAD H0011       0300 39 9019 0653
664           STU H0011       0653 32 0997 1273
665           RAU SYS+1       1273 21 0997 0520
666           MPY 50          COMPLETE      0520 60 0079 0583
667           RAA 8002        THE COLUMN    0583 19 0186 1156
668           RAU ATOM1       FOR AAY       1156 80 8002 1265
669           RSB 8003       1265 60 0642 1797
670           RAU RV011 B     1797 83 8003 0082
671           NZU             0082 60 9415 1289
672           FMP NI          1289 44 1543 1194
673           FAD 0047 A     1543 39 9019 1396
674           STU 0047 A     1396 32 2047 1323
675           AXR 0001       1323 21 2047 1194
676           NZR             1194 52 0001 0350
677           SXA 0050       0350 42 1053 1065
678           RAA INDXA       1053 51 0050 0082
679           RAC INDXC       1065 40 9029 1373
680 1           GO TO NEXT
681 1           PRODUCT      1373 88 9030 1246
682 1
683 1          CONSTANTS FOR VECTOR MULTIPLY
684 1          ROUTINE
685 1          50          00 0000 0050          0186 00 0000 0050
686 1
687 1          MATRIX CLEAN UP ROUTINE FOR
688 1          GENERAL ROCKET PERFORMANCE
689 1          CALCULATION
690   MATRX   RAU LNAAY        GET AAY      0257 60 0001 1205
691   MCC03   LDD MCC03        FROM         1205 69 0258 1850
692           STU AAY          LNAAY        0258 21 1133 0236
693           LDD ATM-1        SET INDXB    0236 69 0164 0567
694           RAR 8001         TO ATM-1     0567 82 8001 1423
695           RAU SOLID        1423 60 0158 1313
696           AUP UNITY        SET INDXA    1313 10 0104 0559
697           AUP 8001         TO SOLID     0559 10 8001 0617
698           MPY 50          PLUS TWO     0617 19 0186 1206
699 1           RAA 8002       TIMES 50    1206 80 8002 1315
700   MCC07   RAU AQMOL P     MCC09        ADD MASS      1315 60 4005 0609
701   MCC09   FMP AAY         BALANCE      0609 39 1133 0653
702           STU TEMPO        AND         0633 21 9059 1441
703           FSR 0047 A       ENTHALPY    1441 33 2047 1473
704           FAD 0049 A       OR ENTROPY   1473 32 2049 0375
705           STU 0049 A       DELTAS TO    0375 21 2049 0652
706 1           MATRIX
707           RAU TEMPO        STORE        0652 60 9059 0659
708           FSR 0047 A       ERRORS       0659 33 2047 1523
709           EDV TEMPO        1523 34 9059 0226
710           STU RV002 R      0226 21 9406 0983
711           RMR MCC031       0983 43 0286 1337
712           NZR MCC015       1337 42 1590 1491
713   MCC15   SXR 0001        1590 53 0001 1446
714           AXA 0050       1446 50 0050 1315
715   MCC17   RAA 0000       1491 80 0000 1298
716           RSR 0001        1298 43 0001 0504
717           RAU COMEX        0504 60 0111 1365
718           NZU MCC019       1365 44 0519 0570
719   MCC19   LDD S SR        0519 69 9036 0425
720           STD 0047        IN ENTROPY    0425 24 0047 0400

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721		RAU SOLR	MC009	ROW AND	0400	60	0003	0609
722	1			COLUMN A				
723	MC021	RAU H0/R	MC009		0570	60	0004	0609
724	MC031	RAU P0		ADD	0286	60	0015	0569
725		FSR P		PRESSURE	0569	33	1112	1339
726		STU TEMPO		DELTA TO	1339	21	9059	1398
727		FAD 0099		MATRIX	1298	32	0099	0475
728		STU 0099			0475	21	0099	1052
729		RAU TEMPO		STORE	1052	60	9059	1059
730		FDV P0		ERROR	1059	34	0015	1415
731		STU RV000	MC103		1415	21	9004	1573
732	MC103	RAU COMEX		COMPLETE	1573	60	0111	1465
733		NZU MC109	MC105	ENTROPY	1465	44	0619	0620
734	MC105	RAU S CPR		AND THE	1620	60	9032	0477
735		FMP T		ENTHALPY	1477	39	9003	0080
736		FAD 0048		EQUATIONS	1080	32	0048	0525
737		STU 0048			0525	21	0048	0601
738		SET 9037			0601	27	9037	1256
739		LDR 0037			1256	09	0037	1690
740		SFT 9037			1690	27	9037	1445
741		STR H0001	MC115		1445	29	0987	1740
742	MC109	RAU S CPR			0619	60	9032	0527
743		FAD 0048			0527	32	0048	0575
744		STU 0048			0575	21	0048	0651
745		RAU S CPR			0651	60	9037	1159
746		FMP T			1159	39	9003	0262
747		FAD 0998			0262	32	0998	0625
748		STU 0998	MC115		0625	21	0998	1740
749	1							
750	1			DURING COMPLETION OF SYMMETRIC				
751	1			PORTIONS OF MATRIX FOR GAS				
752	1			PHASE INDXA WILL TRACK THE				
753	1			EQUATION BEING USED INDXR				
754	1			WILL TRACK THE DIAGONAL				
755	1			POSITION AND INDXC WILL TRACK				
756	1			THE CURRENT MOVE OPERATION				
757	1							
758	1			THE PHASE TEST WORD CHECK IS				
759	1			ZERO FOR GAS REFLECTION AND				
760	1			UNITY FOR SOLID REFLECTION				
761	1							
762	MC115	RSU SOLID			1740	61	0158	1363
763		SLT 0004		SET CHECK	1363	35	0004	1673
764		STL CHECK		TO GAS	1673	20	0309	0312
765		AUP LDD			0312	10	1515	1069
766		STU MOVE1		GENERATE	1069	21	9058	0577
767		RSU SYSTM		MOVE1 AND	0577	61	0638	1593
768		AUP STD		MOVE2	1593	10	1496	1051
769		STU MOVE2		ORDERS	1051	21	9059	1209
770		RAU ATM-1		SET INDXB	1209	60	0164	1169
771		NZU	MC151	TO ATM-1	1169	44	1723	0324
772		RSR 8003	MC117	NEGATIVED	1723	83	8003	0282
773	MC117	LDD 8006		SET INDXC	0282	69	8006	1338
774		RAC 8001		TO INDXB	1338	88	8001	1244
775		RSU 8001		INDXA IS	1244	61	8001	1101
776		AUP SOLID		SOLID PLUS	1101	10	0158	1413
777		AUP UNITY		TWO MINUS	1413	10	0104	1259
778		AUP 8001		INDB ALL	1259	10	8001	1067
779		MPY 50		TIMES 50	1067	19	0186	1306
780		RAA 8002			1306	80	8002	1565
781		LDD 8005		GAS	1565	69	8005	0471
782		STD INDXA	MC123		0471	24	9029	0627
783	MC121	LDD 8005		CONDENSED	0450	69	8005	1356
784		STD INDXA			1356	24	9029	0362
785		RSU 8006			0362	61	8006	1219
786		AUP UNITY			1219	10	0104	1309
787		MPY 50			1309	19	0186	1406
788		RAA 8002	MC123		1406	80	8002	0627
789	MC123	SET 9037			0627	27	9037	0332
790		LDR 0037 A			0332	09	2037	1790
791		RAA INDXA			1790	80	9029	1448
792		RAU MOVE1			1448	60	9058	1255
793		ALO MOVE2	8003	REFLECT	1255	15	9059	8003
794	8003	LDD 9046 C	8002	ONE	8003	69	9646	8002
795	8002	STD 0047 A	MC133	EQUATION	8002	24	2047	0500
796	MC133	NZC MC135	MC139	AT A TIME	0500	48	1103	0554
797	MC135	AXC 0001			1103	58	0001	1359
798		SXA 0050	8003		1359	51	0050	8003
799	MC139	AXB 0001			0554	52	0001	0260
800		NZR	MC151		0260	42	1463	0324
801		ALO UNO			1463	15	0416	0521
802		STL MOVE2	MC143		0521	20	9059	0378
803	MC143	RAU CHECK		GAS OR	0378	60	0309	1513
804		NZU MC160	MC117		1513	44	1167	0282
805	MC151	RAU SOLID		ANY SOLIDS	0324	60	0158	1563
806		NZU MC153	MC041	IN SYSTEM	1563	44	1217	0318
807	MC153	RAU CHECK			1217	60	0309	1663
808		NZU MC041	MC159		1663	44	0318	0368
809	MC159	ALO UNITY		SET CHECK	0368	15	0104	1409
810		STL CHECK		TO SOLID	1409	20	0309	0412
811		RSU SOLID			0412	61	0158	1713
812		SLT 0004		GENERATE	1713	35	0004	1773

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R13      STI TEMPO          MOVF1 AND      1773  21 9059 0581
R14      AUP LOD           YOVE2 FOR      0581  10 1515 1269
R15      STI MOVF1         CONDENSED     1269  21 9059 1177
R16      RAI TEMPO        PHASE          1177  60 9059 0335
R17      AID STD          0335  10 1496 1151
R18      STI MOVF2        1151  21 9059 1459
R19      RAI SOLID        1459  60 0159 1763
R20      RSR R003         MC160          NEG SOLID 1763  83 8003 1167
R21      LOD ATV-1        INDEXC IS      1167  69 0164 1767
R22      RSC R001         ATM-1          1267  89 8001 1823
R23      NEGATIVED
R24      RAI SYS+1        INDXA IS      1823  60 0079 1033
R25      MOV 50           SYS+1          1033  19 0186 1456
R26      RAA R002         MC121          TIMES 50 1456  10 8002 0450
R27      AT THIS POINT DECIDE IF
R28      ITERATION WILL BE NEEDED
R29      BY TESTING ON EXPONENT EACH
R30      DELTA MUST BE LESS THAN
R31      SOME SPECIFIED VALUE
R32      MC041 PAR 0052 MC042 EXP TEST 0318 82 0052 0374
R33      ITERATION
R34      MC042 RAI ATOM1 CONTINUED 0374 60 0642 1498
R35      AUP UNITY UNTIL THE 1498 10 0104 1509
R36      RAC R003 MC043 EXPONENT 1509 88 8003 0418
R37      RAI RV000 C OF DELTAS 0418 60 9604 1175
R38      RAC R005 IS FIGHT 1175 32 8006 1305
R39      NZU MC053 LESS THAN 1305 44 1559 0310
R40      NZC MC049 THAT GIVEN 0310 48 1813 0414
R41      SXC 0001 MC043 BY WORD 1813 59 0001 0418
R42      PAR 0054 MC050 IN INDEXP 0418 82 0054 1070
R43      RAA 0000 MC051 1070 80 0000 0276
R44      RAC 0000 MC051 0276 88 0000 0382
R45      RAI P0001 A MC052 0382 60 3599 1153
R46      NZU MC052 1153 44 0557 0308
R47      RAI T0010 C DEL SUR I 0557 60 6669 0424
R48      AXA 0002 0424 50 0002 0130
R49      AXC 0010 0130 58 0010 0336
R50      FAD R006 0336 32 8006 1665
R51      NZU MC053 MC051 1665 44 1559 0382
R52      RAI TESTX CONVERGED 0382 60 1361 1715
R53      NZU MC054 IF ERROR 1715 44 1319 1170
R54      LOD UNITY LESS THAN 1170 69 0104 0607
R55      STD TESTX EXPON 45 0607 24 1361 0464
R56      PAR 0053 MC050 ONCE OR 0464 82 0053 1070
R57      EXPON 46
R58      TWICE
R59      WHEN CONVERGED GO TO MC054
R60      MC054 LOD T SAVE TEMP 1319 69 9003 1225
R61      STD TFF ON DRUM 1225 24 1111 0514
R62      SET 9050 WAS THE 0514 27 9050 1369
R63      LPP TEMP1 ITERATION 1369 08 1048 1201
R64      RAI 9051 DONE WITH 1201 60 9051 1709
R65      FSR T THE RIGHT 1709 33 9003 1389
R66      RMI MC058 THERMAL 1389 46 1242 1693
R67      RAI T DATA 1693 60 9003 1251
R68      FSR 9050 1251 33 9050 0631
R69      RMI MC058 0631 46 1242 0385
R70      ROUTINE TO CHECK ON TRANSITION
R71      FROM GAS TO CONDENSED PHASE
R72      IF POSITION 7 ON THE CONSOLE
R73      IS AN FIGHT CONDENSING
R74      PROGRAM IS PASSED BY
R75      THE PROGRAM ASSUMES THAT BOTH
R76      GAS AND CONDENSED VECTOR ARE
R77      IN STORAGE
R78      LOD R000 0385 69 8000 1541
R79      R07 DONE 1541 97 1294 1546
R80      STL SW1 INITIALIZE 1546 20 1301 0604
R81      RAA 0000 SWITCH SW1 0604 80 0000 0360
R82      RAC 0000 MC201 0360 88 0000 0466
R83      RAI P0001 A ANY MORE 0466 60 3599 1203
R84      NZU MC230 PRODUCTS 1203 44 0657 0358
R85      RAI P0002 A YES IS IT 0657 60 3600 1355
R86      RMI MC227 GASEOUS 1355 46 0408 1759
R87      RAL P0001 A NO 0408 65 3599 1253
R88      SLT 0001 WAS THE 1253 35 0001 1809
R89      NZU MC205 SOLID USED 1809 44 0564 0614
R90      RAL T0008 C YES IS NI 0614 65 6667 0571
R91      RMI MC227 NEGATIVE 0571 46 0474 1759
R92      AUP UNITY YES IGNORE 0474 60 0104 0410
R93      SET 0001 THIS SOLID 0410 30 0001 1317
R94      ALO P0001 A NEXT TIME 1317 15 3599 1303
R95      STL P0001 A 1303 20 3599 1102
R96      RSI UNITY MC219 1102 61 0104 0460

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005	MC205	RAR 0000		NO LOCATE	0564	82	0000	1220
006		RAU P0002 A	MC207	THE GAS	1220	60	3600	1405
007	MC207	AUP P0002 R		PHASE	1405	10	5600	1455
008		NZU	MC211	VECTOR	1455	44	0510	0560
009		SUP 8001			0510	11	8001	1367
010		AXR 0002	MC207		1367	52	0002	1405
011	MC211	RAU 8006		FOUND IT	0560	60	8006	1417
012		MPY FINE			1417	19	1270	1591
013		RAR 8002			1591	82	8002	1549
014	1							
015	1			INDEX C LOCATES SOLID AND				
016	1			INDEX B THE GAS PHASE DATA				
017	1							
018		LDD 8007		STORE	1549	69	8007	1505
019		STD INDXC		INDEX C	1505	24	9030	1411
020		LDD TEE		GET T TWO	1411	69	1111	1064
021		STD T		AND THREE	1064	24	9003	1320
022		SET TWO		FOR CORE	1320	27	9028	1275
023		LRR 80001			1275	08	1247	0250
024		LDD MC215	F/RT		0550	69	1353	1506
025	F/RT	STD LINK		CALCULATES	1506	24	1855	0458
026		SET 9010		F/RT FOR	0458	27	9010	1164
027		LRR T0001 C		SOLID AND	1164	08	6660	1214
028		RAU 1E		GAS	1214	60	9015	0621
029		FDV T			0621	34	9003	0524
030		STU TEM1			0524	21	0428	0981
031		RAU 1D			0981	60	9014	1439
032		FDV TWO			1439	34	9029	1292
033		EMP T			1292	39	9003	1495
034		FAD 1C			1495	32	9013	1325
035		FDV THREE			1325	34	9029	0478
036		EMP T			0478	39	9003	1031
037		FAD 1R			1031	32	9012	1461
038		FDV TWO			1461	34	9028	1264
039		EMP T			1264	39	9003	1467
040		FAD 1E			1467	32	9016	1548
041		FSR TEM1			1548	33	0428	1555
042		STU TEM 1			1555	21	9049	1314
043		RAU ONE			1314	60	1149	1403
044		FSR LNT			1403	33	0002	0429
045		EMP 1A			0429	39	9011	0432
046		FSR TEM 1	LINK		0432	33	9049	1855
047	MC215	STU TEMPO		STORE F/RT	1753	21	9059	1511
048		LDD 8006			1511	69	8006	1517
049		RAC 8001			1517	88	8001	0574
050		LDD MC217	F/RT		0574	69	1227	1506
051	MC217	RSU 8003		CHECK FOR	1227	61	8003	0435
052		FAD TEMPO		CONDENSING	0435	32	9059	1765
053		FSR LNMI			1765	33	9017	1545
054		RMI	MC225		1545	46	1598	1699
055		RAU P0001 A		IT SHOULD	1598	60	3599	1453
056		SLT 0001		HAVE BEEN	1453	35	0001	0610
057		SRT 0001		CONDENSED	0610	30	0001	1567
058		STU P0001 A		FIX IT	1567	21	3599	1152
059		RAU UNITY	MC219		1152	60	0104	0460
060	MC219	AND SYS		MODIFY	0460	10	0018	0624
061		STU SYS		SYS	0624	21	0018	1071
062		LDD UNITY		SET SWITCH	1071	69	0104	1057
063		STD SW1	MC225	SW1	1057	24	1301	1699
064	MC225	RAC INDXC	MC227	ADVANCE TO	1699	88	9030	1759
065	MC227	AXA 0002		THE NEXT	1759	50	0002	1815
066		AXC 0010	MC201	PRODUCT	1815	58	0010	0466
067	MC230	STL TESTX			0358	20	1361	1364
068		RAU SW1		ANY WRONG	1364	60	1301	1705
069		NZU UNPAK	DONE	PRODUCTS	1705	44	0101	1294
070	DONE	LDD S SR		SUMMATIONS	1294	69	9036	0600
071		STD S		CE S/P AND	0600	24	1124	1277
072		LDD S HPT		H/RT ON	1277	69	9034	1183
073		STD H		DRUM	1183	24	1113	0516
074		LDD ATV-1		INDXC IS	0516	69	0164	1667
075		RCC 8001		ATM-1 NEG	1667	39	8001	1074
076		LDD SYS+2		INDXA IS	1074	69	0036	1489
077		RSA 8001		SYS+2 NEG	1489	81	8001	1595
078		SET 9059 C		STORE	1595	27	9659	0650
079		LRR 9099 A		PRESSURE	0650	08	2099	1202
080		SET 9059 C		ROW IN	1202	27	9659	1107
081		SAP 20010 C	MC057	Z REGION	1107	28	7349	1252
082	MC058	STL TESTX	MC059		1242	20	1361	1414
083	1							
084	1			TEST CONSOLE FOR PUNCHING				
085	1			INTERMEDIATE ANSWERS				
086	1							
087	MC053	LDD ITERA	TEST1		1559	69	0462	0566
088	MC057	LDD DERIV	TEST1		1252	69	1755	0566
089	MC059	LDD MC060	TEST1		1414	69	1717	0566
090	MC060	LDD TEE			1717	69	1111	1464
091		STD T	TDATA		1464	24	9003	0034
092	TEST1	STD LINK1			0566	24	1419	0272
093		LDD 8000			0272	69	8000	0528
094		R02 DELS	NEXT1	TEMPORARY	0528	92	1181	1233
095	NEXT1	LDD 8000		PUNCHES	1233	69	8000	1539
096		R03 VARIA	NEXT2	FOR	1539	93	1392	1394

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997 NEXT2 LDD R000          PROGRAM 1394 69 R000 1000
998 R04 MTRIX LINK1        CHECKING 1000 94 1503 1419
999
1000 1          CONSTANTS FOR MATRIX
1001 1          CLEAN UP ROUTINE
1002 LDD LDD R045 C R002          1515 69 9646 8002
1003 STD STD R047 A MC133          1496 24 2047 0500
1004 LMC LMC R001 R000          0416 00 0001 0000
1005 FINE FINE R000 R005          1270 00 0000 0005
1006 1
1007 1
1008 1          ROUTINE FOR CALCULATING THE
1009 1          CORRECTIONS TO THE CURRENT
1010 1          COMPOSITIONS MAY AND THE
1011 1          TEMPERATURE
1012 1
1013 ITER4 PAU SYS+2 NEW00        SOLVE FOR 0462 60 0036 1691
1014 NEW00 LDD NEW01 SOLVE        CORRECTIONS 1691 69 1444 1698
1015 NEW01 LDD SYS+2 LOAD          1444 69 0036 1589
1016 RSR R001 VARIABLES          1589 83 8001 1695
1017 SET M0001 IN                1495 27 9000 1050
1018 LDR R0050 R NEW02 M-REGION 1050 09 4050 1553
1019 1
1020 1          INDXA WILL TRACK THE PRODUCT
1021 1          CODE AND INDC WILL TRACK
1022 1          THE LN NI
1023 1
1024 NEW02 PSA 0002              1553 81 0002 0960
1025 RSC 0010                    0960 89 0010 0616
1026 LDD SOLID                    0616 69 0158 1561
1027 STD COUNT NEW03              1561 24 0152 1805
1028 1
1029 NEW03 LDD ATOM1              1805 69 0642 1745
1030 PAR 0010                      CLEAR 11 1745 82 0010 1351
1031 PAU WIPE9 R003                CORE 1351 60 0654 8003
1032 R003 STL N0001 R NEW04        LOCATIONS 8003 20 9415 1066
1033 NEW04 NZR NEW06 NEW06        FOR ROW 1066 42 1469 1370
1034 SXR 0001 R003                VECTOR 1469 53 0001 8003
1035 WIPE9 STL N0001 R NEW04        0654 20 9415 1066
1036 1
1037 NEW06 AXA 0002              1370 50 0002 0326
1038 AXC 0010                      0326 58 0010 0482
1039 PAL P0001 A                  DO WE HAVE 0482 65 4599 1703
1040 NZF NEW07 NEW18              A PRODUCT 1703 45 1556 1157
1041 SLT 0001                      YES USE 1556 35 0001 1514
1042 NZU NEW06 NEW08              OR BYPASS 1514 44 1370 0468
1043 1
1044 NEW08 PAU P0002 A            TEST FOR 0468 60 3600 1706
1045 PMI NEW20 NEW10              CONDENSED 1706 46 1060 1160
1046 1
1047 NEW10 SRT 0002              GET THE 1160 30 0002 1767
1048 SUP R003                      MOLECULE 1767 11 8003 1375
1049 STD TEMPO                      SUBSCRIPTS 1375 24 9059 1231
1050 SLT 0001                      AND LOCATE 1231 35 0001 1387
1051 ALO 51                        POSITION 1387 15 0166 1171
1052 PAR R003                      TO STORE 1171 82 8003 0180
1053 STL N0001 R                  STORE 0180 20 9415 1388
1054 PAU TEMPO                      SUBSCRIPTS 1388 60 9059 1795
1055 NZU NEW10                      IN CORE 1795 44 1160 1100
1056 LDD SYS+2                      LOAD 1100 69 0036 1689
1057 RAP R001                      OI AND 1689 82 8001 1596
1058 SET N0000 R                  DELTA 1596 27 9414 1401
1059 LDR T0009 C NEW15            ON CORE 1401 09 6668 1221
1060 1
1061 NEW15 SET C0001              ROUTINE 1221 27 9050 0376
1062 LPR C0001 C0001              FOR 0376 08 1020 9050
1063 SXR 0001 C0002              DEL LN PI 1020 53 0001 9051
1064 C0002 PAU M0001 R C0003      1021 60 9400 9052
1065 C0003 FMP N0001 R C0004      1022 39 9415 9053
1066 C0004 FAD N0002 R C0005      1023 32 9416 9054
1067 C0005 STU N0001 R C0006      1024 21 9415 9055
1068 C0006 NZR C0001 C0007        1025 42 9050 9056
1069 C0007 FAD T0008 C C0008      NEW LN NI 1026 32 6667 9057
1070 C0008 STU T0008 C NEW03      FOR GAS 1027 21 6667 1805
1071 1
1072 NEW20 LDD COUNT              NEW NI 1060 69 0152 1756
1073 RSR R001 NEW21              FOR 1756 83 8001 0512
1074 NEW21 PAU D0048 R NEW22      CONDENSED 0512 60 4048 1753
1075 NEW22 FAD T0008 C            1753 32 6667 1743
1076 STU T0008 C                1743 21 6667 1420
1077 PAU COUNT                      DECFASE 1420 60 0152 1207
1078 SUP UNITY                      COUNT 1207 11 0104 1210
1079 STU COUNT NEW06              FOR SOLIDS 1210 21 0152 1370
1080 1
1081 NEW18 PAU D0049 NEW19        NEW LNT 1157 60 0049 1803
1082 NEW19 FAD LNT                1803 32 0002 0479
1083 STU LNT NEW60                0479 21 0002 1806
1084 NEW60 PSU D0048 NEW61        NEW LNA 1806 51 0048 1104
1085 NEW61 FAD LMAAY              1104 32 0001 1327
1086 STU LMAAY                      1327 21 0001 1154
1087 PAU R000                      PUNCH THE 1154 60 8000 1661
1088 PMI DELX UNPAK              CORRECTION 1661 46 1564 0101
1089 1

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1090 1          START NEW ITERATION AT UNPAK
1091 1
1092 1
1093 1          PERFORMANCE PARAMETER ROUTINE
1094 1
1095 1          WHEN ITERATION IS COMPLETED
1096 1          ENTER AT DERIV
1097 1
1098 1  DERIV  RAU SYS+2  D1          SOLVE FOR 1755 60 0036 1741
1099 1  D1      LDD 1LESS REDUC      DLNPI/   1741 69 1494 1748
1100 1  1LESS  RAU SYS+1          DLNT AT   1494 60 0079 1283
1101 1          LDD CP 1          SOLVE      CONSTANT P 1283 69 0386 1698
1102 1  CP 1    LDD SYS+1          LOAD       0386 69 0079 0532
1103 1          PSA 8001          PARTIALS   0532 81 8001 1438
1104 1          PAR 8001          DLNPI/     1438 82 8001 1544
1105 1          SET M0001          DLNT AT   1544 27 9000 1749
1106 1          LDR 00050 A        CONSTANT P 1749 09 2050 1204
1107 1          ON CORE
1108 1
1109 1          SET M0001          ENTHALPY   1204 27 9015 1260
1110 1          LDR M0012 A CP 2    ROW MOVED 1260 09 2998 1451
1111 1          TO CORE
1112 1
1113 1  CP 2    EXP 0001          CALCULATE 1451 53 0001 1257
1114 1          PSI M0001 A        SPECIFIC 1257 61 9400 1166
1115 1          EMP M0001 R        HEAT TIMES 1166 39 9415 1519
1116 1          FAD M0002 R        MOLECULAR 1519 32 9416 1799
1117 1          STU M0001 R        WEIGHT     1799 21 9415 1307
1118 1          NZR CP 2          DIVIDED    1307 42 1451 1711
1119 1          EDV P              BY R       1711 34 1112 0562
1120 1          EDV TFF           0562 34 1111 1761
1121 1          STU COMR          1761 21 1216 1569
1122 1          RAU 00049 -        STORE      1569 60 0049 1254
1123 1          STU LMTP          DLNM/DLNT 1254 21 1123 0426
1124 1          LDD 8000          AT CONST P 0426 69 8000 0582
1125 1          R01              CHANGES   0582 91 0485 1437
1126 1          LDD NOOP          MADE       0485 69 1488 1791
1127 1          STD MC041 UNPAK    NECESSARY 1791 24 0318 0101
1128 1  ONCE   LDD NORM          BY         1150 69 1304 1357
1129 1          STD MC041          EQUATION   1357 24 0318 1271
1130 1          RAU SYS+2          SHIFTING  1271 60 0036 1442
1131 1          LDD              1442 69 1656 1748
1132 1          RAU SYS+1 REDUC    1656 60 0079 1333
1133 1          LDD              1333 69 0436 1748
1134 1          RAU SYS          0436 60 0018 1174
1135 1          LDD DLMP1 SOLVE    1174 69 1377 1698
1136 1  NOOP   NOP 0000          ONCE      1488 00 0000 1150
1137 1  NORM   PAR 0052          MC042     1304 82 0052 0374
1138 1  CP 3    RAU SYS+1          1437 60 0079 1383
1139 1          LDD 2LESS REDUC    1383 69 0486 1748
1140 1
1141 1  2LESS  RAU SYS          0486 60 0018 1224
1142 1          LDD DLMP1 BACK     1224 69 1377 0230
1143 1
1144 1
1145 1          CONSTANTS FOR USE IN PARAMETER
1146 1          CALCULATIONS
1147 1
1148 1  CONS1   14 6960 0652      PSI/ATM   1140 14 6960 0652
1149 1  CONS2   86 4554 0052      1141 86 4554 0052
1150 1  CONS3   10 0000 0054      1142 10 0000 0054
1151 1  CONS4   29 4980 0053      1143 29 4980 0053
1152 1  CONS5   57 0000 0050      1144 57 0000 0050
1153 1  52      00 0000 0052      1145 00 0000 0052
1154 1  R       19 8718 0051      CAL/MOL K 1146 19 8718 0051
1155 1  GC      32 1740 0052      GRAVITY   1147 32 1740 0052
1156 1  ONF     10 0000 0051      1149 10 0000 0051
1157 1
1158 1          SET CORE LOCATIONS EQUIVALENT
1159 1          TO PARAMETERS AND CONSTANTS
1160 1          OF THE F REGION
1161 1
1162 1          EQU PCP M0001 9000
1163 1          EQU TFF M0002
1164 1          EQU P M0003
1165 1          EQU H M0004
1166 1          EQU I M0005
1167 1          EQU M M0006
1168 1          EQU CF M0007
1169 1          EQU EPSIL M0008
1170 1          EQU MACH M0009
1171 1          EQU I VAC M0010
1172 1          EQU CP M0011
1173 1          EQU GAMMA M0012
1174 1          EQU LMPT M0013
1175 1          EQU LMTP M0014
1176 1          EQU S M0015
1177 1          EQU NI M0016
1178 1          EQU NT M0017
1179 1          EQU NFPS M0018
1180 1          EQU NCSTR M0019

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1181 EQU CSTAR M0020
1182 EQU AW M0021
1183 EQU NAW M0022
1184 EQU HSTR M0023
1185 EQU AAY M0024
1186 EQU HC M0025
1187 EQU RECMC M0026
1188 EQU NAWT M0027
1189 EQU AWT M0028
1190 EQU HSTR2 M0029
1191 EQU P1 M0030
1192 EQU CONS1 M0031
1193 EQU CONS2 M0032
1194 EQU CONS3 M0033
1195 EQU CONS4 M0034
1196 EQU CONS5 M0035
1197 EQU 52 M0036
1198 EQU R M0037
1199 EQU GC M0038
1200 EQU IDENT M0039
1201 EQU ONE M0040 9039
1202 1
1203 1 CALCULATE THE PARTIAL DERIV
1204 1 OF THE LOG OF MOLEC WEIGHT
1205 1 WITH RESPECT TO THE LOG OF
1206 1 PRESSURE AT CONSTANT TEMPURTUR
1207 1
1208 DLMPT SET M0001 1377 27 9000 0632
1209 LDB F0001 0632 09 1110 1664
1210 LDD SYS LOAD 1664 69 0018 1321
1211 RSA 8001 DLNPT/DLNA 1321 81 8001 1427
1212 SET M0041 IN CORE 1427 27 9040 0982
1213 LDR D0050 A 0982 09 2050 1354
1214 LDD ATM-1 1354 69 0164 1817
1215 RSA 8001 1817 81 8001 1274
1216 RAB 8001 1274 82 8001 0280
1217 SET M0051 0280 27 9050 0535
1218 LDR Z0010 A LMPT1 BRING AAY 0535 09 3349 1302
1219 RAU M0041 R COLUMN 1302 60 9440 1310
1220 FMP M0051 R TO CORE 1310 39 9450 1714
1221 FAD LMPT 1714 32 9012 1793
1222 STU LMPT 1793 21 9012 1501
1223 NZR LMPT2 1501 42 1404 1407
1224 SXR 0001 LMPT1 1404 53 0001 1302
1225 RAU P LMPT2 1407 60 9002 1266
1226 FDV LMPT 1266 34 9012 1669
1227 FSB ONE 1669 33 9039 1200
1228 STU LMPT 1200 21 9012 1457
1229 1
1230 1 CALCULATE SEVERAL OTHER
1231 1 PARAMETERS
1232 1
1233 RAU AAY CALCULATE 1457 60 9023 1316
1234 FDV P MOLECULAR 1316 34 9002 1719
1235 STU M WEIGHT 1719 21 9005 1477
1236 1
1237 RAU CPMR SPECIFIC 1477 60 1216 1371
1238 FMP R HEAT 1371 39 9036 1324
1239 FDV M CAL/G 1324 34 9005 1527
1240 STU CP 1527 21 9010 0585
1241 1
1242 RAU ONE GAMMA 0585 60 9039 1594
1243 FSR LMTP EQUALS 1594 33 9013 1374
1244 FMP 8003 PARTIAL OF 1374 39 8003 1577
1245 STU TEMPO LN PRESSUR 1577 21 9059 0635
1246 RAU ONE WITH RESP 0635 60 9039 1694
1247 FAD LMPT TO 1694 32 9012 1424
1248 FMP CPMR LN DENSITY 1424 39 1216 1366
1249 FSR TEMPO AT CONSTNT 1366 33 9059 1746
1250 STU TEMPO ENTROPY 1746 21 9059 1454
1251 RAU CPMR 1454 60 1216 1421
1252 FDV TEMPO 1421 34 9059 1474
1253 STU GAMMA 1474 21 9011 1281
1254 1
1255 RAU H CALCULATE 1281 60 9003 1739
1256 FDV AAY ENTHALPY 1739 34 9023 1492
1257 FMP TEE CAL/G 1492 39 9001 1796
1258 FMP R 1796 39 9036 1250
1259 STU H 1250 21 9003 1507
1260 1
1261 RAU S CALCULATE 1507 60 9014 1416
1262 FDV AAY ENTROPY 1416 34 9023 1769
1263 STU TEMPO 1769 21 9059 1677
1264 FMP R 1677 39 9036 0330
1265 STU S 0330 21 9014 1487
1266 1
1267 1 TEST IF COMBUSTION THROAT OR
1268 1 EXIT
1269 1
1270 RAU COMEX 1487 60 0111 1466
1271 NZU TOREX 1466 44 1819 1470
1272 1

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1273          RAU ONE          STORE          1470 60 9039 1727
1274          FDV M            1/MC           1727 34 9005 0380
1275          STU RECMC        0380          21 9025 1537
1276 1
1277          FMP R            CALCULATE       1537 39 9036 1542
1278          FDV CP            N SUB T        1542 34 9010 1798
1279          FMP LMTP         1798          39 9013 1551
1280          RSU 8003         1551          61 8003 1360
1281          STU NT           1360          21 9016 0518
1282 1
1283          LDD H            SAVE HC          0518 69 9003 1524
1284          STD HC           1524          24 9024 0430
1285          LDD TEMPO        0430          69 9059 0536
1286          STD SO/R         0536          24 0003 1557
1287          RSU UNITY        SFT COMEX       1557 61 0104 1410
1288          FIX H            STU COMEX        1410 21 0111 1764
1289          H FIX            STL CSTAR        1764 20 9019 0322
1290 1
1291 1          TEST IF THROAT OR EXIT IS
1292 1          BEING PROCESSED
1293 1
1294 1
1295          TOREX            RMI THROT        1819 46 0372 1574
1296          EXIT            LDD REMAN        1574 69 1777 0480
1297 1
1298 1
1299          EQU TWO          80001
1300 1
1301          THROT            RAU TEE          CALCULATE       0372 60 9001 0529
1302          FDV M            HSTR AS         0529 34 9005 1032
1303          FMP R            H PLUS          1032 39 9036 0985
1304          FDV TWO          VELOCITY        0985 34 1247 1300
1305          STU RT/2M        OF SOUND        1300 21 1504 1707
1306          FMP GAMMA        SQUARED        1707 39 9011 1460
1307          FAD H            OVER TWO       1460 32 9003 1789
1308          STU HSTR         1789          21 9022 1350
1309          FDV HC            THROAT IS      1350 34 9024 1554
1310          FSR FINS         GOOD WHEN      1554 33 1757 1433
1311          NZU              CSTR1           HSTR EQUAL     1433 44 1587 1538
1312 1          HC
1313          RAU GAMMA        THROAT NOT      1587 60 9011 1400
1314          FAD ONE          DONE YET        1400 32 9039 0579
1315          FMP RT/2M        0579          39 1504 1704
1316          STU TEMPO        CALCULATE       1704 21 9059 1811
1317          RAU HC            THE NEXT       1811 60 9024 1520
1318          FSR HSTR         PRESSURE       1520 33 9022 1450
1319          FDV TEMPO        ESTIMATE       1450 34 9059 1754
1320          FAD ONE          FOR THROAT     1754 32 9039 1483
1321          FMP R            1483          39 9002 0586
1322          STU PA           0586          21 0015 0568
1323          RAU PC           0568          60 1109 1814
1324          STL TESTX        1814          20 1361 1516
1325          FDV PA           1516          34 0015 1566
1326          STU R0002        1566          21 1076 0629
1327          STU F0001        UNPAK          STOR PC/PT     0629 21 1110 0101
1328 1
1329 1          START REITERATING WITH THE NEW
1330 1          THROAT PRESSURE ESTIMATE
1331 1
1332 1          CONSTANT FOR TESTING THROAT
1333 1          FOR CONVERGENCE
1334 1
1335          FINS            CO 1000          0053          THROT TEST 1757 00 1000 0053
1336 1
1337 1
1338          CSTR1            LDD CSTR2        SEVRL          1538 69 1592 0480
1339 1
1340          CSTR2            STU NAWT          CALCULATE       1592 21 9026 1500
1341          FAD ONE          C STAR           1500 32 9039 1029
1342          STU NCSTR        EXPONENT         1029 21 9018 1687
1343 1
1344          RAU AW            STORE           1687 60 9020 1550
1345          STD AW            THROAT A/W      1550 24 9027 1807
1346 1
1347          FMP PC           1807          39 1109 1510
1348          FMP GC            CALCULATE       1510 39 9037 1666
1349          FMP CONS1        CSTAR           1666 39 9030 1570
1350          STU CSTAR        1570          21 9019 1827
1351 1
1352          LDD UNITY        SFT COMEX       1827 69 0104 0508
1353          STD COMEX        REMAN           0508 24 0111 1777
1354 1
1355 1
1356 1          SUBROUTINE TO
1357 1          CALCULATE SEVERAL PERFORMANCE
1358 1          PARAMETERS WHICH ARE NEEDED
1359 1          AFTER BOTH THROAT AND EXIT ARE
1360 1          CONVERGED BUT ARE ALSO USED TO
1361 1          OBTAIN SEVERAL SPECIAL THROAT
1362 1          PARAMETERS AFTER THROAT IS
1363 1          CONVERGED
1364 1

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1365	SEVRL	STD LINK1	CALCULATE	0480	24	1419	0422
1366		PAU MC	SPECIFIC	0422	60	9024	1179
1367		FSR H	IMPULSF	1179	33	9003	1560
1368		FDV CONS3		1560	34	9032	1716
1369		LDD IMPUL	SORT	1716	69	1670	1900
1370	IMPUL	FMP CONS4		1670	39	9033	1674
1371		STU I		1674	21	9004	1331
1372	1						
1373		RSU ONE	CALCULATE	1331	61	9039	1692
1374		FDV M	SPECIFIC	1692	34	9005	1700
1375		FAD RECMC	IMPULSE	1700	32	9025	1229
1376		FMP TEE	EXPONENT	1229	39	9001	1182
1377		FMP CONS2		1182	39	9031	1035
1378		FDV I		1035	34	9004	1588
1379		FDV I		1588	34	9004	1742
1380		STU NI		1742	21	9015	1750
1381	1						
1382		PAU TEE	CALCULATE	1750	60	9001	0558
1383		FDV AAY	AREA PER	0558	34	9023	0612
1384		FDV I	UNIT FLOW	0612	34	9004	1766
1385		FMP CONS2	RATE	1766	39	9031	1720
1386		FDV CONS1		1720	34	9030	1724
1387		STU AW		1724	21	9020	1381
1388	1						
1389		PAU R	CALCULATE	1381	60	9036	1792
1390		FDV CP	R OVER	1792	34	9010	1800
1391		FMP RCPMC	CP TIMES	1800	39	9025	1804
1392		STU RCPMC	MC	1804	21	0608	1062
1393	1						
1394		PAU ONE	CALCULATE	1062	60	9039	1770
1395		FDV GAMMA	AREA PER	1770	34	9011	1774
1396		STU TEMPO	UNIT FLOW	1774	21	9059	1431
1397		PAU LMTP	RATE	1431	60	9013	1744
1398		FSR ONE	EXPONENT	1744	33	9039	1824
1399		FMP RCPMC		1824	39	0608	0658
1400		FSR TEMPO		0658	33	9059	1737
1401		FSR NI		1737	33	9015	0618
1402		STU NAW	LINK1	0618	21	9021	1419
1403	1						
1404	1						
1405	1						
1406	1						
1407	1						
1408	1						
1409	1						
1410	REMAN	PAU I	CALCULATE	1777	60	9004	1185
1411		FMP GC	THRUST	1185	39	9037	1688
1412		FDV CSTAR	COEFFICIEN	1688	34	9019	1794
1413		STU CF	C SUB F	1794	21	9006	1701
1414	1						
1415		PAU AW	CALCULATE	1701	60	9020	1660
1416		FDV AWT	AREA RATIO	1660	34	9027	1816
1417		STU EPSIL		1816	21	9007	1425
1418	1						
1419		PAU AW	CALCULATE	1425	60	9020	1533
1420		FMP P	SPEC IMPLS	1533	39	9002	0636
1421		FMP CONS1	ASSUMING	0636	39	9030	1751
1422		FAD I	AMBIENT	1751	32	9004	1481
1423		STU I VAC	PRESS ZERO	1481	21	9009	1801
1424	1						
1425		PAU GAMMA	CALCULATE	1801	60	9011	1710
1426		FMP TEE	MACH	1710	39	9001	1068
1427		FMP CONS2	NUMBER	1068	39	9031	1471
1428		FDV M		1471	34	9005	1475
1429		LDD MACH1	SORT	1475	69	0578	1900
1430	MACH1	STU TEMPO		0578	21	9059	1235
1431		PAU I		1235	60	9004	1352
1432		FDV TEMPO		1352	34	9059	1058
1433		STU MACH		1058	21	9008	1168
1434	1						
1435		PAU ONE	CALCULATE	1168	60	9039	1525
1436		FSR LMTP	TEMPERATUR	1525	33	9013	1108
1437		FDV CPMR	EXPONENT	1108	34	1216	1218
1438		FSR RCPMC	N SUB T	1218	33	0608	1285
1439		STU NT		1285	21	9016	1402
1440	1						
1441		PAU NAW	CALCULATE	1402	60	9021	1760
1442		FSR NAWT	AREA RATIO	1760	33	9026	1452
1443		STU NEPS	EXPONENT	1452	21	9017	0322
1444	1						
1445	1						
1446	1						
1447	1						
1448	1						
1449	1						
1450	1						
1451	PNCH	PAU 8003	SET CARD	0322	60	8003	1279
1452		STL CARDN	NUMBR ZERO	1279	20	1852	1158
1453		SET M0001		1158	27	9000	1268
1454		STB F0001		1268	29	1110	1318
1455		RSA 0005	PUNCHES 2	1318	81	0005	1575
1456		RAR 0004	PERFORMANC	1575	82	0004	1531

1457		LDD IDENT		PARAMETERS	531	69	9038	1787
1458		STD M0011	PUNCH1	ON 4 CARDS	787	24	9010	1502
1459	1							
1460	PUNCH1	NZR	COMP1	EACH CARD	502	42	1208	1258
1461		EXP 0001		HAS 5	208	53	0001	1368
1462		AXA 0005		PARAMETERS	368	50	0005	1675
1463		SFT M0005		PLUS	575	27	9005	0530
1464		LPR F0001 A		IDENTIFI-	430	08	3110	1418
1465		NZA SPEC		CATION AS	418	40	1521	0472
1466		RAL SPEC1	PUNCH2	6TH WORD	1472	65	1775	1329
1467	PUNCH2	LDD PUNCH1	PUNCH		1329	69	1502	1950
1468	1							
1469	SPEC	RAL SPEC2	PUNCH2		1521	65	1775	1329
1470	COMP1	RAA 0000			1258	80	0000	1468
1471		RAR 0000	COMP2		1468	82	0000	1825
1472	1							
1473	COMP2	PSC 0005		CLEAR	1825	89	0005	1581
1474		RAU 0003	COMP3	POSITIONS	1581	60	8003	1552
1475	COMP3	STL M0011 C		FOR	1552	20	9610	1810
1476		AXC 0001		PRODUCTS	1810	58	0001	1518
1477		RMC COMP3		AND CODES	1518	49	1552	0522
1478	1							
1479		PSC 0004	COMP4		1522	89	0004	0628
1480	COMP4	RAU P0001 A		DO WE HAVE	1628	60	3599	1308
1481		NZU	COMP5	A PRODUCT	1308	44	1162	1212
1482	1							
1483		STU M0010 C		LOAD CODE	1162	21	9609	1820
1484		AXC 0001			1820	58	0001	0476
1485	1							
1486		RAU P0002 A		TEST FOR	0476	60	3600	1358
1487		RMI COMP6		CONDENSED	1358	46	1262	1312
1488	1							
1489		RAU T0008 R		CALC PI	1312	60	4667	1571
1490		LDD COMP7	EXP E	FROM LM PI	1571	69	0526	1850
1491	COMP7	STU M0010 C		AND LOAD	0526	21	9609	1583
1492		AXA 0002			1583	50	0002	1702
1493		AXR 0010			1702	52	0010	1408
1494		AXC 0001			1408	58	0001	1568
1495		RMC COMP4	COMP5		1568	49	0628	1212
1496	1							
1497	COMP5	NZA	SPACE		1212	40	1668	1718
1498		RAL SPEC2	COMP6		1668	65	1775	1379
1499	SPACE	RAL SPEC3	COMP6		1718	65	1671	1379
1500	COMP6	LDD	PUNCH	PRODUCTS	1379	69	1232	1950
1501		RAU P0001 A		AND CODES	1232	60	3599	1458
1502		NZU COMP2	FROZ		1458	44	1825	1362
1503	FROZ	LDD UNPAK	PCP 1		1362	69	0101	0637
1504	1							
1505	COMP6	RAU T0008 R	COMP7	COND IS NI	1262	60	4667	0526
1506	1							
1507	1							
1508	1							
1509	1							
1510	SPEC1	07 M0006	0006		1725	07	9005	0006
1511	SPEC2	00 M0006	0006		1775	00	9005	0006
1512	SPEC3	06 M0006	0006		1671	06	9005	0006
1513	1							
1514	1							
1515		EQU PCP	F0001					
1516		EQU TFE	F0002					
1517		EQU P	F0003					
1518		EQU H	F0004					
1519		EQU I	F0005					
1520		EQU M	F0006					
1521		EQU CF	F0007					
1522		EQU EPSIL	F0008					
1523		EQU MACH	F0009					
1524		EQU I VAC	F0010					
1525		EQU CP	F0011					
1526		EQU GAMMA	F0012					
1527		EQU LMPT	F0013					
1528		EQU LMTP	F0014					
1529		EQU S	F0015					
1530		EQU NI	F0016					
1531		EQU NT	F0017					
1532		EQU NEPS	F0018					
1533		EQU NCSTR	F0019					
1534		EQU CSTAR	F0020					
1535		EQU AX	F0021					
1536		EQU NAX	F0022					
1537		EQU HSTR	F0023					
1538		EQU AAY	F0024					
1539		EQU HC	F0025					
1540		EQU RECMC	F0026					
1541		EQU NAMT	F0027					
1542		EQU AMT	F0028					
1543		EQU HSTR2	F0029					
1544		EQU P1	F0030					
1545		EQU CONS1	F0031					
1546		EQU CONS2	F0032					
1547		EQU CONS3	F0033					
1548		EQU CONS4	F0034					

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1549 EQU CONS5 F0035
1550 EQU 52 F0036
1551 EQU P F0037
1552 EQU GC F0038
1553 EQU IDENT F0039
1554 1
1555 1
1556 1
1557 1
1558 1
1559 PCP 1 STD LINK 0637 24 1855 1508
1560 RAL PCPCT ADVANCE 1508 65 0017 1721
1561 ALO UNITY PRESSURE 1721 15 0104 1412
1562 STL PCPCT RATIO 1412 20 0017 1771
1563 1
1564 RAA 8001 1771 80 8001 1028
1565 SLT 0004 1028 35 0004 1752
1566 STL PROR 1752 20 1904 1558
1567 PAU 00000 A 1558 60 3074 1429
1568 STL TESTX 1429 20 1361 1768
1569 STU PCP NEW PC/PF 1768 21 1110 1818
1570 NZU 9999 TEST FOR 1818 44 1821 9999
1571 1 LAST PC/PF
1572 PAU PC 1821 60 1109 0572
1573 EDV PCP 0572 34 1110 1462
1574 STU PC CLER1 1462 21 0015 0622
1575 1
1576 CLER1 RAR 0018 CLEAR 18 0622 82 0018 1178
1577 PAU WIPE7 8003 PARAMETER 1178 60 1681 8003
1578 8003 STL F0001 P CL 1 STORAGES 8003 20 5110 1072
1579 CL 1 SXR 0001 1072 53 0001 1228
1580 NZR 8003 LINK 1228 42 8003 1855
1581 1
1582 1
1583 1
1584 1
1585 UNITY 00 0000 0001 0104 00 0000 0001
1586 WIPE7 STL F0001 P CL 1 1681 20 5110 1072
1587 1
1588 1
1589 1
1590 1
1591 1
1592 SOLVE STD LINK 1698 24 1855 1708
1593 STU EQUAT 1708 21 1512 1172
1594 SUP UNITY 1172 11 0104 1562
1595 NZU OKFH 1562 44 1222 1272
1596 PAU 00049 1272 60 0049 1758
1597 EDV 00048 1758 34 0048 1802
1598 STU 00049 LINK 1802 21 0049 1855
1599 OKFH AUP UNITY START 1222 10 0104 1662
1600 1
1601 1
1602 BACK STD LINK BACK 0230 24 1855 1808
1603 STU NOROW SOLUTION 1808 21 9049 1322
1604 PAU 00049 BACK1 ONLY 1322 60 0049 1712
1605 STU NOROW STORE EQUA 1662 21 9049 1372
1606 STD MINEX NUMBER 1372 24 9045 1278
1607 STL MINCO 1278 20 9046 0986
1608 LDD 8000 MUST EQUA 0986 69 8000 1762
1609 PD1 AGAIN STRT1 RE SHIFTED 1762 91 1422 1472
1610 AGAIN STU VAPRL 1422 21 9048 1479
1611 SUP UNITY 1479 11 0104 1812
1612 PMT SHOVE 1812 46 1522 1572
1613 MPY 50 1572 19 0186 1672
1614 PAR 8002 INDXB 1672 82 8002 1731
1615 SXR NOROW FOLLOWS 1731 53 9049 1722
1616 PAU NOROW EQUATIONS 1722 60 9049 1529
1617 SUP UNITY VARIABLES 1529 11 0104 1772
1618 NZU BACKS 1772 44 0576 0626
1619 PAA 8003 0576 80 8003 0334
1620 PAC 8003 0334 88 8003 1822
1621 SET M0001 BRING EQUA 1822 27 9000 1328
1622 LDR 00049 P TO CORE 1328 09 4049 1176
1623 SET C0001 1176 27 9050 1781
1624 LDR U0001 C0001 1781 09 0050 9050
1625 U0001 PAU M0001 C0002 DIVIDE THE 0050 60 9000 9051
1626 U0002 NZU C0003 LEAVE EQUATION 0051 44 9052 1226
1627 U0003 PAU M0001 A C0004 BY THE 0052 60 9200 9053
1628 U0004 EDV M0001 C0005 LEADING 0053 34 9000 9054
1629 U0005 PAM 8003 C0006 COEFFICIENT 0054 67 8003 9055
1630 U0006 STL M0001 A C0007 0055 20 9200 9056
1631 U0007 SXA 0001 C0008 0056 51 0001 9057
1632 U0008 NZA C0003 C0009 0057 40 9052 9058
1633 U0009 STU MAXCO 0058 21 9047 1326
1634 PAA NOROW TO ZERO 1326 30 9049 0384
1635 SXA 0001 0384 51 0001 1376
1636 SET C0001 1376 27 9050 1831
1637 LDR Y0001 C0001 1831 09 0059 9050
1638 Y0001 PAU MAXCO C0002 SEARCH FOR 0059 60 9047 9051
1639 Y0002 FSR M0001 A C0003 MAXIMUM 0060 33 9200 9052
1640 Y0003 PMT C0004 C0006 COEFFICIENT 0061 46 9053 9055

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1641	Y0004	LDD M0001 A	C0005			0362	69	9200	9054
1642	Y0005	STD MAXCO	C0006			0363	24	9047	9055
1643	Y0006	SXA 0001	C0007			0364	51	0001	9056
1644	Y0007	NZA C0001				0365	40	9050	1426
1645		RSU MINCO			PLACE	1426	61	9046	1683
1646		NZU	BOOK		SMALLEST	1683	44	1738	1788
1647		FAD MAXCO			COEFFICIENT	1738	32	9047	1476
1648		RMI BOOK	LEAVE		IN MINCO	1476	46	1788	1226
1649	BOOK	LDD MAXCO			AND EQUAT	1788	69	9047	1526
1650		STD MINCO			NUMBER IN	1526	24	9046	1282
1651		LDD VARPL			MINEX	1282	69	9048	1576
1652		STD MINEX	LEAVE			1576	24	9045	1226
1653	LEAVE	RAU VARPL			GO TO NEXT	1226	60	9048	1733
1654		SUP UNITY	AGAIN		EQUATION	1733	11	0104	1422
1655	SHOVE	RAU NOROW				1422	60	9049	1579
1656		SUP MINEX				1579	11	9045	1676
1657		NZU	STRTO			1676	44	1679	0580
1658		RAU NOROW				1679	60	9049	1726
1659		SUP UNITY				1726	11	0104	1776
1660		MPY 50				1776	19	0186	1826
1661		RAA 8002				1826	80	8002	1335
1662		RAU MINEX				1335	60	9045	1378
1663		SUP UNITY				1378	11	0104	1428
1664		MPY 50				1428	19	0186	1478
1665		RAR 8002				1478	82	8002	1528
1666		SET M0001			SHIFT THE	1528	27	9000	1783
1667		LDR D0037 A			EQUATIONS	1783	09	2037	1578
1668		LDR D0037 B				1578	09	4037	1678
1669		SET M0001				1678	27	9000	0434
1670		STR D0037 R				0434	29	4037	1728
1671		STR D0037 A	STRTO			1728	29	2037	0580
1672	STRTO	RAU NOROW	STRTO			0580	60	9049	1472
1673	STRTO	SUP UNITY				1472	11	0104	1778
1674		NZE	BACKS			1778	45	1332	0626
1675		MPY 50				1332	19	0186	1828
1676		RAR 8002				1828	82	8002	1729
1677		SXB NOROW				1729	53	9049	1779
1678		SET M0001			TRANSFER	1779	27	9000	0484
1679		LDB D0049 R			EQ TO CORE	0484	09	4049	1829
1680		RAA NOROW	DIV			1829	80	9049	0630
1681	DIV	SET C0001				0630	27	9050	1385
1682		LBB I0001	C0001		DIVIDE	1385	08	1001	9050
1683	I0001	RAU M0001 A	C0002		ELEMENTS	1001	60	9200	9051
1684	I0002	FDV M0001	C0003		OF FIRST	1002	34	9000	9052
1685	I0003	STJ M0001 A	C0004		EQUATION	1003	21	9200	9053
1686	I0004	SXA 0001	C0005		BY LEADING	1004	51	0001	9054
1687	I0005	NZA C0001	NEXTR		COEFFIC	1005	40	9050	1030
1688	1								
1689	NEXTR	SET M0002			AND STORE	1030	27	9001	1435
1690		STR D0050 R			BACK ON	1435	29	4050	1180
1691		SET C0001			DRUM	1180	27	9050	1485
1692		LBB J0001	NEW R			1485	08	1006	1230
1693	1								
1694	NEW R	SXB 0050			ANY MORE	1230	53	0050	1036
1695		AXB NOROW			EQUATIONS	1036	52	9049	1280
1696		BOV OFLO1			CHK OVRFL0	1280	47	0534	1535
1697		BMB OUT 1				1535	43	1330	1380
1698		SXB NOROW			YES	1380	53	9049	1430
1699		SET N0001				1430	27	9015	1585
1700		LDB D0049 R				1585	09	4049	1480
1701		RAA NOROW	ELMIN			1480	80	9049	9050
1702	OFLO1	HLT 0000	9955			0534	01	0000	9955
1703	OUT 1	RAU NOROW			NO	1330	60	9049	1530
1704		SUP UNITY	START			1530	11	0104	1662
1705	J0001	RSU N0001	C0002		ELIMINATE	1006	61	9015	9051
1706	J0002	FMP M0001 A	C0003		A VARIABLE	1007	39	9200	9052
1707	J0003	BOV ZEROU	C0004		CHK OVRFL0	1008	47	1580	9053
1708	J0004	FAD N0001 A	C0005			1009	32	9215	9054
1709	J0005	STU N0001 A	C0006			1010	21	9215	9055
1710	J0006	SXA 0001	C0007			1011	51	0001	9056
1711	J0007	NZA ELMIN				1012	40	9050	1680
1712		SET N0002				1680	27	9016	1685
1713		STR D0050 R	NEW R			1685	29	4050	1230
1714	ZEROU	RAU 8002	C0004		OVERFLOW	1580	60	8002	9053
1715	1								
1716	BACKS	RAU N0003	B1		LEAVES THE	0626	60	9017	0584
1717	R1	FDV N0002			LAST	0584	34	9016	1730
1718		LDD EQUAT			VARIABLE	1730	69	1512	1780
1719	1				IN UPPER				
1720		STD NOROW	BACK1			1780	24	9049	1712
1721	BACK1	RAR 0000				1712	82	0000	1830
1722		RAC 0001				1830	88	0001	1186
1723		SET C0001				1186	27	9050	1382
1724		LBB K0001	S7			1382	08	1013	1432
1725	1								
1726	S7	SXC 0001				1432	59	0001	1482
1727		STU D0049 C			CHK OVRFL0	1482	21	6049	1532
1728		BOV OFLO2				1532	47	1735	1582
1729		RSL 8007				1582	66	8007	1682
1730		RAA 8002				1682	80	8002	1732
1731		AXA 0001				1732	50	0001	1782

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1732      AXR 0049
1733      SXA NOROW
1734      BMA LINK
1735      AXA NOROW
1736      SET M0001
1737      LDR D0049 C
1738      SET M0001
1739      LDR D0049 R S1
1740      OFLO2 HLT 0000 9966
1741      49 49 0000 0000
1742 1
1743 1
1744 1
1745 1
1746 1
1747      K0001 SXA 0001 C0002
1748      K0002 RSU M0001 A C0003
1749      K0003 FMP M0001 A C0004
1750      K0004 ROV ZERUP C0005
1751      K0005 FAD M0002 A C0006
1752      K0006 STU M0001 A C0007
1753      K0007 NZA S1 S7
1754      ZERUP RAU 8002 C0005
1755 1
1756 1
1757 1
1758 1
1759 1
1760      REDUC STD LINK
1761      RSR 8003
1762      RAA 8003
1763      SXA 0001 SHIFT
1764      AXR 0050
1765      SET M0001
1766      LDR D0049 R
1767      SET M0001
1768      STB D0000 R
1769      SXA 0001
1770      NZA SHIFT LINK
1771 1
1772 1
1773 1
1774 1
1775 1
1776 1
1777 1
1778 1
1779 1
1780 1
1781 1
1782 1
1783 1
1784 1
1785 1
1786 1
1787 1
1788 1
1789 1
1790 1
1791 1
1792 1
1793      REG R1951 1960
1794      REG V1599 1659
1795      REG C9000 9000
1796      EQU PCH10 1986
1797      EQU ODIN C0048
1798      EQU OASIS C0049
1799      EQU RELAY C0050
1800 1
1801      8000 RCD R0001 1998
1802      R0001 00 0000 V0001
1803      V0001 SFT C0003 V0002
1804      V0002 LDR V0003 C0003
1805      V0003 PAA 0000 C0004
1806      V0004 PAR 0000 C0005
1807      V0005 PAC 0000 C0006
1808      V0006 SUP 8003 C0007
1809      V0007 STU RELAY C0008
1810      V0008 RCD PCH10 9977
1811      PCH10 NOP 0000 C0009
1812      V0009 RAU R0001 C0010
1813      V0010 NZU C0011 C0042
1814      V0011 RAU R0002 C0012
1815      V0012 NZU C0013 C0008
1816      V0013 RAU R0004 C0014
1817      V0014 RMI C0025 C0015
1818      V0015 SRT 0002 C0016
1819      V0016 NZU C0025 C0017
1820      V0017 SLT 0001 C0018
1821      V0018 SLO ODIN C0019
1822      V0019 PAL 8002 C0020
1782      52 0049 1832
1832      51 9049 0634
0634      41 0984 1855
0984      50 9049 1034
1034      27 9000 1184
1184      09 6049 1234
1234      27 9015 1284
1284      09 4049 9050
1735      01 0000 9966
1334      49 0000 0000
1013      51 0001 9051
1014      61 9200 9052
1015      39 9215 9053
1016      47 13H4 9054
1017      32 9216 9055
1018      21 9215 9056
1019      40 9050 1432
1384      60 8002 9054
1748      24 1855 1434
1434      83 8003 1484
1484      80 8003 1534
1534      51 0001 1584
1584      52 0050 1684
1684      27 9000 1734
1734      09 4049 1784
1784      27 9000 1785
1785      29 4000 1236
1236      51 0001 1286
1286      40 1584 1855
1748      24 1855 1434
1434      83 8003 1484
1484      80 8003 1534
1534      51 0001 1584
1584      52 0050 1684
1684      27 9000 1734
1734      09 4049 1784
1784      27 9000 1785
1785      29 4000 1236
1236      51 0001 1286
1286      40 1584 1855
ROUTINE TO LOAD PACKED VECTORS
AND GENERATE ATOM1 AND SYS THE
PROGRAM DEFINING CONSTANTS
PRECEED PACKED VECTORS WITH
A LOAD HUB TRANSFER CARD WHICH
IS NOP GO TO V0001
FOLLOW PACKED VECTORS WITH A
LOAD HUB CARD WORD1 EQUAL ZERO
THE PROGRAM BYPASSES THE
PROPELLANT IDENTIFICATION CARD
INDEXB TOTALS GASEOUS ATOMS
INDEXC TOTALS CONDENSED PHASES
OASIS SPECIFIES WHICH OF THE
CONDENSED PHASES ARE USED
READ BAND
IN PREGION
WRD 10 PCH
CONSOLE 8000 70 1951 1998
TRANSFER CD 1951 00 0000 1599
1599 27 9002 1600
1600 09 1601 9002
1601 80 0000 9003
1602 82 0000 9004
1603 88 0000 9005
1604 11 8003 9006
1605 21 9049 9007
1606 70 1986 9977
1986 00 0000 9008
1607 60 1951 9009
1608 44 9010 9041
1609 60 1952 9011
1610 44 9012 9007
1611 60 1954 9013
1612 46 9024 9014
1613 30 0002 9015
1614 44 9024 9016
1615 35 0001 9017
1616 16 9047 9018
1617 65 8002 9019

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1823 V0020 NZE C0025 C0021
1824 V0021 AXR 0001 C0022
1825 V0022 RAU RELAY C0023
1826 V0023 NZU C0024 C0037
1827 V0024 HLT 0000 9988
1828 V0025 LDD ODIN C0026
1829 V0026 STD RELAY C0027
1830 V0027 RAU R0004 C0028
1831 V0028 RMI C0029 C0037
1832 V0029 RAU OASIS C0030
1833 V0030 SRT 0001 C0031
1834 V0031 STU OASIS C0032
1835 V0032 RAL 8002 C0033
1836 V0033 NZE C0036 C0034
1837 V0034 RAL R0002 C0035
1838 V0035 AXC 0001 C0038
1839 V0036 ALO R0002 C0038
1840 V0037 RAL R0002 C0038
1841 V0038 STL P0001 A C0039
1842 V0039 LDD R0004 C0040
1843 V0040 STD P0002 A C0041
1844 V0041 AXA 0002 C0008
1845 V0042 RAU 8007 C0043
1846 V0043 STL P0001 A C0044
1847 V0044 LDD 8006 C0045
1848 V0045 STD ATOM1 C0046
1849 V0046 AUP 8001 C0047
1850 V0047 STU SYS CHECK
1618 45 9024 9020
1619 52 0001 9021
1620 60 9049 9022
1621 44 9023 9036
1622 01 0000 9988
1623 69 9047 9025
1624 24 9049 9026
1625 60 1954 9027
1626 46 9028 9036
1627 60 9048 9029
1628 30 0001 9030
1629 21 9048 9031
1630 65 8002 9032
1631 45 9035 9033
1632 65 1952 9034
1633 58 0001 9037
1634 15 1952 9037
1635 65 1952 9037
1636 20 3599 9038
1637 69 1954 9039
1638 24 3600 9040
1639 50 0002 9007
1640 60 8007 9042
1641 20 3599 9043
1642 69 8006 9044
1643 24 0642 9045
1644 10 8001 9046
1645 21 0018 0499

1851 1
1852 1
1853 1
1854 V0048 10 0000 0000 ODIN 1646 10 0000 0000
1855 V0049 11 1111 1111 OASIS 1647 11 1111 1111

1856 1
1857 1
1858 1
1859 1
1860 T0008 10 0000 0040 ESTIMATES 0667 10 0000 0040
1861 T0018 10 0000 0040 FOR LN OF 0677 10 0000 0040
1862 T0028 10 0000 0040 COMPOSITIO 0687 10 0000 0040
1863 T0038 10 0000 0040 EQUIVALENT 0697 10 0000 0040
1864 T0048 10 0000 0040 TO PARTIAL 0707 10 0000 0040
1865 T0058 10 0000 0040 PRESSURES 0717 10 0000 0040
1866 T0068 10 0000 0040 OF I 0727 10 0000 0040
1867 T0078 10 0000 0040 ATMOSPHERE 0737 10 0000 0040
1868 T0088 10 0000 0040 FOR ALL 0747 10 0000 0040
1869 T0098 10 0000 0040 GASEOUS 0757 10 0000 0040
1870 T0108 10 0000 0040 PRODUCTS 0767 10 0000 0040
1871 T0118 10 0000 0040 0777 10 0000 0040
1872 T0128 10 0000 0040 0787 10 0000 0040
1873 T0138 10 0000 0040 0797 10 0000 0040
1874 T0148 10 0000 0040 0807 10 0000 0040
1875 T0158 10 0000 0040 0817 10 0000 0040
1876 T0168 10 0000 0040 0827 10 0000 0040
1877 T0178 10 0000 0040 0837 10 0000 0040
1878 T0188 10 0000 0040 0847 10 0000 0040
1879 T0198 10 0000 0040 0857 10 0000 0040
1880 T0208 10 0000 0040 0867 10 0000 0040
1881 T0218 10 0000 0040 0877 10 0000 0040
1882 T0228 10 0000 0040 0887 10 0000 0040
1883 T0238 10 0000 0040 0897 10 0000 0040
1884 T0248 10 0000 0040 0907 10 0000 0040
1885 T0258 10 0000 0040 0917 10 0000 0040
1886 T0268 10 0000 0040 0927 10 0000 0040
1887 T0278 10 0000 0040 0937 10 0000 0040
1888 T0288 10 0000 0040 0947 10 0000 0040
1889 T0298 10 0000 0040 0957 10 0000 0040
1890 G0001 50 0000 0051 LNA ESTM T 0001 50 0000 0051
1891 G0002 82 4300 0051 LNT ESTM T 0002 82 4300 0051

1892 1
1893 1
1894 1
1895 1
1896 1
1897 1
1898 1
1899 1
1900 1
1901 1

          TO RUN AT CONSTANT ENTHALPY
          AT VARIOUS PRESSURE RATIOS
          LOAD THE FOLLOWING CARD

1898 FIX H STL COMEX H FIX CONST H 1410 20 0111 1764

          TO RUN FROZEN COMPOSITION
          CALCULATIONS LOAD THE
          FOLLOWING CARD

1898 FROZ HLT 9999 9999 1362 01 9999 9999

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1902 1
1903 1      PUNCH ROUTINE FOR TESTING
1904 1      GENERAL ROCKET PERFORMANCE
1905 1      CALCULATION
1906 1
1907 1      PUNCHING IS CONSOLE CONTROLLED
1908 1      BY POSITIONS 2 3 4 AND SIGN
1909 1      THESE POSITIONS MUST BE EITHER
1910 1      EIGHT OR NINE PUNCHING ON 8
1911 1
1912 1      POSITION 2 PUNCHES ONE MINUS
1913 1      P/P0 ETC AND NEGATIVE DELTA I
1914 1
1915 1      POSITION 3 PUNCHES P T AAY
1916 1      AND THE COMPOSITIONS NI
1917 1
1918 1      POSITION 4 PUNCHES THE
1919 1      REDUCED MATRIX
1920 1
1921 1      A MINUS ON CONSOLE PUNCHES
1922 1      CORRECTION VARIABLES
1923 1
1924 1      ANY COMBINATION OF THE FOUR
1925 1      PUNCHES MAY BE USED TOGETHER
1926 1
1927      BLA 1656      1659
1928      BLA 0940      0959
1929 1
1930 1
1931 1      PUNCH THE DELS AT THIS TIME
1932 1
1933      DELS      RAL PCH01      PUNCH ONE      1181      65      1336      0941
1934      ALO ATOM1      MINUS A      0941      15      0642      0947
1935      LDD DELS1      PUNCH      OVER A0      0947      69      0950      1950
1936      DELS1      RAA 0000      ETC      0950      80      0000      0956
1937      RAC 0000      DELS2      0956      88      0000      1386
1938      DELS2      RAU P0001 A      PUNCH THE      1386      60      3599      0953
1939      NZU      DELS3      PRODUCT      0953      44      0957      0958
1940      STU 9000 A      CODES AND      0957      21      3200      1436
1941      LDD T0010 C      THE DELTA I      1436      69      6669      1486
1942      STD 9001 A      1486      24      9201      0942
1943      AXA 0002      0942      50      0002      0948
1944      AXC 0010      DELS2      0948      58      0010      1386
1945      DELS3      RAL 8005      0958      65      8005      1536
1946      ALO PCH02      1536      15      0940      0945
1947      LDD NEXT1      PUNCH      0945      69      1233      1950
1948 1
1949 1
1950 1      PUNCH THE SOLUTION TO THE
1951 1      CURRENT MATRIX
1952 1
1953      DELX      LDD SYS+1      PUNCH THE      1564      69      0079      1586
1954      RSA 8001      SOLUTION      1586      81      8001      0943
1955      SET 9000      TO THE      0943      27      9000      0949
1956      LDB D0049 A      CORRECTION      0949      09      2049      0952
1957      RAL PCH02      MATRIX      0952      65      0940      0946
1958      ALO SYS+2      0946      15      0036      0944
1959      LDD UNPAK      PUNCH      0944      69      0101      1950
1960 1
1961 1      CONSTANTS FOR THE PUNCH
1962 1      ROUTINE
1963 1

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1964	PCH01	06	RV000	0002			
1965	PCH02	06	9000	0000	1336	06	9004 0002
1966	1				0940	06	9000 0000
1967			PAT				

1968		BLA	1652	1655			
1969		BLA	0920	0939			
1970	1						
1971	1						
1972	1						
			PUNCH THE CURRENT VARIABLES				
1973	VARIA	RAU	LNT		PUNCH TEMP	1392	60 0002 1657
1974		LDD	VAR01	EXP E	PRESSURE	1657	69 0920 1850
1975	VAR01	STU	9000		AND AAY	0920	21 9000 0927
1976		LDD	P			0927	69 1112 0921
1977		STD	9001			0921	24 9001 0928
1978		LDD	AAY			0928	69 1133 0936
1979		STD	9002			0936	24 9002 0951
1980		RAL	PCH03			0951	65 0954 0959
1981		LDD	VAR02	PUNCH		0959	69 0922 1950
1982	VAR02	RAA	0000		PUNCH THE	0922	80 0000 0929
1983		RAC	0000	VAR03	PRODUCT	0929	88 0000 0935
1984	VAR03	RAU	P0001 A		CODE AND	0935	60 3599 1653
1985		NZU		VAR11	MOLES OF	1653	44 1658 1659
1986		STD	9000 A		EACH	1658	24 9200 0923
1987		RAU	P0002 A		COMBUSTION	0923	60 3600 0955
1988		BMI	VAR07		PRODUCT	0955	46 0924 0925
1989		RAU	T0008 C			0925	60 6667 0926
1990		LDD	VAR05	EXP E		0926	69 0930 1850
1991	VAR05	STU	9001 A	VAR09		0930	21 9201 0937
1992	VAR07	LDD	T0008 C			0924	69 6667 0931
1993		STD	9001 A	VAR09		0931	24 9201 0937
1994	VAR09	AXA	0002			0937	50 0002 1652
1995		AXC	0010	VAR03		1652	58 0010 0935
1996	VAR11	RAL	PCH02			1659	65 0940 1654
1997		ALO	8005			1654	15 8005 0932
1998		LDD	NEXT2	PUNCH		0932	69 1394 1950
1999	1						
2000	1						
2001	1						
2002	1						
			PUNCH OUT THE MATRIX				
2003	MTRIX	RAU	SYS+1			1503	60 0079 0933
2004		MPY	50			0933	19 0186 1656
2005		RAA	8002	MTR01		1656	80 8002 0934
2006	MTR01	SET	9000			0934	27 9000 0939
2007		LDB	0037 A			0939	09 2037 1655
2008		RAL	PCH04			1655	65 1686 1736
2009		LDD	MTR03	PUNCH		1736	69 1786 1950
2010	MTR03	NZA		LINK1		1786	40 0938 1419
2011		SXA	0050	MTR01		0938	51 0050 0934
2012	1						
2013	1						
2014	1						
2015	1						
2016	1						
			CONSTANTS FOR THE PUNCH ROUTINE				
2017	PCH03	06	9000	0003		0954	06 9000 0003
2018	PCH04	06	9000	0013		1686	06 9000 0013
2019			PAT				

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2020 1          PROGRAM CHANGE TO CONTROL SIZE
2021 1          OF APPLIED CORRECTION
2022 1
2023          PLA 1652      1655
2024          PLA 0920      0939
2025          REG C9050      9050
2026 1          LOAD AVAILABILITY TABLE GIVEN
2027 1          BY CARD NUMBER 1967
2028 1
2029          NEW00  LDD MAG00  SOLVE          1691 69 0951 1698
2030          MAG00  LDD SYS+1          0951 69 0079 0932
2031          RSA 8001          0932 81 8001 0938
2032          RAB 8001          BRING 0938 82 8001 1652
2033          RAC 8001          SOLUTION 1652 88 3001 1658
2034          SET M0001          VECTOR TO 1658 27 9000 0920
2035          LDB D0049 A MAG01          CORE 0920 09 2049 1653
2036          MAG01  RAM M0001 B          MAKE ALL 1653 67 9400 0921
2037          STL N0001 B          COMPONENTS 0921 20 9415 0928
2038          NZB          MAG03          POSITIVE 0928 42 0931 0933
2039          SXR 0001          MAG01          0931 53 0001 1653
2040          MAG03  RAU N0001 C MAG05          FIND THE 0933 60 9615 0954
2041          MAG05  FSR N0000 C          LARGEST 0954 33 9614 0934
2042          BMI          TOP          COMPONENT 0934 46 0937 0939
2043          RAU N0000 C MAG07          0937 60 9614 1654
2044          TOP  FAD N0000 C MAG07          0939 32 9614 1654
2045          MAG07  SXC 0001          IF THE 1654 59 0001 0922
2046          NZC MAG05          COMPONENT 0922 48 0954 0926
2047          FSB MAXMA          IS LARGER 0926 33 0929 0955
2048          BMI          MAG09          THAN MAXMA 0955 46 0959 1659
2049          LDD F0040          STORE THE 0959 69 1149 1655
2050          STD RATIO NEW01          RATIO OF 1655 24 0923 1444
2051          MAG09  FAD MAXMA          COMPONENT 1659 32 0929 1656
2052          FDV MAXMA          TO MAXMA 1656 34 0929 0930
2053          STU RATIO NEW01          0930 21 0923 1444
2054          MAXMA 50 0000 0051          MAX RATIO 0929 50 0000 0051
2055          Q0006  NZB C0001          1025 42 9050 0935
2056          FDV RATIO Q0007          0935 34 0923 1026
2057          NEW21  RAU D0048 B          0512 60 4048 1657
2058          FDV RATIO NEW22          1657 34 0923 1753
2059          NEW18  RAU D0049          1157 60 0049 0924
2060          FDV RATIO NEW19          0924 34 0923 1803
2061          NEW60  RSU D0048          1806 61 0048 0925
2062          FDV RATIO NEW61          0925 34 0923 1104
2063 1
2064 1
2065 1          PROGRAM MAY BE MODIFIED TO
2066 1          CONVERGE FOR ASSIGNED
2067 1          TEMPERATURE AND PRESSURE BY
2068 1          INCLUDING THE FOLLOWING STEPS
2069 1
2070          BLA 0910      0919
2071          BLA 1650      1651
2072 1
2073          MC021  RAU H0/R          0570 60 0004 0910
2074          STL RV001 MC031          0910 20 9005 0286
2075          ITERA  LDD HOLD1          0462 69 0915 0918
2076          STD BACKS          0918 24 0626 0936
2077          RAU SYS+2 NEW00          0936 60 0036 1691
2078          HOLD1  SUP 8003 B1          0915 11 8003 0584
2079          DERIV  LDD HOLD2          1755 69 0911 0914
2080          STD BACKS*          0914 24 0626 1686
2081          RAU SYS+2 D1          1686 60 0036 1741
2082          HOLD2  RAU N0003 B1          0911 60 9017 0584
2083          PAT

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1          INPUT DATA ROUTINE
8 1
9          RLR 0000 0036
10         RLR 0050 0086
11         RLR 0100 0136
12         RLR 0150 0186
13         RLR 0200 0236
14         RLR 0250 0286
15         RLR 0300 0336
16         RLR 0350 0386
17         RLR 0400 0436
18         RLR 0450 0486
19         RLR 0500 1999
20         RLA 0987 0999
21         RLA 1340 1349
22         REG G0001 0015
23         REG I0040 0045
24         REG F1110 1110
25         REG M9000 9000
26         SYN VFPLS 0598 +FUEL VALN
27         SYN VFMIN 0599 -FUEL VALN
28         SYN VXPLS 0548 +OXID VALN
29         SYN VXMIN 0549 -OXID VALN
30         SYN O/F 0199
31         SYN PCT F 0299
32         SYN EQRAT 0399 EQUIVLENC
RATIO
33 1
34         SYN CHEK 0499
35         SYN REGIN 0000
36         SYN PUNCH 1950
37         SYN PC F0000
38         SYN IDENT F0039
39         SYN R F0037
40         SYN TEMPO 9011
41         SYN CONS1 1140
42         SYN PROR 1904
43 1
44 1          CALCULATE NUMBER OF MOLES OF
45 1          OXIDANT PER MOLE OF FUEL
46 1
47 1
48 1          CHECK
49         RAU O/F 0499 60 0199 0037
50         NZU OXFUL 0037 44 0091 0092
51         RAU PCT F 0092 60 0299 0087
52         NZU PRCNT 0087 44 0141 0142
53         RAU EQRAT 0142 60 0399 0137
54         NZU EQUIV 0137 44 0191 0192
55         HLT 9999 9999 0192 01 9999 9999
56 1
57 1          OXFUL
58         RAU O/F 0091 60 0199 0187
59         FAD 10051 0187 32 0090 0237
60         STU TEMPO 0237 21 9011 0095
61         RAU 10053 0095 60 0048 0287
62         FDV TEMPO 0287 34 9011 0140
63         STU PCT F 0140 21 0299 0337
64 1          EQU
65         RAU VXPLS 0337 60 0548 0387
66         FMP O/F 0387 39 0199 0049
67         FAD VFPLS 0049 32 0598 0437
68         STU TEMPO 0437 21 9011 0145
69         RSU VXMIN 0145 61 0549 0487
70         FMP O/F 0487 39 0199 0099
71         FSR VFMIN 0099 33 0599 0987
72         FDV TEMPO 0987 34 9011 0190
73         STU EQRAT 0190 21 0399 0038
74 1
75 1          PRCNT
76         RAU 10053 0141 60 0048 0088
77         FSR PCT F 0088 33 0299 0138
78         FDV PCT F 0138 34 0299 0149
79         STU O/F 0149 21 0199 0337
80 1
81 1          EQUIV
82         RAU VXPLS 0191 60 0548 0188
83         FMP EQRAT 0188 39 0399 0249
84         FAD VXMIN 0249 32 0549 0238
85         STU TEMPO 0238 21 9011 0195
86         RSU VFPLS 0195 61 0598 0288
87         FMP EQRAT 0288 39 0399 0349
88         FSR VFMIN 0349 33 0599 0338
89         FDV TEMPO 0338 34 9011 0241
90         STU O/F 0241 21 0199 0388
91         FAD 10051 0388 32 0090 0438
92         STU TEMPO 0438 21 9011 0245
93         RAU 10053 0245 60 0048 0488
94         FDV TEMPO 0488 34 9011 0291
95         STU PCT F 0291 21 0299 0038
96 1
97 1          ATM 1
98         RAU O/F 0038 60 0199 0988
99         FAD 10051 0988 32 0090 0039
100        STU 1 O/F 0039 21 0094 0047
101        RAB 0010 0047 82 0010 0089
102        RAA 0000 0089 80 0000 0295
103 1
104 1          ATM 2
105         RAU 0537 A 0295 60 2537 0341
106         FMP O/F 0341 39 0199 0449
107         FAD 0587 A 0449 32 2587 0139
108         STU 1 O/F 0139 34 0094 0144
109         STU G0005 A 0144 21 2005 0189
110         SXR 0001 0189 53 0001 0345

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104		NZB		ATM 3		0345	42	0098	0999	
105		AXA	0001	ATM 2		0098	50	0001	0295	
106	1									
107		ATM 3	RAU	0547		CALCULATE	0999	60	0547	0239
108			FMP	O/F		ENTHALPY	0239	39	0199	1349
109			FAD	0597		OVER R	1349	32	0597	0289
110			FDV	1 O/F		PER GRAM	0289	34	0094	0194
111			FDV	R		OF	0194	34	1146	0046
112			STU	G0004	DIST2	PROPELLANT	0046	21	0004	0339
113	1									
114	1									
115	1									
116	1									
117	1									
118		DIST2	RAU	8000			0339	60	8000	0097
119			BD2		IDEN		0097	92	0389	0439
120			RAL	SPEC1			0389	65	0242	0147
121			LDD		PUNCH		0147	69	0489	1950
122			RAL	SPEC2			0489	65	0292	0197
123			LDD	IDEN	PUNCH		0197	69	0439	1950
124	1									
125		IDFN	RAU	EQRAT		EQUIV RATO	0439	60	0399	0989
126			STD	M0006			0989	24	9005	0395
127			UFA	55 I			0395	02	0148	0240
128			SRT	0002			0240	30	0002	0247
129			SLO	8002			0247	16	8002	0290
130			SLT	0006			0290	35	0006	0340
131			AUP	F0039			0340	10	1148	0390
132			STU	M0011		IDNTFICATN	0390	21	9010	0297
133			SLT	0008			0297	35	0008	0440
134			NZU		IDEN2		0440	44	0093	0244
135			RAU	M0011			0093	60	9010	0490
136			STU	F0039	IDEN3		0490	21	1148	0990
137		IDEN2	RAU	F0000			0244	60	1109	1340
138			SRT	0001			1340	30	0001	0347
139			SLO	8002			0347	16	8002	0391
140			STD	TEMPO			0391	24	9011	0397
141			SRT	0008			0397	30	0008	0441
142			SLO	8002			0441	16	8002	0491
143			ALO	TEMPO			0491	15	9011	0991
144			SLT	0001			0991	35	0001	0447
145			AUP	M0011			0447	10	9010	1341
146			STU	M0011			1341	21	9010	0342
147			STD	F0039	IDEN3		0342	24	1148	0990
148		IDEN3	RAU	F0000		CONVERT	0990	60	1109	0392
149			STD	M0009			0392	24	9008	0198
150			FDV	CONS1		CHAM PRESS	0198	34	1140	0442
151			STU	F0000		TO ATMOSP	0442	21	1109	0492
152			LDD	O/F		OXID/FUEL	0492	69	0199	0992
153			STD	M0007		WT RATIO	0492	24	9006	0248
154			LDD	PCT F		PERCENT	0248	69	0299	1342
155			STD	M0008		FUEL BY WT	1342	24	9007	0193
156			RAU	G0004		ENTHALPY	0193	60	0004	0243
157			FMP	R			0243	39	1146	0096
158			STU	M0010			0096	21	9009	0293
159			RAL	SPEC3			0293	65	0146	0343
160			STU	PROB		CLEAR PROB	0343	21	1904	0393
161			LDD		PUNCH		0393	69	0196	1950
162			RAA	0050	IDEN1		0196	80	0050	0443
163		IDEN1	SET	9005			0443	27	9005	0348
164			LBB	0537 A			0348	08	2537	0493
165			RAL	SPEC3			0493	65	0146	0993
166			LDD		PUNCH		0993	69	0246	1950
167			SET	9005			0246	27	9005	1343
168			LBB	0542 A			1343	08	2542	0445
169			RAL	SPEC3			0445	65	0146	0294
170			LDD		PUNCH		0294	69	0497	1950
171			SET	9005			0497	27	9005	0344
172			LBB	0547 A			0344	08	2547	0394
173			RAL	SPEC3			0394	65	0146	0444
174			STU	M0009		CLEAR	0444	21	9008	0494
175			STD	M0010		CLFAR	0494	24	9009	0994
176			LDD		PUNCH		0994	69	0997	1950
177			NZA		BEGIN		0997	40	1344	0000
178			RAA	0000	IDEN1		1344	80	0000	0443
179	1									
180	1									
181	1									
182	1									
183	1									
184			10051	10	0000	0051	0090	10	0000	0051
185			10053	10	0000	0053	0048	10	0000	0053
186			55 I	00	0000	0055	0148	00	0000	0055
187			R	19	8718	0051	1146	19	8718	0051
188			CONS1	14	6960	0652	1140	14	6960	0652
189			SPEC1	00	G0005	0010	0242	00	0005	0010
190			SPEC2	00	G0004	0001	0292	00	0004	0001
191			SPEC3	00	M0006	0006	0146	00	9005	0006
192			SPEC4	00	9005	0006	0495	00	9005	0006
193			PAT							

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1 1      ROCKET PACKAGE EXCERPT FOR
2 1      FOR GENERAL ROCKET PERFORMANCE
3 1
4 1
5      SYN PROB      1904
6      SYN EXP E     1850
7      SYN SORT      1900
8      SYN PUNCH     1950
9      SYN LINK       1855
10     SYN CARDN     1852
11     SYN JOONN     1961
12     REG X1883     1899
13     REG C9050     9050
14     REG R1951     1960      READ BAND
15     REG J1962     1967
16     REG K1968     1973
17     REG P1977     1986
18     REG S1987     1995
19     RLR 0000      1832
20 1
21 1
22 1      EXPONENTIAL
23 1
24     REG X1883     1899      17 WORDS
25 1
26     EXP E      STD LINK      EXPO 7 1850 24 1855 1858
27     FMP EX1     EXB1          NENTIAL 7 858 39 1861 1911
28     43 4294     4850          ENTRY 7 861 43 4294 4850
29     EXR1      SET 9043          911 27 9043 1866
30     SET 9043          72 866 27 9043 1871
31     LDR X0001     72 1871 09 1883 1836
32     STU 9040     72 1836 21 9040 1843
33     FSR 9043     1843 33 9043 1873
34     RMI          EXR2         1873 46 1876 1877
35     FAD 9043     1876 32 9043 1905
36     NZU          EXR61        1905 44 1859 1860
37     FAD 9043     1859 32 9043 1839
38     BMI EXB3     1839 46 1842 1943
39     RAU 9040     EXPONENT72 1943 60 9040 1851
40     RMI          EXB4         MINUS 72 851 46 1854 1856
41     LDD EX2     EXR5          YES 72 854 69 1857 1910
42     X0001      40 0000     0052 72 1883 40 0000 0052
43     EXR2      LDD 8666     EXR3  ALARM 73 877 69 8666 1842
44     EXR3      RAU 8002     LINK  ZERO 73 842 60 8002 1855
45     EXR61     RAU 9040     860 60 9040 1867
46     FDV EX1     867 34 1861 1862
47     FAD 9058     LINK          862 32 9058 1855
48     EXR4      RSU 8003     NO 73 856 61 8003 1863
49     STU 9040     73 863 21 9040 1921
50     LDD EX3     EXB5          73 1921 69 1874 1910
51     EXR5      STD 9041     FIND 74 1910 24 9041 1916
52     FAD HALF     1916 32 1869 1845
53     UFA EXP58     9049     LAMBDA 74 1045 02 1848 9049
54     X0007      STU 9042     74 1689 21 9042 1847
55     FAD 8002     9050       74 1847 32 8002 9050
56     X0008      FAM 9040     74 890 37 9040 1919
57     STU 9040     74 919 21 9040 1927
58     LDD 8005     74 927 69 8005 1833
59     STD 9043     A 74 833 24 9043 1939
60     RSA 0007     74 939 81 0007 1945
61     RAU 8002     9059       74 945 60 8002 9059
62     X0017      FMP 9040     9044 74 899 39 9040 9044
63     X0002      FAD 9258     9045 74 884 32 9258 9045
64     X0003      NZA 9046     9047 885 40 9046 9047
65     X0004      AXA 0001     9059 886 50 0001 9059
66     X0005      FMP 8003     9048 74 887 39 8003 9048
67     X0006      STU 9040     EXR6 74 888 21 9040 1846
68     EXR6      RAA 9043     75 846 80 9043 1906
69     RSU 9042     75 906 61 9042 1913
70     SRT 0002     75 913 30 0002 1870
71     RAU 8003     870 60 8003 1878
72     AUP 9040     75 878 10 9040 1835
73     STU 9040     9041       75 835 21 9040 9041
74     EX2      RAU 9058     75 857 60 9058 1865
75     FDV 9040     LINK       865 34 9040 1855
76     EX3      RAU 8001     LINK 874 60 8001 1855
77     HALF      50 0000     0050 869 50 0000 0050
78     X0009      93 2642     6747 76 891 93 2642 6747
79     X0010      25 5491     8048 76 892 25 5491 8048
80     X0011      17 4211     2049 76 893 17 4211 2049
81     X0012      72 9517     3749 76 894 72 9517 3749
82     X0013      25 4393     5750 76 895 25 4393 5750
83     X0014      66 2730     8850 76 896 66 2730 8850
84     X0015      11 5129     2851 76 897 11 5129 2851
85     X0016      10 0000     0051 76 898 10 0000 0051
86     EXP58      00 0000     0058 1848 00 0000 0058
87 1
88 1
89 1      SQUARE ROOT ROUTINE
90 1
91     REG C9050     9050
92     REG S1987     1995      NINE WORDS
93 1
94     SORT      STD LINK      1900 24 1855 1908
95     RMI STOP     1908 46 1912 1864
96     NZE          LINK       1864 45 1868 1855
97     STU C0000     1868 21 9049 1875
98     SET C0001     1875 27 9050 1880

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99	LRR	S0001				1880	08	1987	1840
100	SRT	0002			CUTOFF EXP	1840	30	0002	1947
101	RAU	8002				1947	60	8002	1907
102	MPY	00050			HALF EXP	1907	19	1914	1834
103	SLP	8002			SAVE DEC	1834	11	8002	1844
104	AUP	1ST E				1844	10	1997	1901
105	ALO	8002	C0001			1901	15	8002	9050
106	S0001	STU	C0010	C0002		1987	21	9059	9051
107	S0002	RAU	C0000	C0003	GET N	1988	60	9049	9052
108	S0003	F0V	C0010	C0004	DIV BY R	1989	34	9059	9053
109	S0004	FAD	C0010	C0005	ADD R TO Q	1990	32	9059	9054
110	S0005	FMP	C0009	C0006	DIV BY 2	1991	39	9058	9055
111	S0006	SUP	C0010	C0007	TEST FOR	1992	11	9059	9056
112	S0007	NZE	C0008		END	1993	45	9057	1948
113		RAU	C0010	LINK		1948	60	9059	1855
114	S0008	AUP	C0010	C0001		1994	10	9059	9050
115	S0009	50	0000	0050	ONE HALF	1995	50	0000	0050
116	1								
117	50	00	0000	0050		1914	00	0000	0050
118	1ST F	70	0000	0025		1997	70	0000	0025
119	STOP	99	9999	9999	SORT NEG X	1912	99	9999	9999
120	1								
121	1								
122	1								
123	1								
124		REG	C9050	9050					
125		SYN	J000N	1961					
126		REG	J1962	1967	SIX WORDS				
127		REG	K1968	1973	SIX WORDS				
128		REG	P1977	1986	PUNCH RAND				
129	1								
130	PUNCH	STD	LINK		START HERE	1950	24	1855	1909
131		LDD	8003			1909	69	8003	1917
132		SDA	C0005		1ST WORD	1917	22	9054	1924
133		SLT	0004			1924	35	0004	1935
134		SDA	C0006		NUMRER WDS	1935	22	9055	1942
135		SRT	0002			1942	30	0002	1849
136		RAU	8003			1849	60	8003	1915
137		SRT	0002			1915	30	0002	1872
138		SET	C0007			1872	27	9056	1928
139		LDD	WDCT6			1928	69	1881	1934
140		STD	P0009			1934	24	1985	1838
141		LDD	PROR			1838	69	1904	1918
142		STD	P0008			1918	24	1984	1837
143		LDD	C0005	PCH3		1837	69	9054	1944
144	PCH3	STD	P0007			1944	24	1983	1936
145		ALO	CARDN			1936	15	1852	1920
146		ALO	ONE D			1920	15	1923	1879
147		SDA	CARDN			1879	22	1852	1922
148		STL	P0010	NZERO		1922	20	1986	1940
149	NZERO	RAU	C0006		IS NO OF	1940	60	9055	1998
150		SLP	WDCT6		WORDS LESS	1998	11	1881	1937
151		RMI	LESS6	PCH4		1937	46	1841	1941
152	PCH4	STU	C0006			1941	21	9055	1949
153		RAU	P0009			1949	60	1985	1946
154		SRT	0004			1946	30	0004	1974
155		AUP	XMOVE		SET TO MOV	1974	10	1929	1933
156		ALO	XLOC		N WORDS	1933	15	1938	1996
157		ALO	C0005	MOVEW		1996	15	9054	1853
158	MOVEW	AUP	09999	8002		1853	10	1925	8002
159	8002	LDD	LOC	8003		8002	69	1999	8003
160	8003	STD	P0007	J000N		8003	24	1983	1961
161	J0000	RAU	C0006	PCH2		1961	60	9055	1975
162	J0001	RAU	C0006	PCH2		1962	60	9055	1975
163	J0002	ALO	ONE D	MOVEW		1963	15	1923	1853
164	J0003	ALO	ONE D	MOVEW		1964	15	1923	1853
165	J0004	ALO	ONE D	MOVEW		1965	15	1923	1853
166	J0005	ALO	ONE D	MOVEW		1966	15	1923	1853
167	J0006	ALO	ONE D	MOVEW		1967	15	1923	1853
168	PCH2	PCH	P0001			1975	71	1977	1930
169		NZE		LINK		1930	45	1902	1855
170		RAU	P0007			1902	60	1983	1903
171		AUP	P0009			1903	10	1985	1926
172		STU	C0005	PCH3		1926	21	9054	1944
173	1								
174	LESS6	RAL	C0006			1841	65	9055	1976
175		STD	P0009			1976	24	1985	1931
176		SRT	0004		CLEAR ZERO	1931	30	0004	1882
177		ALO	XCLER	8002		1882	15	1932	8002
178	8002	00	0000	K0001		8002	00	0000	1968
179	K0001	STU	P0001	K0002		1968	21	1977	1969
180	K0002	STU	P0002	K0003		1969	21	1978	1970
181	K0003	STU	P0003	K0004		1970	21	1979	1971
182	K0004	STU	P0004	K0005		1971	21	1980	1972
183	K0005	STU	P0005	K0006		1972	21	1981	1973
184	K0006	STU	P0006	PCH4		1973	21	1982	1941
185	1								
186	XCLER	00	0000	K0001		1932	00	0000	1968
187	WDCT6	00	0006	0000		1881	00	0006	0000
188	9999	00	0000	9999		1925	00	0000	9999
189	XLOC	LDD	0000	8003		1938	69	0000	8003
190	XMOVE	STD	P0000	J0001		1929	24	1976	1962
191	CARDN	00	0000	0000		1852	20	0000	0000
192	ONE D	00	0001	0000		1923	00	0001	0000
193		PLA	0000	1832					
194		PAT							

APPENDIX G
FROZEN-COMPOSITION PROGRAM

```

1 1      GENERAL FROZEN COMPOSITION
2 1      PERFORMANCE PROGRAM
3 1
4 1
5 1
6 1      THIS PROGRAM ASSUMES THAT
7 1      LN OF COMBUSTION COMPOSITION
8 1      TEMPERATURE PRESSURE ENTHALPY
9 1      MOLECULAR WEIGHT FACTOR A AND
10 1     ALL NECESSARY THERMODYNAMIC
11 1     COEFFICIENTS ARE ALREADY IN
12 1     STORAGE
13 1
14 1
15      SYN LNX      1700
16      SYN EXP E    1850
17      SYN SORT     1900
18      SYN PUNCH    1950
19      SYN PCPCT     0017
20      SYN COMEX     0061
21      SYN START     0500
22      SYN TEMP1     1048
23      SYN TEMP2     1049
24      SYN PC        1109
25      SYN RDB       1193
26      SYN LINK      1855
27      SYN CARDN     1852
28      SYN PROB      1904
29      REG A1347     1349
30      REG B1247     1249
31      REG C9050     9050
32      REG F1110     1149
33      REG G0001     0015
34      REG M9000     9000
35      REG P1599     1659
36      REG R1075     1099
37      REG T0660     0959
38      BLR 1832      1999
39      EQU PCP       F0001
40      EQU TEE       F0002
41      EQU P         F0003
42      EQU H         F0004
43      EQU I         F0005
44      EQU M         F0006
45      EQU CF        F0007
46      EQU EPSIL     F0008
47      EQU MACH      F0009
48      EQU I VAC     F0010
49      EQU CP        F0011
50      EQU GAMMA     F0012
51      EQU S         F0015
52      EQU CSTAR     F0020
53      EQU AW        F0021
54      EQU HSTR      F0023
55      EQU AAY       F0024
56      EQU HC        F0025
57      EQU PLNP      F0026
58      EQU SC        F0027
59      EQU AWT       F0028
60      EQU RA        F0029
61      EQU RM        F0030
62      EQU CONS1     F0031
63      EQU CONS2     F0032
64      EQU CONS3     F0033
65      EQU CONS4     F0034
66      EQU CONS5     F0035
67      EQU R         F0037
68      EQU GC        F0038
69      EQU IDENT     F0039
70      EQU ONE       F0040
71      EQU LNT       G0002
72      EQU PO        G0015
73      EQU S CPR     1347
74      EQU S HRT     1348
75      EQU S SR      1349
76      EQU CODE      9000
77      EQU T         9003
78      EQU A         9021
79      EQU B         9022
80      EQU C         9023
81      EQU D         9024
82      EQU E         9025
83      EQU F         9026
84      EQU NI        9027
85      EQU TWO       9028
86      EQU THREE     9029
87      EQU FOUR      9030
88      EQU TEM 1     9049
89      EQU BASIC     9050
90      EQU TEMPO     9059

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E-417

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91 1
92 START RSM IDENT
93 STL IDENT X1 REVRS SIGN 0500 68 1148 0053
94 1
95 1 CONVERT LNNI TO NI
96 X1 RAA 0000 0051 80 0000 0057
97 RAC 0000 X2 0057 88 0000 0063
98 X2 RAL P0001 A 0063 65 3599 0103
99 NZE X5 0103 45 0056 0107
100 RAU P0002 A 0056 60 3600 0055
101 BMI X3 X4 0055 46 0058 0059
102 X4 RAU T0008 C 0059 60 6667 0021
103 LDD EXP E 0021 69 0024 1850
104 STU T0008 C X3 0024 21 6667 0058
105 X3 AXA 0002 0058 50 0002 0064
106 AXC 0010 X2 0064 58 0010 0063
107 1 CLEAR F REGION
108 X5 SET M0004 0107 27 9003 0062
109 LDB F0004 0062 09 1113 0016
110 RSA 0026 0016 81 0026 0022
111 RAU 8003 X6 0022 60 8003 0029
112 X6 STL F0030 A 0029 20 3139 0042
113 NZA X7 0042 40 0045 0046
114 AXA 0001 X6 0045 50 0001 0029
115 1
116 1 SAVE TEE HC M AND AAY
117 1 OF COMBUSTION
118 X7 LDD M0024 AAY 0046 69 9023 0052
119 STD F0024 0052 24 1133 0036
120 LDD M0025 HC 0036 69 9024 0092
121 STD F0025 0092 24 1134 0037
122 LDD TEE 0037 69 1111 0114
123 STD T 0114 24 9003 0020
124 LDD M0006 M 0020 69 9005 0026
125 STD F0006 0026 24 1115 0018
126 1
127 1 COMPUTE R/AAY AND STORE IN RA
128 RAU R 0018 60 1146 0101
129 FDV AAY 0101 34 1133 0033
130 STU RA 0033 21 1138 0041
131 1
132 1 COMPUTE R/M AND STORE IN RM
133 RAU R 0041 60 1146 0151
134 FDV M 0151 34 1115 0065
135 STU RM 0065 21 1139 0142
136 RAU 8003 0142 60 8003 0049
137 STL COMEX 0049 20 0061 0164
138 1
139 1 FOR COMBUSTION OUT IS Z1
140 LDD Z1 0164 69 0067 0070
141 STD OUT Y1 0070 24 0023 0076
142 1
143 1 LOOP TO COMPUTE
144 1 SUM NI CPR
145 1 SUM NI HRT
146 1 SUM NI SR
147 1
148 1 LOOP IS COMPLETED WHEN ZERO
149 1 APPEARS IN P REGION
150 1 THEN GO TO OUT
151 1 OUT FOR COMB IS Z1
152 1 OUT FOR THROAT AND EXIT IS
153 1 FROZN
154 1
155 Y1 RAU 8003 0076 60 8003 0083
156 STL S CPR 0083 20 1347 0000
157 STL S HRT CLER S CPR 0000 20 1348 0201
158 STL S SR CLER S HRT 0201 20 1349 0102
159 RAA 0000 0102 80 0000 0108
160 RAC 0000 Y2 0108 88 0000 0214
161 Y2 RAL P0001 A 0214 65 3599 0153
162 NZE OUT 0153 45 0106 0023
163 STL CODE THERM 0106 20 9000 0264
164 THERM SET 9020 0264 27 9020 0019
165 LBB T0001 C 0019 08 6660 0113
166 RAU 9020 0113 60 9020 0071
167 SUP CODE 0071 11 9000 0079
168 NZU TH009 0079 44 0133 0034
169 HLT 0000 8866 0133 01 0000 8866

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170	TH009	SET TWO	0034	27	9028	0039
171		LDB R0001	0039	09	1247	0050
172		RAU D	0050	60	9024	0157
173		FMP T	0157	39	9003	0060
174		FAD C	0060	32	9023	0089
175		FMP T	0089	39	9003	0192
176		FAD B	0192	32	9022	0121
177		FMP T	0121	39	9003	0074
178		FAD A	0074	32	9021	0203
179		FMP NI	0203	39	9027	0156
180		FAD S CPR	0156	32	1347	0073
181		STU S CPR	0073	21	1347	0100
182		RAU D	0100	60	9024	0207
183		FDV FOUR	0207	34	9030	0110
184		FMP T	0110	39	9003	0163
185		STU TEMPO	0163	21	9059	0171
186		RAU C	0171	60	9023	0129
187		FDV THREE	0129	34	9029	0032
188		FAD TEMPO	0032	32	9059	0111
189		FMP T	0111	39	9003	0314
190		STU TEMPO	0314	21	9059	0221
191		RAU B	0221	60	9022	0179
192		FDV TWO	0179	34	9028	0082
193		FAD TEMPO	0082	32	9059	0161
194		FMP T	0161	39	9003	0364
195		STU TEMPO	0364	21	9059	0271
196		RAU E	0271	60	9025	0229
197		FDV T	0229	34	9003	0132
198		FAD TEMPO	0132	32	9059	0211
199		FAD A	0211	32	9021	0091
200		FMP NI	0091	39	9027	0044
201		FAD S HRT	0044	32	1348	0025
202		STU S HRT	0025	21	1348	0251
203		RAU D	0251	60	9024	0109
204		FDV THREE	0109	34	9029	0112
205		FMP T	0112	39	9003	0115
206		STU TEMPO	0115	21	9059	0123
207		RAU C	0123	60	9023	0031
208		FDV TWO	0031	34	9028	0084
209		FAD TEMPO	0084	32	9059	0213
210		FMP T	0213	39	9003	0066
211		FAD B	0066	32	9022	0095
212		FMP T	0095	39	9003	0048
213		STU TEMPO	0048	21	9059	0105
214		RAU A	0105	60	9021	0263
215		FMP LNT	0263	39	0002	0152
216		FAD TEMPO	0152	32	9059	0081
217		FAD F	0081	32	9026	0261
218		FMP NI	0261	39	9027	0414
219		FAD S SR	0414	32	1349	0075
220		STU S SR	0075	21	1349	0202
221		AXA 0002	0202	50	0002	0158
222		AXC 0010 Y2	0158	58	0010	0214
223	1					
224	1	TEST FOR CONVERGENCE				
225	1	IS DEL S ZERO				
226	1					
227	1	YES MEANS CONVERGENCE				
228	1	GO TO B THER				
229	1					
230	1	NO MEANS NO CONVERGENCE				
231	1	CORRECT T AND THEN GO TO Y1				
232	1					
233	FROZN	RAU PLNP	0150	60	1135	0139
234		FAD S SR	0139	32	1349	0125
235		STU TEM 1	0125	21	9049	0183
236		FDV SC	0183	34	1136	0086
237		FSB EINSS	0086	33	0189	0165
238		NZU B THER	0165	44	0069	0120
239		RSU TEM 1	0069	61	9049	0027
240		FAD SC	0027	32	1136	0313
241		FDV S CPR	0313	34	1347	0047
242		FAD LNT	0047	32	0002	0279
243		STU LNT	0279	21	0002	0155
244		LDD EXP E	0155	69	0208	1850
245		STU T	0208	21	9003	0215
246		LDD FROZN	0215	69	0150	0253
247		STD OUT Y1	0253	24	0023	0076


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248 1
249 1      AFTER CONVERGENCE TEST IF
250 1      CORRECT TDATA IS IN STORAGE
251 1      YES GO TO FIX
252 1      NO GO TO TDATA
253 1
254      BOTHER SET 9050      0120 27 9050 0175
255      LBB TEMP1      0175 08 1048 0301
256      RAU 9051      0301 60 9051 0159
257      FSB T      0159 33 9003 0239
258      BMI TDATA      0239 46 0242 0043
259      RAU T      0043 60 9003 0351
260      FSB 9050      0351 33 9050 0131
261      BMI TDATA FIX      0131 46 0242 0035
262 1
263 1      READ THERMAL DATA
264 1      WHEN CORRECT TDATA IS FOUND
265 1      GO TO Y1
266      TDATA RAA 0000      0242 80 0000 0098
267      RAC 0000 TD001      0098 88 0000 0054
268      TD001 RCD BASIC BELL      0054 70 9050 0104
269      BASIC RAL 9051 RDB      9050 65 9051 1193
270      RDB SLT 0004      1193 35 0004 0303
271      STU 9051      0303 21 9051 0311
272      SUP P0001 A      0311 11 3599 0353
273      NZU TD005      0353 44 0257 0258
274      LDD T0008 C      0258 69 6667 0170
275      STD 9058      0170 24 9058 0126
276      SET 9051      0126 27 9051 0181
277      SBB T0001 C      0181 28 6460 0363
278      AXA 0002      0363 50 0002 0119
279      AXC 0010 TD001      0119 58 0010 0054
280      TD005 HLT 0000 7766      0257 01 0000 7766
281      BELL RAU 9051      0104 60 9051 0361
282      FSB T      0361 33 9003 0141
283      BMI TDATA      0141 46 0242 0145
284      RAU T      0145 60 9003 0403
285      FSB 9050      0403 33 9050 0233
286      BMI TDATA      0233 46 0242 0087
287      SET 9050      0087 27 9050 0292
288      SBB TEMP1 Y1      0292 28 1048 0076
289 1
290      FIX LDD T      0035 69 9003 0191
291      STD TEE      0191 24 1111 0464
292      LDD PO      0464 69 0015 0068
293      STD P Z1      0068 24 1112 0067
294 1
295      EQU PCP M0001
296      EQU TEE M0002
297      EQU P M0003
298      EQU H M0004
299      EQU I M0005
300      EQU M M0006
301      EQU CF M0007
302      EQU EPSIL M0008
303      EQU MACH M0009
304      EQU I VAC M0010
305      EQU CP M0011
306      EQU GAMMA M0012
307      EQU S M0015
308      EQU CSTAR M0020
309      EQU AW M0021
310      EQU HSTR M0023
311      EQU AAY M0024
312      EQU HC M0025
313      EQU PLNP M0026
314      EQU SC M0027
315      EQU AWT M0028
316      EQU RA M0029
317      EQU RM M0030
318      EQU CONS1 M0031
319      EQU CONS2 M0032
320      EQU CONS3 M0033
321      EQU CONS4 M0034
322      EQU CONS5 M0035
323      EQU R M0037
324      EQU GC M0038
325      EQU IDENT M0039
326      EQU ONE M0040
327 1

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328 1
329 1      CALCULATE ROCKET PERFORMANCE
330 1      PARAMETERS
331 1
332 21      SET M0001      0067 27 9000 0072
333      LDB F0001      0072 09 1110 0413
334 1
335 1      COMPUTE CP
336      RAU S CPR      0413 60 1347 0401
337      FMP RA      0401 39 9028 0154
338      STU CP      0154 21 9010 0411
339 1
340 1      COMPUTE GAMMA
341      FSB RM      0411 33 9029 0241
342      STU TEM 1      0241 21 9049 0099
343      RAU CP      0099 60 9010 0307
344      FDV TEM 1      0307 34 9049 0160
345      STU GAMMA      0160 21 9011 0117
346 1
347 1      COMPUTE ENTHALPY
348      RAU S HRT      0117 60 1348 0453
349      FMP TEE      0453 39 9001 0206
350      FMP RA      0206 39 9028 0209
351      STU H      0209 21 9003 0167
352 1
353 1      TEST COMEX
354 1      ZERO MEANS COMBUSTION
355 1      NONZERO MEANS THROAT OR EXIT
356 1
357      RAU COMEX      0167 60 0061 0265
358      NZU TOREX      0265 44 0169 0220
359 1
360 1      COMPUTE PSEUDO ENTROPY FOR
361 1      COMBUSTION
362      RAU S SR      0220 60 1349 0503
363      STU SC      0503 21 9026 0461
364      FMP RA      0461 39 9028 0514
365      STU S      0514 21 9014 0321
366      RSU UNITY      0321 61 0124 0329
367      STU COMEX      PNCH      SET COMEX      FOR THROAT
368 1
369 1      COMPUTE PSEUDO ENTROPY FOR
370 1      THROAT AND EXIT
371 TOREX      RAU S SR      0169 60 1349 0553
372      FAD PLNP      0553 32 9025 0283
373      FMP RA      0283 39 9028 0136
374      STU S      0136 21 9014 0093
375      RAU COMEX      0093 60 0061 0315
376      BMI THROT      0315 46 0118 0219
377      EQU TWO      EXIT      B0001
378 1
379 1      CONVERGENCE TEST FOR THROAT
380 1      IS HC EQUAL TO HSTR
381 1      IF YES GO TO CSTR1
382 1      IF NO THEN CORRECT P AND GO
383 1      TO FROZN
384 1
385 THROT      RAU TEE      0118 60 9001 0225
386      FDV M      0225 34 9005 0028
387      FMP R      0028 39 9036 0231
388      FDV TWO      0231 34 1247 0097
389      STU RT/2M      0097 21 0252 0205
390      FMP GAMMA      0205 39 9011 0308
391      FAD H      0308 32 9003 0137
392      STU HSTR      0137 21 9022 0195
393      FDV HC      0195 34 9024 0148
394      FSB EINS      0148 33 0451 0077
395      NZU      CSTR1      0077 44 0281 0182
396      RAU GAMMA      0281 60 9011 0289
397      FAD ONE      0289 32 9039 0269
398      FMP RT/2M      0269 39 0252 0302
399      STU TEMPO      0302 21 9059 0259
400      RAU HC      0259 60 9024 0217
401      FSB HSTR      0217 33 9022 0147
402      FDV TEMPO      0147 34 9059 0200
403      FAD ONE      0200 32 9039 0379
404      FMP P      0379 39 9002 0232
405      STU PO      0232 21 0015 0168
406      RAU PC      0168 60 1109 0463
407      FDV PO      0463 34 0015 0365
408      STU R0002      0365 21 1076 0429
409      STU F0001      0429 21 1110 0513
410      LDD      LNX      0513 69 0116 1700
411      FMP PC      0116 39 1109 0309
412      STU F0026      FROZN      0309 21 1135 0150
413      LDD CSTR2      SEVRL      0182 69 0085 0038
414 1

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415 1      STORE A/W FOR THROAT
416 CSTR2  RAU AW
417      STD AWT
418 1
419 1      COMPUTE CSTAR
420      FMP PC
421      FMP GC
422      FMP CONS1
423      STU CSTAR
424      LDD UNITY
425      STD COMEX      REMAN      SET COMEX
426 1      FOR EXIT
427 EXIT    LDD REMAN      SEVRL
428 1
429 1      COMPUTE THRUST COEFFICIENT CF
430 REMAN   RAU I
431      FMP GC
432      FDV CSTAR
433      STU CF
434 1
435 1      COMPUTE AREA RATIO
436      RAU AW
437      FDV AWT
438      STU EPSIL
439 1
440 1      COMPUTE SP IMP IN VACUUM IVAC
441      RAU AW
442      FMP P
443      FMP CONS1
444      FAD I
445      STU I VAC
446 1
447 1      COMPUTE MACH NUMBER
448      RAU GAMMA
449      FMP TEE
450      FMP CONS2
451      FDV M
452      LDD MACH1      SORT
453 MACH1   STU TEMPO
454      RAU I
455      FDV TEMPO
456      STU MACH      PNCH
457 SEVRL   STD LINK1
458 1
459 1      COMPUTE SPECIFIC IMPULSE I
460      RAU HC
461      FSB H
462      FDV CONS3
463      LDD IMPUL      SORT
464 IMPUL   FMP CONS4
465      STU I
466 1
467 1      COMPUTE A/W
468      RAU TEE
469      FDV P
470      FDV M
471      FDV I
472      FMP CONS2
473      FDV CONS1
474      STU AW      LINK1
475 1
476 1      PUNCH RESULTS THEN GO TO PCP 1
477 PNCH    RAU 8003
478      STL CARDN
479      SET M0001
480      STB F0001
481      RSA 0005
482      RAB 0004
483      LDD IDENT
484      STD M0011      PNCH1
485 PNCH1   NZB      PCP 1
486      SXB 0001
487      AXA 0005
488      SET M0006
489      LBB F0001 A
490      NZA SPEC
491      RAL SPEC1      PNCH2
492 PNCH2   LDD PNCH1      PUNCH
493 SPEC    RAL SPEC2      PNCH2
494 COMP1   LDD FROZN      PCP 1
495 1

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0085	60	9020	0143
0143	24	9027	0149
0149	39	1109	0359
0359	39	9037	0162
0162	39	9030	0415
0415	21	9019	0173
0173	69	0124	0127
0127	24	0061	0614
0219	69	0614	0038
0614	60	9004	0371
0371	39	9037	0174
0174	34	9019	0177
0177	21	9006	0135
0135	60	9020	0193
0193	34	9027	0096
0096	21	9007	0603
0603	60	9020	0511
0511	39	9002	0964
0964	39	9030	0267
0267	32	9004	0197
0197	21	9009	0255
0255	60	9011	0563
0563	39	9001	0166
0166	39	9031	0319
0319	34	9005	0122
0122	69	0275	1900
0275	21	9059	0333
0333	60	9004	0291
0291	34	9059	0094
0094	21	9008	0564
0038	24	0341	0144
0144	60	9024	0501
0501	33	9003	0331
0331	34	9032	0134
0134	69	0187	1900
0187	39	9033	0040
0040	21	9004	0247
0247	60	9001	0305
0305	34	9002	0358
0358	34	9005	0561
0561	34	9004	1014
1014	39	9031	0317
0317	34	9030	0270
0270	21	9020	0341
0564	60	8003	0421
0421	20	1852	0355
0355	27	9000	0210
0210	29	1110	0613
0613	81	0005	0369
0369	82	0004	0325
0325	69	9038	0381
0381	24	9010	0237
0237	42	0090	0391
0090	53	0001	0146
0146	50	0005	0352
0352	27	9005	0357
0357	08	3110	0963
0963	40	0216	0367
0367	65	0320	0375
0375	69	0237	1950
0216	65	0419	0375
0250	69	0150	0391

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496 1
497 EQU PCP F0001
498 EQU TEE F0002
499 EQU P F0003
500 EQU H F0004
501 EQU I F0005
502 EQU M F0006
503 EQU CF F0007
504 EQU EPSIL F0008
505 EQU MACH F0009
506 EQU I VAC F0010
507 EQU CP F0011
508 EQU GAMMA F0012
509 EQU S F0015
510 EQU CSTAR F0020
511 EQU AW F0021
512 EQU HSTR F0023
513 EQU AAY F0024
514 EQU HC F0025
515 EQU PLNP F0026
516 EQU SC F0027
517 EQU AWT F0028
518 EQU RA F0029
519 EQU RM F0030
520 EQU CONS1 F0031
521 EQU CONS2 F0032
522 EQU CONS3 F0033
523 EQU CONS4 F0034
524 EQU CONS5 F0035
525 EQU R F0037
526 EQU GC F0038
527 EQU IDENT F0039
528 EQU ONE F0040

529 1
530 1 ADVANCE PRESSURE RATIO PCP
531 1 COMPUTE PC LN PC/PE
532 1 AND STORE IN PLNP
533 1

534 PCP 1 RAL PCPCT 0391 65 0017 0471
535 ALO UNITY 0471 15 0124 0479
536 STL PCPCT 0479 20 0017 0370
537 RAA 8001 0370 80 8001 0176
538 SLT 0004 0176 35 0004 0287
539 STL PROB 0287 20 1904 0407
540 RAU R0000 A 0407 60 3074 0529
541 STU PCP 0529 21 1110 1013
542 NZU 9999 FINISHED 1013 44 0417 9999
543 LDD LNX 0417 69 0420 1700
544 FMP PC 0420 39 1109 0409
545 STU PLNP 0409 21 1135 0088
546 RAU PC 0088 60 1109 1063
547 FDV PCP 1063 34 1110 0260
548 STU PO FROZN 0260 21 0015 0150

549 1
550 1 CONSTANTS FOR PROGRAM
551 ONE 10 0000 0051 1149 10 0000 0051
552 B0001 20 0000 0051 1247 20 0000 0051
553 B0002 30 0000 0051 1248 30 0000 0051
554 B0003 40 0000 0051 1249 40 0000 0051
555 CONS1 14 6960 0652 1140 14 6960 0652
556 CONS2 86 4554 0052 1141 86 4554 0052
557 CONS3 10 0000 0054 1142 10 0000 0054
558 CONS4 29 4980 0053 1143 29 4980 0053
559 CONS5 57 0000 0050 1144 57 0000 0050
560 R 19 8718 0051 1146 19 8718 0051
561 GC 32 1740 0052 1147 32 1740 0052
562 EINS 00 1000 0053 0451 00 1000 0053
563 EINSS 01 0000 0052 0189 01 0000 0052
564 UNITY 00 0000 0001 0124 00 0000 0001
565 SPEC1 07 M0006 0006 0320 07 9005 0006
566 SPEC2 00 M0006 0006 0419 00 9005 0006

567 1

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```

568 1
569 1
570 1      LNX ROUTINE EXCERPT FROM
571 1      THE ROCKET PACKAGE
572 1
573
574 1      REG C9050      9050
575      LNX      STD LINK
576      LDD OP1
577      STD C0005
578      NZU      HLT
579      BMI HLT
580      SRT 0002
581      ALO EXP52      EXPON IN
582      STL C0001      LO PUT IN
583      SLO 8001      FLT NOTATN
584      ALO 51EXP      CLEAR LO
585      SLT 0002      NUM IN UPR
586      STU C0002      ADD 51 EXP
587      RAU C0001      SUB 51 FRM
588      FSB 51LNK      EXPONENT
589      FMP LN10      MUL LN 10
590      FAD LN3      ADD LN 3
591      STU C0001
592      RAU C0002
593      FAD K
594      STU C0003      X MINUS 3
595      RAU C0002      OVER
596      FSB K      X PLUS 3
597      FDV C0003      EQUALS Y
598      FAD 8003      FORM 2Y
599      ALO 8001      Y IN LOWER
600      STU C0003      2Y IN 9003
601      RSU 8002      MINUS Y IN
602      FMP 8001      Y SQUARED
603      STU C0002
604      FMP K1
605      FAD K2
606      FMP C0002
607      FAD K3
608      FMP C0002      FORM
609      FAD K4      NUMERATOR
610      STU C0004
611      RAU C0002
612      FMP K5
613      FAD K6
614      FMP C0002
615      FAD K7
616      FMP C0002      FORM
617      FAD K4      DENOMNATOR
618      FDV C0004
619      FMP C0003      QUOTIENT
620      FAD C0001      MULT BY 2Y
621      FMP C0005      LINK
622      HLT      HLT 1111      1111
623 1
624 1      LN X ROUTINE CONSTANTS
625      EXP52      00 0000      0052
626      51EXP      51 0000      0000
627      51LNK      51 0000      0052
628      K      30 0000      0051
629      LN10      23 0258      5151
630      LN3      10 9861      2351
631      OP1      10 0000      0051
632      K1      81 5850      8249
633      K2      73 4265      7350
634      K3      16 1538      4651
635      K4      99 9999      9950
636      K5      17 0496      1749
637      K6      39 5804      2050
638      K7      12 8205      1351

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1700	24	1355	0408
0408	69	0611	1064
1064	24	9054	0470
0470	44	0223	0224
0223	46	0224	0227
0227	30	0002	0383
0383	15	0186	0441
0441	20	9050	0198
0198	16	8001	0405
0405	15	0458	1163
1163	35	0002	0469
0469	21	9051	0277
0277	60	9050	0185
0185	33	0138	0465
0465	39	0218	0268
0268	32	0521	0297
0297	21	9050	0455
0455	60	9051	1213
1213	32	0266	0243
0243	21	9052	0551
0551	60	9051	0459
0459	33	0266	0293
0293	34	9052	0196
0196	32	8003	0425
0425	15	8001	0433
0433	21	9052	0491
0491	61	8002	0199
0199	39	8001	0402
0402	21	9051	0509
0509	39	0212	0262
0262	32	0515	0541
0541	39	9051	0194
0194	32	0347	0273
0273	39	9051	0226
0226	32	0579	0505
0505	21	9053	1263
1263	60	9051	0571
0571	39	0274	0324
0324	32	0327	0653
0653	39	9051	0256
0256	32	0559	0235
0235	39	9051	0188
0188	32	0579	0555
0555	34	9053	0508
0508	39	9052	0961
0961	32	9050	0591
0591	39	9054	1855
0224	01	1111	1111

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00 0000      0052      0186      00 0000      0052
51 0000      0000      0458      51 0000      0000
51 0000      0052      0138      51 0000      0052
30 0000      0051      0266      30 0000      0051
23 0258      5151      0218      23 0258      5151
10 9861      2351      0521      10 9861      2351
10 0000      0051      0611      10 0000      0051
81 5850      8249      0212      81 5850      8249
73 4265      7350      0515      73 4265      7350
16 1538      4651      0347      16 1538      4651
99 9999      9950      0579      99 9999      9950
17 0496      1749      NUM      4      0274      17 0496      1749
39 5804      2050      NUM      3      0327      39 5804      2050
12 8205      1351      NUM      2      0559      12 8205      1351

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[illegible]

APPENDIX H
VECTOR AND PROPELLANT PROGRAM

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1 1      PROGRAM FOR ASSEMBLING
2 1      COMBUSTION PRODUCT PACKED
3 1      VECTORS AND FUEL AND OXIDANT
4 1      GRAM ATOM RATIOS ENTHALPIES
5 1      AND OXIDATION NUMBERS
6 1
7      REG A0001    0011    ATOM TABLE
8      REG F0100    0199    FUELS
9      REG X0200    0299    OXIDANTS
10     REG L0300    0309    PCTS FUEL
11     REG D0310    0319    PCTS OXID
12     REG H0320    0329    FUEL ENTH
13     REG E0330    0339    OXID ENTH
14     REG W0340    0349    ATOMIC WTS
15     REG S0350    0359    OXID NUMBR
16     REG N0360    0379    MOLES
17     REG G0380    0399    GRAM ATOMS
18 1      PER GRAM
19     REG M0400    0510    ATOMIC WTS
20     REG V0600    0710    SYMBOL AND
21 1      OXID TABLE
22
23     REG U0800    0809
24     REG R1951    1960    READ BAND
25     REG P1977    1986    PUNCH BAND
26
27     BLR 0000    0000
28     BLR 0090    0099    ZEROS
29     BLR 0360    0379    SPARE
30     BLR 0537    0549    OXIDANT
31     BLR 0587    0599    FUEL
32     BLR 0900    0909
33     BLR 1500    1999
34     SYN PUNCH    1930
35     SYN RMPCH    1940
36     EQU TEMPO    C0001    TEMPORARY
37     EQU TEMP1    C0002    TEMPORARY
38     EQU TEMP2    C0003    TEMPORARY
39 1      EQU R000X    R0001
40
41     EQU U01XX    U0101
42     EQU V00XX    V0001
43     EQU M00XX    M0001
44 1      EQU XXXXX    0000
45 1
46 1      TABLE OF ATOMIC WEIGHTS
47 M0001    39 9440    0052    ARGON      0400 39 9440 0052
48 M0002    22 7000    0053    ACTINIUM   0401 22 7000 0053
49 M0003    10 7880    0053    SILVER    0402 10 7880 0053
50 M0004    26 9800    0052    ALUMINUM  0403 26 9800 0052
51 M0005    24 3000    0053    AMERICIUM 0404 24 3000 0053
52 M0006    74 9100    0052    ARSENIC   0405 74 9100 0052
53 M0007    21 1000    0053    ASTATINE  0406 21 1000 0053
54 M0008    19 7000    0053    GOLD      0407 19 7000 0053
55 M0009    10 8200    0052    BORON     0408 10 8200 0052
56 M0011    90 1300    0051    BERYLLIUM 0410 90 1300 0051
57 M0012    20 9000    0053    BISMUTH   0411 20 9000 0053
58 M0013    24 5000    0053    BERKELIUM 0412 24 5000 0053
59 M0010    13 7360    0053    BARIUM    0409 13 7360 0053
60 M0014    79 9160    0052    BROMINE   0413 79 9160 0052
61 M0015    12 0110    0052    CARBON    0414 12 0110 0052
62 M0016    40 0800    0052    CALCIUM   0415 40 0800 0052
63 M0017    11 2410    0053    CADMIUM   0416 11 2410 0053
64 M0018    14 0130    0053    CERIUM    0417 14 0130 0053
65 M0019    24 8000    0053    CALIFORNIUM 0418 24 8000 0053
66 M0020    35 4570    0052    CHLORINE  0419 35 4570 0052
67 M0021    24 5000    0053    CURIUM    0420 24 5000 0053
68 M0022    58 9400    0052    COBALT    0421 58 9400 0052
69 M0023    52 0100    0052    CHROMIUM  0422 52 0100 0052
70 M0024    13 2910    0053    CESIUM    0423 13 2910 0053
71 M0025    63 5400    0052    COPPER    0424 63 5400 0052
72 M0026    16 2510    0053    DYSPROSIUM 0425 16 2510 0053
73 M0027    25 5000    0053    EINSTEINIUM 0426 25 5000 0053
74 M0028    16 7270    0053    ERBIUM    0427 16 7270 0053
75 M0029    15 2000    0053    EUROPIUM  0428 15 2000 0053
76 M0030    19 0000    0052    FLUORINE  0429 19 0000 0052
77 M0031    55 8500    0052    IRON      0430 55 8500 0052
78 M0032    25 2000    0053    FERMIUM   0431 25 2000 0053
79 M0033    22 3000    0053    FRANCIUM  0432 22 3000 0053
80 M0034    69 7200    0052    GALLIUM   0433 69 7200 0052
81 M0035    15 7260    0053    GADOLINIUM 0434 15 7260 0053
82 M0036    72 6000    0052    GERMANIUM 0435 72 6000 0052
      M0037    10 0800    0051    HYDROGEN  0436 10 0800 0051

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83	M0038	40	0300	0051	HELIUM	0437	40	0300	0051
84	M0039	17	8580	0053	HAFNIUM	0438	17	8580	0053
85	M0040	20	0610	0053	MERCURY	0439	20	0610	0053
86	M0041	16	4940	0053	HOLMIUM	0440	16	4940	0053
87	M0042	12	6910	0053	IODINE	0441	12	6910	0053
88	M0043	11	4820	0053	INDIUM	0442	11	4820	0053
89	M0044	19	2200	0053	IRIDIUM	0443	19	2200	0053
90	M0045	39	1000	0052	POTASSIUM	0444	39	1000	0052
91	M0046	83	8000	0052	KRYPTON	0445	83	8000	0052
92	M0047	13	8920	0053	LANTHANUM	0446	13	8920	0053
93	M0048	69	4000	0051	LITHIUM	0447	69	4000	0051
94	M0051	17	4990	0053	LUTETIUM	0450	17	4990	0053
95	M0052	24	3200	0052	MAGNESIUM	0451	24	3200	0052
96	M0053	54	9400	0052	MANGANESE	0452	54	9400	0052
97	M0054	95	9500	0052	MOLYBDENUM	0453	95	9500	0052
98	M0055	25	6000	0053	MENDELEVUM	0454	25	6000	0053
99	M0056	14	0080	0052	NITROGEN	0455	14	0080	0052
100	M0057	22	9910	0052	SODIUM	0456	22	9910	0052
101	M0058	92	9100	0052	NI0BIUM	0457	92	9100	0052
102	M0059	14	4270	0053	NEODYMIUM	0458	14	4270	0053
103	M0060	20	1830	0052	NEON	0459	20	1830	0052
104	M0061	58	7100	0052	NICKEL	0460	58	7100	0052
105	M0062	23	7000	0053	NEPTUNIUM	0461	23	7000	0053
106	M0063	16	0000	0052	OXYGEN	0462	16	0000	0052
107	M0064	19	0200	0053	OSMIUM	0463	19	0200	0053
108	M0065	30	9750	0052	PHOSPHORUS	0464	30	9750	0052
109	M0066	23	1000	0053	PROTACTINIUM	0465	23	1000	0053
110	M0067	20	7210	0053	LEAD	0466	20	7210	0053
111	M0068	10	6700	0053	PALLADIUM	0467	10	6700	0053
112	M0069	14	5000	0053	PROMETHIUM	0468	14	5000	0053
113	M0070	21	0000	0053	POLONIUM	0469	21	0000	0053
114	M0071	14	0920	0053	PRASEODYMIUM	0470	14	0920	0053
115	M0072	19	5090	0053	PLATINUM	0471	19	5090	0053
116	M0073	24	2000	0053	PLUTONIUM	0472	24	2000	0053
117	M0074	22	6050	0053	RADIUM	0473	22	6050	0053
118	M0075	85	4800	0052	RUBIDIUM	0474	85	4800	0052
119	M0076	18	6220	0053	RHENIUM	0475	18	6220	0053
120	M0077	10	2910	0053	RHODIUM	0476	10	2910	0053
121	M0078	22	2000	0053	RADON	0477	22	2000	0053
122	M0079	10	1100	0053	RUTHENIUM	0478	10	1100	0053
123	M0080	32	0660	0052	SULFUR	0479	32	0660	0052
124	M0081	12	1760	0053	ANTIMONY	0480	12	1760	0053
125	M0082	44	9600	0052	SCANDIUM	0481	44	9600	0052
126	M0083	78	9600	0052	SELENIUM	0482	78	9600	0052
127	M0084	28	0900	0052	SILICON	0483	28	0900	0052
128	M0085	15	0350	0053	SAMARIUM	0484	15	0350	0053
129	M0086	11	8700	0053	TIN	0485	11	8700	0053
130	M0087	87	6300	0052	STRONTIUM	0486	87	6300	0052
131	M0088	18	0950	0053	TANTALUM	0487	18	0950	0053
132	M0089	15	8930	0053	TERBIUM	0488	15	8930	0053
133	M0090	99	0000	0052	TECHNETIUM	0489	99	0000	0052
134	M0091	12	7610	0053	TELLURIUM	0490	12	7610	0053
135	M0092	23	2050	0053	THORIUM	0491	23	2050	0053
136	M0093	47	9000	0052	TITANIUM	0492	47	9000	0052
137	M0094	20	4390	0053	THALLIUM	0493	20	4390	0053
138	M0095	16	8940	0053	THULIUM	0494	16	8940	0053
139	M0096	23	8070	0053	URANIUM	0495	23	8070	0053
140	M0097	50	9500	0052	VANADIUM	0496	50	9500	0052
141	M0098	18	3860	0053	TUNGSTEN	0497	18	3860	0053
142	M0101	13	1300	0053	XENON	0500	13	1300	0053
143	M0102	88	9200	0052	YTTORIUM	0501	88	9200	0052
144	M0103	17	3040	0053	YTTERBIUM	0502	17	3040	0053
145	M0104	65	3800	0052	ZINC	0503	65	3800	0052
146	M0105	91	2200	0052	ZIRCONIUM	0504	91	2200	0052
147	1								
148	1								
149	V0001	61	0000	0000	ARGON	0500	61	0000	0000
150	V0002	61	6300	0000	ACTINIUM	0501	61	6300	0000
151	V0003	61	6700	0000	SILVER	0502	61	6700	0000
152	V0004	61	7300	0003	ALUMINUM	0503	61	7300	0003
153	V0005	61	7400	0000	AMERICIUM	0504	61	7400	0000
154	V0006	61	8200	0000	ARSENIC	0505	61	8200	0000
155	V0007	61	8300	0000	ASTATINE	0506	61	8300	0000
156	V0008	61	8400	0000	GOLD	0507	61	8400	0000
157	V0009	62	0000	0003	BORON	0508	62	0000	0003
158	V0010	62	6100	0000	BARIUM	0509	62	6100	0000
159	V0011	62	6500	0002	BERYLLIUM	0510	62	6500	0002
160	V0012	62	6900	0000	BISMUTH	0511	62	6900	0000
161	V0013	62	7200	0000	BERKELIUM	0512	62	7200	0000
162	V0014	62	7900	0001	BROMINE	0513	62	7900	0001
163	V0015	63	0000	0004	CARBON	0514	63	0000	0004
164	V0016	63	6100	0002	CALCIUM	0515	63	6100	0002
165	V0017	63	6400	0000	CADMIUM	0516	63	6400	0000
166	V0018	63	6500	0000	CERIUM	0517	63	6500	0000

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167	V0019	63	6600	0000	CALIFORNIUM	0618	63	6600	0000
168	V0020	- 63	7300	0001	CHLORINE	0619	-63	7300	0001
169	V0021	63	7400	0000	CURIUM	0620	63	7400	0000
170	V0022	63	7600	0000	COBALT	0621	63	7600	0000
171	V0023	63	7900	0000	CHROMIUM	0622	63	7900	0000
172	V0024	63	8200	0000	CESIUM	0623	63	8200	0000
173	V0025	63	8400	0000	COPPER	0624	63	8400	0000
174	V0026	64	8800	0000	DYSPROSIUM	0625	64	8800	0000
175	V0027	65	0000	0000	EINSTEINIUM	0626	65	0000	0000
176	V0028	65	7900	0000	ERBIUM	0627	65	7900	0000
177	V0029	65	8400	0000	EUROPIUM	0628	65	8400	0000
178	V0030	- 66	0000	0001	FLUORINE	0629	-66	0000	0001
179	V0031	66	6500	0000	IRON	0630	66	6500	0000
180	V0032	66	7400	0000	FERMIUM	0631	66	7400	0000
181	V0033	66	7900	0000	FRANCIUM	0632	66	7900	0000
182	V0034	67	6100	0000	GALLIUM	0633	67	6100	0000
183	V0035	67	6400	0000	GADOLINIUM	0634	67	6400	0000
184	V0036	67	6500	0000	GERMANIUM	0635	67	6500	0000
185	V0037	68	0000	0001	HYDROGEN	0636	68	0000	0001
186	V0038	68	6500	0000	HELIUM	0637	68	6500	0000
187	V0039	68	6600	0000	HAFNIUM	0638	68	6600	0000
188	V0040	68	6700	0000	MERCURY	0639	68	6700	0000
189	V0041	68	7600	0000	HOLMIUM	0640	68	7600	0000
190	V0042	- 69	0000	0001	IODINE	0641	-69	0000	0001
191	V0043	69	7500	0000	INDIUM	0642	69	7500	0000
192	V0044	69	7900	0000	IRIDIUM	0643	69	7900	0000
193	V0045	72	0000	0001	POTASSIUM	0644	72	0000	0001
194	V0046	72	7900	0000	KRYPTON	0645	72	7900	0000
195	V0047	73	6100	0000	LANTHANUM	0646	73	6100	0000
196	V0048	73	6900	0001	LITHIUM	0647	73	6900	0001
197	V0051	73	8400	0000	LUTETIUM	0650	73	8400	0000
198	V0052	74	6700	0002	MAGNESIUM	0651	74	6700	0002
199	V0053	74	7500	0000	MANGANESE	0652	74	7500	0000
200	V0054	74	7600	0000	MOLYBDENUM	0653	74	7600	0000
201	V0055	74	8500	0000	MENDELEVUM	0654	74	8500	0000
202	V0056	75	0000	0000	NITROGEN	0655	75	0000	0000
203	V0057	75	6100	0001	SODIUM	0656	75	6100	0001
204	V0058	75	6200	0000	NIوبيUM	0657	75	6200	0000
205	V0059	75	6400	0000	NEODYMIUM	0658	75	6400	0000
206	V0060	75	6500	0000	NEON	0659	75	6500	0000
207	V0061	75	6900	0000	NICKEL	0660	75	6900	0000
208	V0062	75	7700	0000	NEPTUNIUM	0661	75	7700	0000
209	V0063	- 76	0000	0002	OXYGEN	0662	-76	0000	0002
210	V0064	76	8200	0000	OSMIUM	0663	76	8200	0000
211	V0065	77	0000	0000	PHOSPHORUS	0664	77	0000	0000
212	V0066	77	6100	0000	PROTACTIUM	0665	77	6100	0000
213	V0067	77	6200	0000	LEAD	0666	77	6200	0000
214	V0068	77	6400	0000	PALLADIUM	0667	77	6400	0000
215	V0069	77	7400	0000	PROMETHIUM	0668	77	7400	0000
216	V0070	77	7600	0000	POLONIUM	0669	77	7600	0000
217	V0071	77	7900	0000	PRASEODYMIUM	0670	77	7900	0000
218	V0072	77	8300	0000	PLATINUM	0671	77	8300	0000
219	V0073	77	8400	0000	PLUTONIUM	0672	77	8400	0000
220	V0074	79	6100	0000	RADIUM	0673	79	6100	0000
221	V0075	79	6200	0000	RUBIDIUM	0674	79	6200	0000
222	V0076	79	6500	0000	RHENIUM	0675	79	6500	0000
223	V0077	79	6800	0000	RHODIUM	0676	79	6800	0000
224	V0078	79	7500	0000	RADON	0677	79	7500	0000
225	V0079	79	8400	0000	RUTHENIUM	0678	79	8400	0000
226	V0080	82	0000	0004	SULFUR	0679	82	0000	0004
227	V0081	82	6200	0000	ANTIMONY	0680	82	6200	0000
228	V0082	82	6300	0000	SCANDIUM	0681	82	6300	0000
229	V0083	82	6500	0000	SELENIUM	0682	82	6500	0000
230	V0084	82	6900	0004	SILICON	0683	82	6900	0004
231	V0085	82	7400	0000	SAMARIUM	0684	82	7400	0000
232	V0086	82	7500	0000	TIN	0685	82	7500	0000
233	V0087	82	7900	0000	STRONTIUM	0686	82	7900	0000
234	V0088	83	6100	0000	TANTALUM	0687	83	6100	0000
235	V0089	83	6200	0000	TERBIUM	0688	83	6200	0000
236	V0090	83	6300	0000	TECHNETIUM	0689	83	6300	0000
237	V0091	83	6500	0000	TELLURIUM	0690	83	6500	0000
238	V0092	83	6800	0000	THORIUM	0691	83	6800	0000
239	V0093	83	6900	0000	TITANIUM	0692	83	6900	0000
240	V0094	83	7300	0000	THALLIUM	0693	83	7300	0000
241	V0095	83	7400	0000	THULIUM	0694	83	7400	0000
242	V0096	84	0000	0000	URANIUM	0695	84	0000	0000
243	V0097	85	0000	0000	VANADIUM	0696	85	0000	0000
244	V0098	86	0000	0000	TUNGSTEN	0697	86	0000	0000
245	V0101	87	6500	0000	XENON	0700	87	6500	0000
246	V0102	88	0000	0000	YTTRIUM	0701	88	0000	0000
247	V0103	88	6100	0000	YTTERBIUM	0702	88	6100	0000
248	V0104	89	7500	0000	ZINC	0703	89	7500	0000
249	V0105	89	7900	0000	ZIRCONIUM	0704	89	7900	0000

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251 1          CLEAR ROUTINE
252 1
253 CLEAR      RAA 0010          0050 80 0010 0056
254          RAM 8002 CLR 1      0056 67 8002 0015
255 CLR 1      STU 9049 A        0015 21 9749 0023
256          NZA          CLR 2  0023 40 0026 0027
257          SXA 0001 CLR 1      0026 51 0001 0015
258 CLR 2      SET 9049          0027 27 9049 0032
259          STB A0001          0032 29 0001 0054
260          RAA 0300 CLR 3      0054 80 0300 0060
261 CLR 3      SET 9050          0060 27 9050 0065
262          SBB 0090 A          0065 28 2090 0043
263          NZA          SET01  0043 40 0046 0047
264          SXA 0010 CLR 3      0046 51 0010 0060
265 SET01      RSU UNITY          0047 61 0550 0055
266          STU ATMCT          0055 21 0560 0013
267          STD RELAY READ      SET SWITCH- 0013 24 0016 0019
                                   TO ATOMS
268 1
269 1
270 1          READ ROUTINE
271 READ      RCD R0001          READ CARD  0019 70 1951 0051
272          LDD R0001          TRANSFER  0051 69 1951 0554
273          STD P0001          IMPUT FROM  0554 24 1977 0030
274          LDD R0002          READ BAND   0030 69 1952 0555
275          STD P0002          TO PUNCH    0555 24 1978 0031
276          LDD R0003          BAND        0031 69 1953 0556
277          STD P0003          0556 24 1979 0082
278          LDD R0004          0082 69 1954 0057
279          STD P0004          0057 24 1980 0033
280          LDD R0005          0033 69 1955 0058
281          STD P0005          0058 24 1981 0034
282          LDD R0006          0034 69 1956 0059
283          STD P0006          0059 24 1982 0035
284          RAU R0010          0035 60 1960 0515
285          STL P0007          CLER P0007  0515 20 1983 0036
286          STD P0009          CLER P0009  0036 24 1985 0038
287          SRT 0002          0038 30 0002 0045
288          STU P0008          0045 21 1984 0037
289          NZU          PV007          SET P0010 0037 44 0041 0042
290          ALO 823RD          TO PUNCH  0041 15 0044 0049
291          STL P0010          PNCH          TYPE1 CARD 0049 20 1986 0039
292 PV007      RAU R0004          REARRANGE 0042 60 1954 0559
293          SRT 0004          VECTOR IN  0559 30 0004 0069
294          SLO 8002          WORDS 2 3  0069 16 8002 0077
295          STD R0004          4 5 AND 6  0077 24 1954 0557
296          SLT 0004          0557 35 0004 0017
297          STU SYMBL          SAVE SYMBL  0017 21 0022 0025
298          RAL R0004          0025 65 1954 0759
299          SLT 0002          0759 35 0002 0565
300          SLO 8002          0565 16 8002 0073
301          STD TEMPO          0073 24 9000 0029
302          ALO R0003          0029 15 1953 0757
303          SLT 0008          0757 35 0008 0075
304          STU R0003          0075 21 1953 0756
305          STL TEMP1          0756 20 9001 0014
306          RAU R0006          0014 60 1956 0061
307          SRT 0004          0061 30 0004 0021
308          STL R0006          0021 20 1956 0859
309          RAL 8003          0859 65 8003 0067
310          SLT 0004          0067 35 0004 0527
311          AUP R0005          0527 10 1955 0959
312          SRT 0004          0959 30 0004 0519
313          STL R0005          0519 20 1955 0558
314          AUP TEMP1          0558 10 9001 0715
315          STU R0004          0715 21 1954 0857
316          RAU TEMPO          0857 60 9000 0765
317          SRT 0002          0765 30 0002 0071
318          AUP R0004          0071 10 1954 1009
319          STU R0004          LOOK        1009 21 1954 0957
320 1          CONSTANTS FOR READ ROUTINE
321 823RD      00 0000 0880          0044 00 0000 0880
322 1
323 1          TABLE LOOKUP ROUTINE TO FIND
324 1          CORRECT ROUTINE FOR SYMBOL
325 1          BEING PROCESSED
326 1
327 LOOK      LDD SYMBL          0957 69 0022 0525
328          TLU U0001          0525 84 0800 0755
329          SUP 8003          0755 11 8003 0063
330          SRT 0004          0063 30 0004 0523
331          ALO 100 I          8002          0523 15 0076 8002
332 8002      00 0000 U01XX          8002 00 0000 0900
333 1

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334 U0101  RAU SYMBL          ATM PROGRAM 0900 60 0022 0577
335          SUP ATM          0577 11 0080 0085
336          NZU              PV009      0085 44 0089 0040
337          HLT 9999          1111      0089 01 9999 1111
338 1
339 U0102  RAU SYMBL          BOP PROGRAM 0901 60 0022 0727
340          SUP BOP          0727 11 0530 0535
341          NZU              CLEAR      0535 44 0739 0050
342          HLT 9999          2222      0739 01 9999 2222
343 1
344 U0103  RAU SYMBL          FUEL          0902 60 0022 0777
345          SRT 0006          ENTHALPY    0777 30 0006 0741
346          SLO 8002          PROGRAM     0741 16 8002 0749
347          STD CODE          0749 24 0052 0855
348          SLT 0006          0855 35 0006 0569
349          SUP EF            0569 11 0072 0827
350          NZU              OK 3        0827 44 0081 0532
351          HLT 9999          3333      0081 01 9999 3333
352 OK 3    RAA 0319          PAR 1      0532 80 0319 0088
353 1
354 1
355 1
356 1      CONSOLE POSITION 2 IS SET TO 8
357 1      IF IT IS DESIRED TO PUNCH OUT
358 1      FUELS OXIDANTS PERCENTS AND
359 1      ENTHALPIES
360 1
361 U0104  RAU SYMBL          PROPELLANT 0903 60 0022 0877
362          SUP END          READY TO    0877 11 0580 0585
363          NZU              DIST2      0585 44 0789 0740
364          HLT 9999          4444      0789 01 9999 4444
365 DIST2   LDD 8000          0740 69 8000 0746
366          BD2              END 1      0746 92 0799 0551
367          RAL SPEC5        0799 65 0552 1007
368          LDD END 1        PUNCH      1007 69 0551 1930
369 SPEC5   00 0100          0240      0552 00 0100 0240
370 1
371 U0105  RAU SYMBL          OXIDANT      0904 60 0022 0927
372          SRT 0006          ENTHALPY    0927 30 0006 0791
373          SLO 8002          PROGRAM     0791 16 8002 0849
374          STD CODE          0849 24 0052 0955
375          SLT 0006          0955 35 0006 0719
376          SUP EX            0719 11 0522 0977
377          NZU              OK 5        0977 44 0531 0582
378          HLT 9999          5555      0531 01 9999 5555
379 OK 5    RAA 0329          PAR 1      0582 80 0329 0088
380 1
381 U0106  RAU SYMBL          FUEL          0905 60 0022 1027
382          SRT 0008          PROGRAM     1027 30 0008 0745
383          SLO 8002          0745 16 8002 0053
384          STD CODE          0053 24 0052 1005
385          SLT 0008          1005 35 0008 0573
386          SUP F            0573 11 0526 0581
387          NZU              OK 6        0581 44 0735 0086
388          HLT 9999          6666      0735 01 9999 6666
389 OK 6    RAA 0099          PV180     0086 80 0099 0742
390          STL R0007        0742 20 1957 0760
391 1
392 U0107  RAU SYMBL          MOLECULE     0906 60 0022 1077
393          SUP MOL          PROGRAM     1077 11 0730 0785
394          NZU              PV015      0785 44 0839 0790
395          HLT 9999          7777      0839 01 9999 7777
396 1
397 U0108  RAU SYMBL          PERCENT      0907 60 0022 1127
398          SRT 0006          FUEL        1127 30 0006 0841
399          SLO 8002          PROGRAM     0841 16 8002 0899
400          STD CODE          0899 24 0052 1055
401          SLT 0006          1055 35 0006 0769
402          SUP PF            0769 11 0572 1177
403          NZU              OK 8        1177 44 0731 0732
404          HLT 9999          8888      0731 01 9999 8888
405 OK 8    RAA 0299          PAR 1      0732 80 0299 0088
406 1
407 U0109  RAU SYMBL          PERCENT      0908 60 0022 1227
408          SRT 0006          OXIDANT     1227 30 0006 0891
409          SLO 8002          PROGRAM     0891 16 8002 0949
410          STD CODE          0949 24 0052 1105
411          SLT 0006          1105 35 0006 0819
412          SUP PX            0819 11 0722 1277
413          NZU              OK 9        1277 44 0781 0782
414          HLT 9999          9999      0781 01 9999 9999
415 OK 9    RAA 0309          PAR 1      0782 80 0309 0088
416 1

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417 U0110 RAU SYMBL          OXIDANT 0909 60 0022 1327
418 SRT 0008                PROGRAM 1327 30 0008 0795
419 SLO 8002                0795 16 8002 0553
420 STD CODE                0553 24 0052 1155
421 SLT 0008                1155 35 0008 0723
422 SUP X                   0723 11 0576 0831
423 NZU                     0831 44 0835 0536
424 HLT 9999 OK 10          0835 01 9999 0000
425 RAA 0199                0536 80 0199 0792
426 STL R0007 PV180        CLER R0007 0792 20 1957 0760
427 1
428 1      CONSTANTS FOR TABLE LOOKUP
429 1      ROUTINE
430 ATM 61 8374 0000        0080 61 8374 0000
431 BOP 62 7677 0000        0530 62 7677 0000
432 EF 65 6600 0000        0072 65 6600 0000
433 END 65 7564 0000       0580 65 7564 0000
434 EX 65 8700 0000        0522 65 8700 0000
435 F 66 0000 0000         0526 66 0000 0000
436 MOL 74 7673 0000       0730 74 7673 0000
437 PF 77 6600 0000        0572 77 6600 0000
438 PX 77 8700 0000        0722 77 8700 0000
439 X 87 0000 0000         0576 87 0000 0000
440 U0001 61 8374 0000      ATM 0800 61 8374 0000
441 U0002 62 7677 0000      BOP 0801 62 7677 0000
442 U0003 65 6699 0000      EF9 0802 65 6699 0000
443 U0004 65 7564 0000      END 0803 65 7564 0000
444 U0005 65 8799 0000      EX9 0804 65 8799 0000
445 U0006 66 9900 0000      F9 0805 66 9900 0000
446 U0007 74 7673 0000      MOL 0806 74 7673 0000
447 U0008 77 6699 0000      PF9 0807 77 6699 0000
448 U0009 77 8799 0000      PX9 0808 77 8799 0000
449 U0010 87 9900 0000      X9 0809 87 9900 0000
450 100 1 00 0000 0100    0076 00 0000 0100
451 1
452 1      ROUTINE FOR PACKED VECTORS
453 1      ATOMS START AT PV009 AND
454 1      MOLECULES START AT PV015
455 1
456 PV009 LDD R0007          PLACE CODE 0040 69 1957 0810
457 STD P0009                IN OUTPUT 0810 24 1985 0738
458 RAU RELAY                ITS ATOM 0738 60 0016 0521
459 NZU PV011                0521 44 0575 0726
460 HLT 2222 8888            SWITCH NOT 0726 01 2222 8888
461 1 INITIALIZE
462 PV011 RAL R0002          IS ATOM 0575 65 1952 1057
463 SLT 0004                MORE THAN 1057 35 0004 0517
464 SUP 8003                2 LETTERS 0517 11 8003 0725
465 NZE PV013              0725 45 0028 0079
466 HLT 3333 PV013          YES STOP 0028 01 3333 7777
467 RAL ATMCT                NO 0079 65 0560 0815
468 ALO UNITY                ADVANCE 0815 15 0550 1205
469 STL ATMCT                ATOM COUNT 1205 20 0560 0513
470 ALO R0002                STORE ATOM 0513 15 1952 1107
471 AUP ATMCT                COLUMN 1107 10 0560 0865
472 SLO 8002                EQUIVALENT 0865 16 8002 0773
473 SLT 0004                IN TABLE 0773 35 0004 0083
474 ALO 8001                0083 15 8001 0941
475 AUP STORE 8003          0941 10 0744 8003
476 STL A0001 PACKA        8003 20 0001 0754
477 RAU ATMCT                FORM ATOM 0754 60 0560 0915
478 SLT 0001                VECTOR 0915 35 0001 0571
479 AUP UNITY                STORE IN 0571 10 0550 1255
480 STU P0007 PV116        PUNCH BAND 1255 21 1983 0586
481 LDD R0007                PLACE CODE 0790 69 1957 0860
482 STD P0009                IN OUTPUT 0860 24 1985 0788
483 RAU RELAY                IS THIS 0788 60 0016 0721
484 NZU PV019              FIRST MOL 0721 44 0775 0776
485 STL RELAY                YES 0775 20 0016 0869
486 RAU UNITY                DID WE 0869 60 0550 1305
487 SLT 0001                PROCESS 1305 35 0001 0511
488 SUP 8001                MORE THAN 0511 11 8001 0919
489 SUP ATMCT                TEN ATOMS 0919 11 0560 0965
490 BMI PV017              0965 46 0018 0969
491 HLT 4444 PV017          TOO MANY 0018 01 4444 6666
492 STU COUNT PV019        SET SOLIDS 0969 21 0024 0776
493 1 COUNTER
494 PV019 RAU R0010          NO IS THIS 0776 60 1960 1015
495 SRT 0001                MOLECULE 1015 30 0001 0771
496 RAL 8002                CONDENSED 0771 65 8002 0529
497 NZE PV023              0529 45 0832 0533
498 RAU COUNT                YES MAY WE 0832 60 0024 0579
499 NZU PV024              PROCESS IT 0579 44 0583 0084
500 HLT 5555 5555          NO 0084 01 5555 5555

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501	PV024	SUP UNITY		YES	0583	11	0550	1355
502		STU COUNT	PV023		1355	21	0024	0533
503	PV023	RAU R0005		IS MOLCULE	0533	60	1955	1059
504		NZU	PV025	MORE THAN	1059	44	0563	0064
505	1			15 PLACES				
506		HLT 6666	4444	YES	0563	01	6666	4444
507	PV025	RAL R0002			0064	65	1952	1157
508		NZE PV031			1157	45	0910	0561
509		HLT 7777	3333	NO MOLCULE	0561	01	7777	3333
510	PV031	RAU CNTR1		CLEAR DATA	0910	60	0713	0567
511		STU CNTRX		ADDRESS	0567	21	0772	0825
512		STL TEMP1	PV032	SET ZERO	0825	20	9001	0882
513	PV032	RAL R0002		IS PRODUCT	0882	65	1952	1207
514		NZE	PV115	FINISHED	1207	45	0960	0711
515		SLT 0001		NO	0960	35	0001	0717
516		SUP NINE1			0717	11	0020	0875
517		NZU LETTR	NUMBR		0875	44	0729	0780
518	LETTR	LDD PV032	PV033		0729	69	0882	0885
519	PV033	STD LINK			0885	24	0838	0991
520		RAL R0002			0991	65	1952	1257
521		AUP TEMP1			1257	10	9001	1065
522		SLT 0002			1065	35	0002	0821
523		STU TEMP1			0821	21	9001	0779
524		STL R0002			0779	20	1952	1405
525		RAU CNTRX			1405	60	0772	1377
526		AUP TWO D			1377	10	0830	0935
527		STU CNTRX	LINK		0935	21	0772	0838
528	1							
529	NUMBR	LDD PV034	PV033		0780	69	0733	0885
530	PV034	RAU TEMP1			0733	60	9001	1041
531		SRT 0002	PV087		1041	30	0002	0747
532	PV087	SLO NINE		STORE	0747	16	0750	1455
533		SLO 8002		MAGNITUDE	1455	16	8002	0763
534		STD MAGNI		OF THE	0763	24	0066	1019
535		SCT 0000		COMPONENT	1019	36	0000	1091
536		STU COMPO	PV089		1091	21	0796	0999
537	PV089	RAL A000X		SEARCH	0999	65	1550	0856
538		LDD PV091		SYMBOL	0856	69	1109	0012
539		SDA PV091	8001	TABLE FOR	0012	22	1109	8001
540	1			COMPONENT				
541	PV091	RAL A0001	PV093		1109	65	0001	0956
542	PV093	NZE	PV095		0956	45	1010	0761
543		SRT 0001			1010	30	0001	0767
544		SLT 0001			0767	35	0001	0823
545		SLO COMPO			0823	16	0796	0751
546		NZE	PV097		0751	45	0854	1006
547		RAL PV091		ADVANCE	0854	65	1109	0813
548		ALO ONE D		ONE PLACE	0813	15	0516	0871
549		STL PV091	8001	ALONG	0871	20	1109	8001
550	1			TABLE				
551	PV095	HLT 8888	2222	NOT IN	0761	01	8888	2222
552	1			TABLE				
553	PV097	RAL PV091		GOT THE	1006	65	1109	0863
554		LDD PV099		RIGHT ONE	0863	69	0566	1069
555		SDA PV099	8001		1069	22	0566	8001
556	PV099	RAU A0001	PV100	ADD IT TO	0566	60	0001	1056
557	PV100	SRT 0001		REST OF	1056	30	0001	0913
558		ALO MAGNI		PACKED	0913	15	0066	0921
559		SUP 8003		VECTOR IN	0921	11	8003	0829
560		AUP P0007		P0007	0829	10	1983	0087
561		SLT 0002			0087	35	0002	0743
562		STU P0007			0743	21	1983	0736
563		RAL R0003	CNTRX	SHIFT	0736	65	1953	0772
564	CNTRX	SLT XXXXX	PV101	WORD 3	0772	35	0000	0845
565	1							
566	PV101	AUP R0002			0845	10	1952	1307
567		STU R0002			1307	21	1952	1106
568		STL R0003			1106	20	1953	1156
569	1							
570		RAL CNTRX		CNTRY DATA	1156	65	0772	1427
571		LDD CNTR2		ADRES SAME	1427	69	0880	0783
572		SDA CNTRY		AS CNTRX	0783	22	0737	0840
573	1							
574		RAL P0004	CNTRY	SHIFT	0840	65	1954	0737
575	CNTRY	SLT XXXXX	PV102	WORD 4	0737	35	0000	1159
576	PV102	AUP R0003			1159	10	1953	1357
577		STU R0003			1357	21	1953	1206
578		STL R0004	PV031		1206	20	1954	0910
579	PV115	RAU R0010			0910	60	1960	1115
580		SRT 0001			1115	30	0001	0971
581		RAU 8002			0971	60	8002	0879
582		NZU	PV116	A SIGN FOR	0879	44	0833	0586
583		RSU P0007	PV116	THE PACKED	0833	61	1983	0787
584		STU P0007		VECTOR	0787	21	1983	0586
585	PV116	LDD 8390			0586	69	0389	0842
586		STD P0010	PNCH		0842	24	1986	0039
587	PNCH	PCH P0001	READ	PUNCH CARD	0039	71	1977	0019

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588 1
589 1
590 1
591 1
592 1      UNITY      00 0000 0001      0550 00 0700 0001
593 1      ONE D      00 0001 0000      0516 00 0001 0000
594 1      TWO D      00 0002 0000      0830 00 0002 0000
595 1      NINEI      00 0000 0009      0020 00 0000 0009
596 1      NINE      90 0000 0000      0750 90 0000 0000
597 1      STORE      STL A0001  PACKA      0744 20 0001 0754
598 1      A000X      00 A0001  0000      1550 00 0001 0000
599 1      CNTR1      SLT 0000  PV101      0713 35 0000 0845
600 1      CNTR2      SLT 0000  PV102      0880 35 0000 1159
601 1      83RD      00 0000 0800      0889 00 0000 0800
602 1
603 1
604 1
605 1
606 1
607 1      PV180      RAU RELAY      IF NO      0760 60 0016 1021
608 1      NZU      PV198      MOLECULES      1021 44 0925 0826
609 1
610 1
611 1
612 1      STL RELAY      YES      0925 20 0016 1119
613 1      RAU NINEI      ARE THERE      1119 60 0020 0975
614 1      SUP ATMCT      MORE THAN      0975 11 0560 1165
615 1      BMI      PV198      TEN ATOMS      1165 46 0068 0826
616 1      HLT 9988      YES      0068 01 9988 9988
617 1      PV198      RAU R0002      0826 60 1952 1407
618 1      NZU PV200      NO LETTERS      1407 44 0811 0062
619 1      HLT 9876      9876      OR NUMBERS      0062 01 9876 9876
620 1      PV200      STL TEMP1      CLER TEMP1      0811 20 9001 0518
621 1      STD TEMP2      CLER TEMP2      0518 24 9002 0074
622 1      STU RELA1      SET NONZRO      0074 21 0078 0881
623 1      RAB 0000      PV201      B IS NUMBR      0881 82 0000 0837
624 1
625 1      PV201      RAL R0002      ANY FUEL      0837 65 1952 1457
626 1      NZE      PV220      OR OX LEFT      1457 45 1060 0861
627 1      SLT 0001      YES      1060 35 0001 0817
628 1      SUP NINEI      IS SYMBOL      0817 11 0020 1025
629 1      BMI LETR      NUMR      LET OR NUM      1025 46 0528 0929
630 1      LETR      RAU RELA1      DO WE STOR      0528 60 0078 0882
631 1      NZU      PV221      PREV COEFF      0883 44 0887 0888
632 1      RAL R0002      NO      0887 65 1952 0758
633 1      AUP TEMP1      0758 10 9001 1215
634 1      SLT 0002      1215 35 0002 1071
635 1      STU TEMP1      PV209      1071 21 9001 0979
636 1
637 1      PV209      STL R0002      0979 20 1952 1256
638 1      RSC 0003      PV210      SHIFT      1256 89 0003 0512
639 1      PV210      RAL R0006 C      WORDS 2 3      0512 65 7956 0911
640 1      AUP R0005 C      4 5 AND 6      0911 35 0002 0867
641 1      STU R0005 C      0867 10 7955 1209
642 1      STL R0006 C      1209 21 7955 0858
643 1      NZC      PV201      0858 20 7956 1259
644 1      AXC 0001      PV210      1259 48 0562 0837
645 1      STU RELA1      CLER RELA1      0562 58 0001 0512
646 1      AUP TEMP2      ADD TO CNT      0929 21 0078 0931
647 1      SLT 0001      0931 52 0001 0937
648 1      STU TEMP2      0937 10 9002 0895
649 1      LDD PAR 6      PV209      0895 35 0001 0851
650 1      LDD PV200      PV222      0851 21 9002 0979
651 1      STD LINK      PV222      0861 69 0514 C917
652 1      RSC 0009      YES      0888 69 0811 0917
653 1      RAU TEMP1      0917 24 0838 1141
654 1      SCT 0000      1141 89 0009 0797
655 1      STU TEMP1      PV223      0797 60 9001 1306
656 1      RAL A0010 C      FIND      1306 36 0000 1029
657 1      SRT 0001      SYMBOL N      1029 21 9001 0987
658 1      SLT 0001      TABLE      0987 65 6010 1265
659 1      SLO TEMP1      1265 30 0001 1121
660 1      NZE      PV225      1121 35 0001 1477
661 1      NZC      PV224      1477 16 9001 0985
662 1      AXC 0001      PV223      0985 45 0938 0939
663 1      HLT 4321      0938 48 1191 0892
664 1      PV224      NOT IN      1191 58 0001 0987
665 1      RAU CODE      TABLE      0892 01 4321 4321
666 1      SLT 0001      GENERATE      0939 60 0052 0958
667 1      SRT 0008      STORAGE      0958 35 0001 1315
668 1      NZU PV227      PV226      1315 30 0008 0933
669 1      RAU 100 I      PV227      0933 44 1037 0988
670 1
671 1

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672 PV227 AUP 8005 1037 10 8005 0945
673 AUP 8007 0945 10 8007 0753
674 SLT 0004 0753 35 0004 0963
675 AUP MASK1 0963 10 0716 1171
676 STU PV233 1171 21 0876 1079
677 RAU TEN I IS NUMBER 1079 60 0932 1087
678 SUP 8006 OVER TEN 1087 11 8006 0995
679 BMI PV230 4455 DIGITS 0995 46 0048 1049
680 HLT 2233 PV231 YES ERROR 0048 01 2233 4455
681 PV230 NZU PV231 IS IT TEN 1049 44 0853 0954
682 SUP ONE I NO 0853 11 1356 0961
683 NZU PV232 IS IT NINE 0961 44 1365 0766
684 HLT 5544 3322 YES ERROR 0766 01 5544 3322
685 PV231 RAU TEMP2 PV233 0954 60 9002 0876
686 PV232 RAU TEMP2 1365 60 9002 0873
687 SCT 0000 0873 36 0000 1045
688 AUP 8006 1045 10 8006 0953
689 RAB 0050 0953 82 0050 1309
690 AUP 8006 1309 10 8006 0967
691 SLO 8002 PV233 0967 16 8002 0876
692 PV233 STU XXXXX LINK 0876 21 0000 0838
693 1
694 1
695 1
696 1
697 1
698 ONE I 00 0000 0001 1356 00 0000 0001
699 NINE I 00 0000 0009 0020 00 0000 0009
700 TEN I 00 0000 0010 0932 00 0000 0010
701 100 I 00 0000 0100 0076 00 0000 0100
702 MASK1 STU 0000 LINK 0716 21 0000 0838
703 1
704 1
705 1
706 1
707 1
708 1
709 1
710 PAR 1 RAU R0004 0088 60 1954 1359
711 STL TEMPO 1359 20 9000 0816
712 NZU ERR 1 0816 44 1169 0070
713 ERR 1 HLT 8888 1111 PARAMETER 1169 01 8888 1111
714 1 MORE THAN
715 1 10 FIGURES
716 COLAP RSB 0001 COLAP 0070 83 0001 0926
717 COLAP RAC 0005 0926 88 0005 0982
718 RAL R0003 B 0982 65 5953 1008
719 SLO 90909 PAR 2 1008 16 1011 1415
720 PAR 2 SLT 0001 REMOVING 1415 35 0001 1221
721 AUP TEMPO NINES 1221 10 9000 1129
722 SLT 0001 1129 35 0001 1035
723 STU TEMPO 1035 21 9000 0793
724 SUP 8003 0793 11 8003 0951
725 SXC 0001 0951 59 0001 1058
726 NZC PAR 2 1058 48 1415 0712
727 NZB PAR 3 0712 42 1465 0866
728 AXB 0001 COLAP 1465 52 0001 0926
729 PAR 3 RAU CODE GENERATE 0866 60 0052 1108
730 SLT 0001 STORAGE 1108 35 0001 0916
731 SRT 0009 LOCATION 0916 30 0009 1137
732 NZU PAR 5 PAR 4 1137 44 1241 0942
733 PAR 4 RAU TEN I PAR 5 0942 60 0932 1241
734 PAR 5 AUP 8005 1241 10 8005 1099
735 SLT 0004 1099 35 0004 1409
736 AUP MASK5 1409 10 0762 1017
737 ALO TEMPO 8003 1017 15 9000 8003
738 8003 STL XXXXX PAR 6 8003 20 0000 0514
739 PAR 6 PCH P0001 READ 0514 71 1977 0019
740 1
741 1
742 1
743 1
744 1
745 TEN I 00 0000 0010 0932 00 0000 0010
746 90909 90 9090 9090 1011 90 9090 9090
747 MASK5 STL 0000 PAR 6 0762 20 0000 0514
748 1
749 1

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750 1
751 1
752 1
753 1
754 1
755 1
756 1
757 END 1 RAA 0010
758 RAC 0010
759 RAB 0001 END 2
760 END 2 RAA 8003
761 STL TEMPO END 3
762 END 3 RAA L0000 C
763 FAD TEMPO
764 STU TEMPO
765 RAA L0000 C
766 FDV 10053
767 STU C0010 C
768 SXA 0001
769 NZA END 4
770 SXC 0001 END 3
771 END 4 RAA TEMPO
772 FSB 11051
773 BMI FRACT PRCNT
774 FRACT RAA TEMPO END 5
775 PRCNT SET C0010 C
776 SBB L0000 C
777 RAA TEMPO
778 FDV 10053 END 5
779 END 5 FSB 10051
780 RAM 8003
781 AUP 47 I
782 SUP 8002
783 BMI
784 HLT 1111 1111
785 1
786 1
787 END 6 NZB MW 1
788 SXB 0001
789 RAA 0010
790 RAC 0020 END 2
791 1
792 1
793 1
794 1
795 1
796 1
797 1
798 1
799 1
800 1
801 1
802 1
803 MW 1 RAA 0000 MW 2
804 MW 2 RAA A0001 A
805 NZU DIST3
806 SRT 0001
807 SLO 8002
808 SLT 0001
809 ALO MASK6
810 LDD 8003
811 TLU V0001 MW 3
812 MW 3 STL TEMPO 8001
813 8001 RAL V00XX MW 4
814 MW 4 SLT 0009
815 SUP 8003
816 BMI MW 5
817 SLO 51 I MW 6
818 MW 5 ALO 51 I MW 6
819 MW 6 STL S0001 A MW 7
820 MW 7 RAL TEMPO
821 SLO 200 D
822 LDD MASK7
823 SDA TEMPO 8001
824 8001 LDD M00XX MW 8
825 MW 8 STD W0001 A
826 AXA 0001 MW 2
827 1
828 DIST3 LDD 8000
829 BD3 AR 1
830 RAL SPEC6
831 LDD AR 1 PUNCH
832 SPEC6 00 W0001 0020
833 1

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ROUTINE TO CALCULATE THE GRAM
ATOMS AND ENTHALPIES AND THE
OXIDATION NUMBERS PER GRAM OF
COMBINED FUEL OR PER GRAM OF
COMBINED OXIDANT

CLER TEMP
ADD ALL
THE FUEL
OR OXIDANT
PERCENTS
AND CONVR
TO FRACTNS

ARE PERCENT
REALLY
FRACTIONS

PERCENTS
OUT OF
LIMITS

LOCATE AND STORE THE REQUIRED
OXIDATION NUMBERS AND ATOMIC
WEIGHTS

CONSOLE POSITION 3 IS SET TO 8
IF IT IS DESIRED TO PUNCH OUT
ATOMIC WEIGHTS AND OXIDATION
NUMBERS

FIND ATOM
WEIGHT AND
OXID NO
OF COLUMN
ONE
ELEMENT

OXID NO

ATOMIC W
NEXT ELM

834	AR 1	RAA 0000			0973	80 0000	1329
835		RAB 0190			1329	82 0190	1085
836		RAC 0020	AR 2		1085	88 0020	1391
837	AR 2	SUP 8003			1391	11 8003	1149
838		STU TEMPO	AR 3	CLER TEMPO	1149	21 9000	1358
839	AR 3	RAU W0001 A		ATOMIC WT	1358	60 2340	1095
840		NZU	AR 4		1095	44 1199	0850
841		FMP F0001 B		ATOM COEFF	1199	39 4100	0950
842		FAD TEMPO		TEMPO HAS	0950	32 9000	1379
843		STU TEMPO		MOL WT	1379	21 9000	1237
844		AXA 0001			1237	50 0001	0943
845		AXB 0001			0943	52 0001	1249
846		SXA 0010			1249	51 0010	1408
847		NZA	AR 29		1408	40 1211	0862
848		AXA 0010	AR 3		1211	50 0010	1358
849	AR 29	AXA 0010	AR 4		0862	50 0010	0850
850	AR 4	RAU L0000 C		CALCULATE	0850	60 6299	1203
851		NZU	AR 30	NUMBER OF	1203	44 1458	1160
852		FDV TEMPO	AR 30	MOLES OF	1458	34 9000	1160
853	AR 30	STU N0000 C		EACH FUEL	1160	21 6359	0912
854		SXB 2010		OR OXIDANT	0912	53 2010	1319
855		BMB AR 5		WHICH GIVE	1319	43 0922	1023
856		RAA 0000		1 GRAM OF	1023	80 0000	1429
857		SXC 0001	AR 2	COMBINED	1429	59 0001	1391
858 1				FUEL AND 1 GRAM OF			
859 1				COMBINED OXIDANT			
860	AR 5	RAU 10051			0922	60 0524	1479
861		STU RELAY			1479	21 0016	1369
862		SET 9030			1369	27 9030	0724
863		LBB H0001		FUEL ENTH	0724	08 0320	1073
864		SET 9050			1073	27 9050	0778
865		LDR N0001		FUEL MOLES	0778	09 0360	1113
866		SET 9040		CLEAR 904	1113	27 9040	0718
867		LBB 0090		BAND	0718	08 0090	0993
868		RSA 0009			0993	81 0009	1299
869		RAB 0000			1299	82 0000	1210
870		RAC 0000	AR 6		1210	88 0000	1016
871	AR 6	SUP 8003			1016	11 8003	1123
872		STU TEMPO	AR 7	CLER TEMPO	1123	21 9000	1081
873	AR 7	RAU 9059 A		MOLES	1081	60 9259	1089
874		FMP F0001 B		ATOM COEFF	1089	39 4100	1000
875		FAD TEMPO			1000	32 9000	0930
876		STU TEMPO			0930	21 9000	1287
877		BMA	AR 8		1287	41 0940	1441
878		AXA 0001			0940	50 0001	0896
879		AXB 0010	AR 7		0896	52 0010	1081
880	AR 8	STU 9040 C		9040 TO	1441	21 9640	1349
881		RAU A0002 C		9049	1349	60 6002	1260
882		NZU	AR 9	CONTAIN	1260	44 1163	0814
883		RSA 0009		ATOMS PER	1163	81 0009	1419
884		SXB 0089		GRAM OF	1419	53 0089	1225
885		AXC 0001	AR 6	FUEL OR	1225	58 0001	1016
886 1				OXIDANT			
887	AR 9	SUP 8003			0814	11 8003	1421
888		STU TEMPO		CLER TEMPO	1421	21 9000	0980
889		STD TEMP1		CLER TEMP1	0980	24 9001	0836
890		STD TEMP2		CLER TEMP2	0836	24 9002	0992
891		RSA 0009	AR 10		0992	81 0009	0748
892	AR 10	RAU S0010 A			0748	60 2359	1213
893		FMP 9049 A		PLUS AND	1213	39 9249	1066
894		BMI	AR 11	MINUS	1066	46 1469	0570
895		FAD TEMP1		VALENCES	1469	32 9001	1399
896		STU TEMP1	AR 12	PER GRAM	1399	21 9001	1310
897	AR 11	FAD TEMPO		OF FUEL	0570	32 9000	1449
898		STU TEMPO	AR 12	OR OXIDANT	1449	21 9000	1310
899	AR 12	BMA	AR 13		1310	41 1263	0864
900		AXA 0001	AR 10		1263	50 0001	0748
901	AR 13	RSA 0009	AR 14		0864	81 0009	0720
902	AR 14	RAU 9059 A		ENTHALPY	0720	60 9259	0828
903		FMP 9039 A		PER GRAM	0828	39 9239	1131
904		FAD TEMP2		OF FUEL	1131	32 9002	1261
905		STU TEMP2		OR OXIDANT	1261	21 9002	0770
906		BMA	AR 15		0770	41 1173	0774
907		AXA 0001	AR 14		1173	50 0001	0720
908	AR 15	RAU RELAY			0774	60 0016	1471
909		NZU	PCH O		1471	44 1275	0976
910		STL RELAY	PCH F		1275	20 0016	0820
911	PCH F	SET 9040		PUNCH	0820	27 9040	1325
912		SBB 0587		ATOMS AND	1325	28 0587	0990
913		RAL SPEC1		ENTHALPY	0990	65 1043	0897
914		LDD	RMPCH	AND VALENC	0897	69 1050	1940
915		SET 9000		PER GRAM	1050	27 9000	1360
916		STB 0598		OF FUEL	1360	29 0598	1051
917		LDD TEMP2			1051	69 9002	1410
918		STD 0597			1410	24 0597	1100
919		RAL SPEC2			1100	65 1253	1460
920		LDD	RMPCH		1460	69 1313	1940

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921	SET	9030		OXIDANT	1313	27	9030	0768
922	LBB	E0001		ENTHALPIES	0768	08	0330	1083
923	SET	9050		OXIDANT	1083	27	9050	1088
924	LDR	N0011		MOLES	1088	09	0370	1223
925	SET	9040		CLEAR 904	1223	27	9040	0878
926	LBB	0090		BAND	0878	08	0090	1093
927	RSB	0009			1093	81	0009	1499
928	RAB	0100			1499	82	0100	1311
929	RAC	0000	AR 6		1311	88	0000	1016
930	PCH 0	SET	9040	PUNCH	0976	27	9040	1181
931	SBB	0537		ATOMS AND	1181	28	0537	1040
932	RAL	SPEC3		ENTHALPY	1040	65	1143	0947
933	LDD		RMPCH	AND VALENC	0947	69	1150	1940
934	SET	9000		PER GRAM	1150	27	9000	1361
935	STB	0548		OF OXIDANT	1361	29	0548	1101
936	LDD	TEMP2			1101	69	9002	1411
937	STD	0547			1411	24	0547	1200
938	RAL	SPEC4			1200	65	1303	1461
939	LDD	FINIS	RMPCH		1461	69	0914	1940
940 1				CONSTANTS FOR CALCULATING				
941 1				ROUTINE				
942 1								
943	MASK6	RAL	0000	MW 4	0584	65	0000	1308
944	MASK7	LDD	0000	MW 8	0872	69	0000	1153
945	47 I	00	0000	0047	1063	00	0000	0047
946	51 I	00	0000	0051	0843	00	0000	0051
947	200 D	00	0200	0000	0764	00	0200	0000
948	10053	10	0000	0053	1406	10	0000	0053
949	11051	11	0000	0051	0534	11	0000	0051
950	10051	10	0000	0051	0524	10	0000	0051
951	FINIS	HLT	9999	9999	0914	01	9999	9999
952	SPEC1	00	0587	0010	1043	00	0587	0010
953	SPEC2	00	0597	0003	1253	00	0597	0003
954	SPEC3	00	0537	0010	1143	00	0537	0010
955	SPEC4	00	0547	0003	1303	00	0547	0003
956 1								
957 1				ROCKET PACKAGE EXCERPT FOR				
958 1				VECTOR AND PROPELLANTS PROGRAM				
959 1								
960	BLA	1500	1999					
961	BLR	0000	1499					
962 1								
963 1				OUTPUT ROUTINE				
964 1				PUNCH BELL CARDS				
965 1								
966	REG	C9050	9050					
967	REG	J1991	1996					
968	REG	K1965	1970					
969	REG	P1977	1986					
970	SYN	J000N	1990					
971	SYN	PROB	1864					
972	EQU	LOC	0000					
973 1								
974	PUNCH	STD	LINK	START HERE	1930	24	0838	1541
975		LDD	8003		1541	69	8003	1548
976		SDA	C0005	1ST WORD	1548	22	9054	1504
977		SLT	0004		1504	35	0004	1515
978		SDA	C0006	NUMBER WDS	1515	22	9055	1522
979		SRT	0002		1522	30	0002	1529
980		RAU	8003		1529	60	8003	1537
981		SRT	0002		1537	30	0002	1543
982		SET	C0007		1543	27	9056	1598
983		LDD	WDCT6		1598	69	1501	1554
984		STD	P0009		1554	24	1985	1538
985		LDD	PROB		1538	69	1864	1517
986		STD	P0008		1517	24	1984	1587
987		LDD	C0005	PCH3	1587	69	9054	1593
988	PCH3	STD	P0007		1593	24	1983	1536
989		ALO	CARDN		1536	15	1539	1643
990		ALO	ONE D		1643	15	0516	1521
991		SDA	CARDN		1521	22	1539	1542
992		STL	P0010	NZERO	1542	20	1986	1589
993	NZERO	RAU	C0006		1589	60	9055	1547
994		SUP	WDCT6	IS NO OF	1547	11	1501	1505
995		BMI	LESS6	WORDS LESS	1505	46	1508	1509
996	PCH4	STU	C0006		1509	21	9055	1567
997		RAU	P0009		1567	60	1985	1639
998		SRT	0004		1639	30	0004	1549
999		AUP	XMOVE	SET TO MOV	1549	10	1502	1507
1000		ALO	XLOC	N WORDS	1507	15	1510	1565
1001		ALO	C0005	MOVEW	1565	15	9054	1523

1002	MOVEW	AUP	09999	8002		1523	10	1526	8002
1003	8002	LDD	LOC	8003		8002	69	0000	8003
1004	8003	STD	P0007	J000N		8003	24	1983	1990
1005	J0000	RAU	C0006	PCH2		1990	60	9055	1597
1006	J0001	RAU	C0006	PCH2		1991	60	9055	1597
1007	J0002	ALO	ONE D	MOVEW		1992	15	0516	1523
1008	J0003	ALO	ONE D	MOVEW		1993	15	0516	1523
1009	J0004	ALO	ONE D	MOVEW		1994	15	0516	1523
1010	J0005	ALO	ONE D	MOVEW		1995	15	0516	1523
1011	J0006	ALO	ONE D	MOVEW		1996	15	0516	1523
1012	PCH2	PCH	P0001			1597	71	1977	1527
1013		NZE		LINK	IS IT DONE	1527	45	1530	0838
1014		RAU	P0007			1530	60	1983	1637
1015		AUP	P0009			1637	10	1985	1689
1016		STU	C0005	PCH3		1689	21	9054	1593
1017	1								
1018	LESS6	RAL	C0006			1508	65	9055	1615
1019		STD	P0009			1615	24	1985	1588
1020		SRT	0004		CLEAR ZERO	1588	30	0004	1599
1021		ALO	XCLER	8002		1599	15	1552	8002
1022	8002	00	0000	K0001		8002	00	0000	1965
1023	K0001	STU	P0001	K0002		1965	21	1977	1966
1024	K0002	STU	P0002	K0003		1966	21	1978	1967
1025	K0003	STU	P0003	K0004		1967	21	1979	1968
1026	K0004	STU	P0004	K0005		1968	21	1980	1969
1027	K0005	STU	P0005	K0006		1969	21	1981	1970
1028	K0006	STU	P0006	PCH4		1970	21	1982	1509
1029	1								
1030	XCLER	00	0000	K0001		1552	00	0000	1965
1031	WDCT6	00	0006	0000		1501	00	0006	0000
1032	9999	00	0000	9999		1526	00	0000	9999
1033	XLOC	LDD	0000	8003		1510	69	0000	8003
1034	XMOVE	STD	P0000	J0001		1502	24	1976	1991
1035	CARDN	00	0000	0000		1539	00	0000	0000
1036	ONE D	00	0001	0000		0516	00	0001	0000
1037	1								
1038	1								
1039	1								
1040	1								
1041	1								
1042		REG	C9050	9050					
1043		REG	L1841	1844					
1044		REG	P1977	1986					
1045		REG	O1845	1845					
1046		SYN	LOC	0000					
1047	1								
1048	RMPCH	STD	LINK			1940	24	0838	1591
1049		LDD	8006		SAVE INDEX	1591	69	8006	1647
1050		STD	C0003		ACC B AND	1647	24	9052	1503
1051		LDD	8007		C	1503	69	8007	1559
1052		STD	C0004			1559	24	9053	1665
1053		RAC	8002		NO OF WDS	1665	88	8002	1573
1054	1								
1055		LDD	8003			1573	69	8003	1580
1056		SDA	C0005		1ST WORD	1580	22	9054	1586
1057		SLT	0004			1586	35	0004	1697
1058		SDA	C0006		NUMBER WDS	1697	22	9055	1604
1059		SRT	0002			1604	30	0002	1511
1060		RAU	8003			1511	60	8003	1519
1061		SRT	0002			1519	30	0002	1525
1062		SET	C0007			1525	27	9056	1630
1063		LBB	L0001		C0004 IS	1630	08	1841	1544
1064		STL	C0006		COL 80	1544	20	9055	1602
1065		RSB	0004		LOCATION	1602	83	0004	1558
1066		RAL	C0005			1558	65	9054	1715
1067		ALO	PCHX	ENT1	C0003 IS	1715	15	1518	1623
1068	ENT1	STL	C0005		CURRENT	1623	20	9054	1680
1069	1				LOCATION				
1070		ALO	XRAU	8002		1680	15	1533	8002
1071	8002	RAU	LOC	00001		8002	60	0000	1845
1072	00001	NZU	MOVER	C0007	C0007 HAS	1845	44	1649	9056
1073	1				L0001				
1074	L0001	SXC	0001			1841	59	0001	1747
1075		NZC		FINS		1747	48	1500	1551
1076		RAL	C0005			1500	65	9054	1557
1077		ALO	ONE D	ENT1		1557	15	0516	1623
1078	1								

/T#-E

UA-10 BACK

1079	MOVER	STD	P0005	B	MOVE WD	1649	24	5981	1534
1080		RAL	C0005			1534	65	9054	1641
1081		STD	P0010	B		1641	24	5986	1739
1082		NZB		PCH5	IS CARD	1739	42	1592	1693
1083		AXB	0001	C0007	FULL YET	1592	52	0001	9056
1084	PCH5	BMI		PLUS		1693	46	1546	1797
1085		SLO	C0006	BOTH	FIX COL 8	1546	16	9055	1553
1086	PLUS	ALO	C0006	BOTH		1797	15	9055	1553
1087	BOTH	STL	P0010			1553	20	1986	1789
1088		RAL	RMCDN		NUMBER CDS	1789	65	1642	1847
1089		ALO	ONE I			1847	15	1356	1561
1090		STL	RMCDN			1561	20	1642	1545
1091		LDD	P0009			1545	69	1985	1638
1092		SIA	P0009			1638	23	1985	1688
1093		PCW	P0001		PUNCH CARD	1688	71	1977	1577
1094		RSB	0004	C0008	C0008 HAS	1577	83	0004	9057
1095	L0002	STU	C0006	C0007	L0002	1842	21	9055	9056
1096	1								
1097	ONE D	00	0001	0000		0516	00	0001	0000
1098	ONE I	00	0000	0001	ONE INSTR	1356	00	0000	0001
1099	XRAU	59	9999	02001		1533	59	9999	3845
1100	PCHX	00	0000	8000		1518	00	0000	8000
1101	RMCDN	00	0000	0000	RANDOM CD	1642	00	0000	0000
1102	1				NUMBER				
1103	FINS	SET	C0007		CHANGE	1551	27	9056	1506
1104		LBB	L0003		ORDERS	1506	08	1843	1596
1105		RSL	PCHX		FOR FINS	1596	66	1518	1673
1106		STL	C0005	C0007		1673	20	9054	9056
1107	L0003	LDD	8003	MOVER		1843	69	8003	1649
1108	L0004	RAB	C0001		RESTOR	1844	82	9050	1652
1109		RAC	C0002	LINK	INDX ACC	1652	88	9051	0838
1110		PAT							

APPENDIX I

533 CONTROL PANEL ("ROCKET BOARD") WIRING INSTRUCTIONS

I. Read card C is used for reading Bell format cards. The word positions are numbered from the right (see 650 Manual of Operation, p. 10):

Read card C (card column)	Storage entry C	Word size entry C
11	Sign of word 1	
12-21	Word 1, positions 10 to 1	10
22	Sign of word 2	
23-32	Word 2, positions 10 to 1	10
33	Sign of word 3	
34-43	Word 3, positions 10 to 1	10
44	Sign of word 4	
45-54	Word 4, positions 10 to 1	10
55	Sign of word 5	
56-65	Word 5, positions 10 to 1	10
66	Sign of word 6	
67-76	Word 6, positions 10 to 1	10
6-9	Word 7, positions 8 to 5, emit sign +	8
5, 77-79	Word 8, positions 8 to 5, emit sign +	8
80, 1-4	Word 9, positions 9 to 5, emit sign +	9
10	Word 10, position 5, emit sign +; positions 4 to 1 of words 7, 8, 9, and 10 wired to emit zero	5

II. Read card B is used for reading Random location format cards:

Read card B (card column)	Storage entry B	Word size entry B
5-15	Word 1, positions 10 to 1, col. 15 is sign	10
20-30	Word 2, positions 10 to 1, col. 30 is sign	10
35-45	Word 3, positions 10 to 1, col. 45 is sign	10
50-60	Word 4, positions 10 to 1, col. 60 is sign	10
65-75	Word 5, positions 10 to 1, col. 75 is sign	10
1-4	Word 6, positions 8 to 5, emit sign +	8
16-19	Word 7, positions 8 to 5, emit sign +	8
31-34	Word 8, positions 8 to 5, emit sign +	8
46-49	Word 9, positions 8 to 5, emit sign +	8
61-64	Co-selector 1 transferred points (U, 1 to 4)(make col. 61 a split wire. p. 119)	
76-80	Not wired Words 6 to 9 emit zero into positions 4 to 1	

Selector wiring for determining and entering the word count in word 10 and ensuring that word 10 is a legitimate word is as follows:

Co-selector 1 common (W, 1 to 4) to word 10, positions 8 to 5
storage entry B

Word size of word 10. entry B is 8

Co-selector 1 normal (V, 1 to 4), to (V, 32). (This guarantees a nonzero value on word 10 to preserve the negative sign for a branch on minus test.)

Emit zeros to word 10, positions 4 to 2, storage entry B

Emit sign of word 10 minus (V, 28)

Pilot selector 1 common (K, 23) to word 10, position 1, storage entry B

Pilot selector 1 normal (J, 23) to emit zero

Pilot selector 1 transferred (H, 23) to pilot selector 2 common (K, 24)

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Pilot selector 2 transferred (H, 24) to pilot selector 3 common
 (K, 25)
 Pilot selector 3 normal (J, 25) to emit 2 (W, 21)
 Pilot selector 3 transferred (H, 25) to pilot selector 4 common
 (K, 26)
 Pilot selector 4 normal (J, 26) to emit 3 (X, 21)
 Pilot selector 4 transferred (H, 26) to pilot selector 5 common
 (K, 27)
 Pilot selector 5 normal (J, 27) to emit 4 (Y, 21)
 Pilot selector 5 transferred (H, 27) to emit 5 (Z, 21)
 Pilot selector 2 normal (J, 24) to emit 1 (V, 21)
 First reading col. 1 (A, 23) to load (B, 21)
 First reading col. 1 (A, 23) to common of col. split } split wire
 (Z, 34)
 Col. split 0-9 (Y, 34) to D pick pilot selector 1 (F, 23)

 Co-selector 3 pick (R, 25) to col. split 12-X (X, 34)
 Co-selector 3 common (W, 11) to emit 9 (W, 34)
 Co-selector 3 transfer (U, 11) to entry B (D, 21)

 First reading col. 16 (A, 38) to D pick pilot selector 2
 (F, 24)
 First reading col. 31 (C, 33) to D pick pilot selector 3
 (F, 25)
 First reading col. 46 (C, 28) to D pick pilot selector 4
 (F, 26) (Split wire, p. 120)
 First reading col. 61 (D, 23) to D pick pilot selector 5
 (F, 27)
 Couple pilot selector 5 (G, 27) to co-selector pickup 1
 (S, 23)

 Digit impulse (Q, 21) to digit selector common (R, 21)
 First reading col. 15 (A, 37) to col. split 12-X (X, 33)
 Col. split common (Z, 33) to entry B (D, 22)

Hold for pilot selectors 1 to 5 (P, 23 to 27) and co-selectors 1 and 3 (U, 23 and 25) are wired to read hold (T, 39).

III. Read card A is used to read input cards (SOAP II format) for Vector and Propellant Program (requires the alphabetic attachment and pilot selectors 11, 12, 13):

First reading col. 3 (A, 25) to col. split common (Z, 35)
 Col. split 12-X (X, 35) to entry A (C, 22)
 Entry A (C, 23) to pilot selector 12-X pick (E, 34)
 Pilot selector 12 couple exit (G, 34) to alphabetic control WI
 (AL, 12) and also to W2 to W6.

Storage entry A, word 10, position 3 (J, 19) to pilot selector 13 common (K, 35)

Pilot selector 13 normal (J, 35) to zero read impulse (AN, 20)

Pilot selector 13 transfer (H, 35) to read card A, col. 41 (C, 1)

Pilot selector 13 D pick (F, 35) to first reading col. 41 (C, 23)

Storage entry A, word 10, position 2 (J, 20) to pilot selector 13 common (N, 35)

Pilot selector 13 normal (M, 35) to zero read impulse (AP, 20)

Pilot selector 13 transfer (L, 35) to read impulse 9 (V, 34)

Storage entry A, word 10, position 1 (J, 21) to pilot selector 11 common (N, 33)

Pilot selector 11 normal (M, 33) to zero read impulse (AP, 21)

Pilot selector 11 transfer (L, 33) to read impulse 8 (V, 33)

Pilot selector 11 D pick (F, 33) to first reading, col. 42 (C, 24)

Read card A, col. 43 (C, 3) to storage entry A, word 1, position 5 (E, 6)

Read card A, col. 44 to 47 (C, 4 to 7) split wire to word 1, positions 4 to 1 (E, 7 to 10) and to word 7, positions 4 to 1 (H, 7 to 10)

Read card A, col. 48 to 50 (C, 8 to 10) to word 4, positions 5 to 3 (F, 17 to 19)

Read card A, col. 51 (C, 11) to word 2, position 5 (E, 17)

Read card A, col. 52 to 55 (C, 12 to 15) split wire to word 2, positions 4 to 1 (E, 18 to 21) and to word 8, positions 4 to 1 (H, 18 to 21)

Read card A, col. 56 (C, 16) to word 4, position 2 (F, 20)

Read card A, col. 57 (C, 17) to word 3, position 5 (F, 6)

Read card A, col. 58 to 61 (C, 18 to D, 1) split wire to word 3, positions 4 to 1 (F, 7 to 10) and to word 9, positions 4 to 1 (J, 7 to 10)

Read card A, col. 62 (D, 2) to word 4, position 1 (F, 21)

Read card A, col. 63 to 67 (D, 3 to 7) to word 5, positions 5 to 1 (G, 6 to 10)

Read card A, col. 68 to 72 (D, 8 to 12) to word 6, positions 5 to 1 (G, 17 to 21)

First reading, col. 43 to 47 (C, 25 to 29) to alphabetic first read, word 1, positions 5 to 1 (AK, 13 to 17)

Col. 48 to 50 (C, 30 to 32) to alphabetic first read, word 4, positions 5 to 3 (AL, 18 to 20)

Col. 51 to 55 (C, 33 to 37) to alphabetic first read, word 2, positions 5 to 1 (AK, 18 to 22)

Col. 56 (C, 38) to alphabetic first read, word 4, position 2 (AL, 21)

Col. 57 to 61 (C, 39 to D, 23) to alphabetic first read, word 3, positions 5 to 1 (AL, 13 to 17)

Col. 62 (D, 24) to alphabetic first read, word 4, position 1 (AL, 22)

Col. 63 to 67 (D, 25 to 29) to alphabetic first read, word 5, positions 5 to 1 (AM, 13 to 17)

Col. 68 to 72 (D, 30 to 34) to alphabetic first read, word 6, positions 5 to 1 (AM, 18 to 22)

Read validity check wire off (AR, 43) to (AR, 44)
 Chain wire pilot selector hold of pilot selectors 11, 12, and 13
 (P, 33 to 35) to read hold (T, 39)
 Word size entry A, words 7 to 9 (AL, 7 to 9) to word size emitter 4
 (AK, 5)
 Word size entry A, word 10 (AL, 10) to word size emitter 3 (AK, 4)

IV. Punch card C is used to punch Bell format cards and Trace format cards:

Punch card C (card column)	Storage exit C
11	Sign of word 1
12-21	Word 1, positions 10 to 1
22	Sign of word 2
23-32	Word 2, positions 10 to 1
33	Sign of word 3
34-43	Word 3, positions 10 to 1
44	Sign of word 4
45-54	Word 4, positions 10 to 1
55	Sign of word 5
56-65	Word 5, positions 10 to 1
66	Co-selector 7 common (W, 59) Co-selector 7 normal (V, 59) to word 6 sign (AG, 64)(Split wire, see Trace cards)
67	Word 6, position 10
68-72	Co-selectors 6 and 7 common (W, 54 to 58) Co-selectors 6 and 7 normal (W, 54 to 58) to word 6, positions 9 to 5
73-76	Word 6, positions 4 to 1
6-9	Co-selector 6 common (W, 50 to 53) Co-selector 6 normal (V, 50 to 53) to word 7, positions 8 to 5
5, 77-79	Word 8, positions 8 to 5
10	Word 9, position 5
80, 1-4	Word 10, positions 9 to 5

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For Trace cards:

Co-selector 6 transfer (U, 50 to 53) to word 7, positions 4 to 1

Co-selectors 6 and 7 transfer (U, 54 to 57) to word 8, positions
4 to 1

Co-selector 7 transfer (U, 58) to word 6, sign position

Co-selector 7 transfer (U, 59) to word 8, sign position

An 8 in position 9 of word 10 causes Trace cards to be punched by
means of control information:

Control information (AM, 56) to co-selectors 6 and 7 pick (R, 28,
29)

Co-selectors 6 and 7 hold (T, 28, 29) to punch hold (R, 39)

Jack plug "P+" (V, 42) to (W, 42)

V. Punch card B is used to punch Random location cards:

Punch card B (card column)	Storage exit B
5-15	Word 1, positions 10 to 1, col. 15 is sign
20-30	Word 2, positions 10 to 1, col. 30 is sign
35-45	Word 3, positions 10 to 1, col. 45 is sign
50-60	Word 4, positions 10 to 1, col. 60 is sign
65-75	Word 5, positions 10 to 1, col. 75 is sign
1	Pilot selector 6 common (K, 28) Pilot selector 6 normal (J, 28) to word 6, position 8
2-4	Word 6, positions 7 to 5
16	Pilot selector 7 common (K, 29) Pilot selector 7 normal (J, 29) to word 7, position 8
17-19	Word 7, positions 7 to 5
31	Pilot selector 8 common (K, 30) Pilot selector 8 normal (J, 30) to word 8, position 8
32-34	Word 8, positions 7 to 5
46	Pilot selector 9 common (K, 31) Pilot selector 9 normal (J, 31) to word 9, position 8
47-49	Word 9, positions 7 to 5
61	Pilot selector 10 common (K, 32) Pilot selector 10 normal (J, 32) to word 10, position 8
62-64	Word 10, positions 7 to 5
76-79	Word 9, positions 4 to 1
80	Word 10, position 9

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CA-16 back

Pilot selector 6 I pick (G, 28) to sign word 6
Pilot selector 7 I pick (G, 29) to sign word 7
Pilot selector 8 I pick (G, 30) to sign word 8
Pilot selector 9 I pick (G, 31) to sign word 9
Pilot selector 10 I pick (G, 32) to sign word 10
Co-selector 2 pick (R, 24) to punch X impulse (A, 43)
Co-selector 2 common (W, 6) to punch hold (R, 39)
Co-selector 2 transferred (U, 6) split wire to transfer of pilot
selectors 6 to 10 inclusive (L, 28 to 32)
Pilot selectors 6 to 10 common (N, 28 to 32) to pilot selector
hold 6 to 10 (Q, 28 to 32)
Co-selector 2 hold (T, 24) to punch hold (S, 39)
Control information 4 (AK, 61) to punch E (D, 43)

VI. Punch card A is used to punch SOAP II format cards:

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Punch card A (card column)	Storage exit A
1	Col. split common (AM, 52) Col. split 0-9 (AL, 52) to emit 6 (AA, 43) Col. split 12-X (AK, 52) to emit 12 (S, 43); Wire DI (Q, 43) to common (R, 43)
2-6	Emit 9,1,9,5,4, respectively, from punch emitter
7-10	Co-selector 5 common positions 4 to 1 (W, 46 to 49) Co-selector 5 normal positions 4 to 2 (V, 46 to 48) to emit 1,9,5, respectively, from punch emitter Co-selector 5 normal position 1 (V, 49) to col. split common (AM, 45) Col. split 0-9 (AL, 45) to emit 3 Col. split 12-X (AK, 45) to emit 12 (S, 43) Co-selector 5 transfer positions 4 to 2 (U, 46 to 48) to emit 8,0,0, respectively Co-selector 5 transfer position 1 (U, 49) to col. split common (AM, 46) Col. split 0-9 (AL, 46) to emit 3 Col. split 12-X (AK, 46) to emit 12 (S, 43)
11-20	Word 9, positions 10 to 1, wire sign of word 9 to col. 20 with col. split (AM, 47)
21	Emit 2
22	Emit 4
23-26	Word 8, positions 8 to 5
27-29	Emit 8,0,0, respectively
30	Col. split common (AM, 48) Col. split 0-9 (AM, 48) to emit 0 Col. split 12-X (AM, 48) to emit 12
31-40	Word 7, positions 10 to 1, wire sign through col. split to col. 40 and 42
41	Word 8, position 1
42	Sign of word 7
43-47	Word 1, positions 5 to 1
48-50	Word 4, positions 5 to 3
51-55	Word 2, positions 5 to 1
56	Word 4, position 2
57-61	Word 3, positions 5 to 1
62	Word 4, position 1
63-67	Word 5, positions 5 to 1
68-72	Word 6, positions 5 to 1

Control information 2 (AK, 63) to co-selector 5 pick (R, 27)
 Control information 3 (AK, 62) to Alpha cut W1 and also chain wire
 to W2, W3, W4, W5, and W6
 3 (AL, 62) to Punch A (C, 43)
 Co-selector 5 hold (T, 27) to punch hold (R, 40)

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TABLE I. - COEFFICIENTS FOR OBTAINING THERMODYNAMIC DATA FOR SEVERAL SUBSTANCES
[Coefficients for use in equations (105) to (107).]

Sub- stance (a)	Temperature Interval, °K	Coefficients					
		A	B	C	D	E	F
C	150 - 300	+2527 8238 51	+1867 6400 47	-2011 9997 45	+3832 8460 42	+1318 3612 56	+4598 3693 51
	300 - 500	+2511 0512 51	+2341 2431 46	-2064 1813 44	+2504 6361 41	+1318 3951 56	+4694 0319 51
	500 - 700	+2505 9144 51	+1127 9624 46	-6304 0443 43	+5333 3424 40	+1318 4070 56	+4722 3131 51
	700 - 1000	+2503 4230 51	+5325 3290 45	-2160 0382 43	+1354 8725 40	+1318 4156 56	+4737 1984 51
	1000 - 1300	+2503 2775 51	+5521 0150 45	-1695 7438 43	+8055 6245 39	+1318 4123 56	+4737 2493 51
	1300 - 1700	+2504 6546 51	+9314 6910 45	-2465 5314 43	+1190 5488 40	+1318 3969 56	+4726 7149 51
	1700 - 2100	+2501 5285 51	+5907 5500 45	-1820 8474 43	+9928 4700 39	+1318 4349 56	+4749 6818 51
	2100 - 2600	+2488 4570 51	-1345 7700 44	+8780 3410 42	+2879 3181 39	+1318 6460 56	+4852 5918 51
	2600 - 3200	+2472 3653 51	-4335 7912 46	+3975 0497 43	-3693 3212 39	+1319 0115 56	+4990 6948 51
	3200 - 3800	+2476 2539 51	-6493 0882 46	+5315 2588 43	-5893 7109 39	+1319 1045 56	+4983 7555 51
	3800 - 4400	+2504 1340 51	-7041 0160 46	+5063 4142 43	-5359 6037 39	+1318 6229 56	+4783 1816 51
	4400 - 5000	+2546 5888 51	-6519 6370 46	+4555 2568 43	-4063 3061 39	+1317 6142 56	+4455 1751 51
5000 - 6000	+2610 4540 51	-4741 7690 46	+2664 8172 43	-2304 4960 39	+1315 6607 56	+3935 3511 51	
Graphite	300 - 500	+5673 0710 50	-2106 2241 48	+1744 0045 46	-1691 9439 43	+4619 0744 55	-2545 1750 51
	500 - 700	+1058 3269 51	-2054 1842 48	+1091 7536 46	-7970 7376 42	+4607 1927 55	-5175 2399 51
	700 - 1000	+1628 3807 51	-1307 2653 48	+5023 1415 45	-2756 8704 42	+4584 8409 55	-8591 5430 51
	1000 - 1300	+2289 3860 51	-3947 4982 47	+9829 2657 44	-2901 7625 41	+4546 1211 55	-1287 2246 52
	1300 - 1700	+2407 1476 51	-4784 1780 47	+1008 1106 45	-3136 4202 41	+4537 7132 55	-1561 1939 52
	1700 - 2100	+2709 5422 51	-2313 1973 47	+3670 0610 44	-8357 2671 40	+4507 5530 55	-1573 1714 52
	2100 - 2600	+2841 4329 51	-1619 7368 47	+2059 3854 44	-3684 0068 40	+4491 5653 55	-1667 5173 52
	2600 - 3200	+2958 2033 51	-1146 5505 47	+1154 2930 44	-1567 2361 40	+4474 0549 55	-1753 4691 52
	3200 - 3800	+3040 3247 51	-9509 5528 46	+7614 5316 43	-7812 3581 39	+4460 0657 55	-1814 4793 52
	3800 - 4400	+3097 3807 51	-9187 9709 46	+6184 4345 43	-5311 4558 39	+4449 1831 55	-1856 9802 52
	4400 - 5000	+3152 7766 51	-8885 2831 46	+5138 2079 43	-3740 3250 39	+4436 8642 55	-1899 1194 52
	CCl	150 - 300	+3820 3364 51	+4255 4820 47	-7410 0490 45	+2285 0707 43	+1092 3347 56
300 - 500		+3693 1871 51	-9241 6910 47	-7775 5823 45	-8061 9700 42	+1092 5828 56	+6074 2136 51
500 - 700		+3912 5706 51	-7820 0920 47	+4222 7425 45	-3279 9984 42	+1092 0413 56	+4884 6073 51
700 - 1000		+4115 6696 51	-4342 0958 47	+1693 5722 45	-9680 7557 41	+1091 2721 56	+3666 0743 51
1000 - 1300		+4271 6614 51	-2203 0847 47	+6118 7076 44	-2567 6708 41	+1090 4684 56	+2678 1140 51
1300 - 1700		+4378 2291 51	-9382 1810 46	+1978 6630 44	-6167 2272 40	+1089 6529 56	+1956 5236 51
1700 - 2100		+4428 6744 51	-5606 4340 46	+9129 2970 43	-2231 4653 40	+1089 1732 56	+1606 6487 51
2100 - 2600		+4461 6643 51	-3393 9946 46	+4422 3777 43	-8479 8548 39	+1088 7729 56	+1368 9058 51
2600 - 3200		+4466 6128 51	-2289 1842 46	+2381 7346 43	-3571 2362 39	+1088 4376 56	+1199 9462 51
3200 - 3800		+4500 1739 51	-1781 1588 46	+1497 8228 43	-1797 2303 39	+1088 1620 56	+1079 4739 51
3800 - 4400		+4513 7299 51	-1439 9338 46	+1005 6037 43	-7752 0000 38	+1087 8935 56	+9798 2788 50
4400 - 5000		+4522 5949 51	-1319 2912 46	+7941 9120 42	-6609 4577 38	+1087 6927 56	+9117 3280 50
5000 - 6000	+4532 7490 51	-1122 4142 46	+5808 8556 42	-3943 1880 38	+1087 4110 56	+8309 5849 50	
CCl ₄	150 - 300	+6883 4230 51	-2183 6856 49	+2209 0207 47	-3765 2673 44	+4132 9670 55	-2005 0830 51
	300 - 500	+6534 3172 51	-7160 8000 48	+6201 5460 46	-7111 6167 43	+4098 5503 55	-1142 3036 52
	500 - 700	+1008 7133 52	-4760 2740 48	+2629 9117 46	-2170 8108 43	+4062 5210 55	-1986 7563 52
	700 - 1000	+1120 9988 52	-2287 4058 48	+9007 1820 45	-5425 6390 42	+4022 5045 55	-2659 6737 52
	1000 - 1300	+1195 6348 52	-1043 2162 48	+2943 6828 45	-1282 6918 42	+3986 5351 55	-3131 0836 52
	1300 - 1700	+1248 4721 52	-3391 1184 47	+7258 7051 44	-2338 0965 41	+3945 8748 55	-3490 8748 52
	1700 - 2100	+1268 0666 52	-1729 2303 47	+2873 9710 44	-7327 1794 40	+3926 8367 55	-3627 8094 52
	2100 - 2600	+1279 3339 52	-8857 1920 46	+1192 5272 44	-2449 6562 40	+3912 7677 55	-3709 6952 52
	2600 - 3200	+1286 1578 52	-4880 6790 46	+5345 6302 43	-8955 1435 39	+3902 3779 55	-3760 5577 52
	3200 - 3800	+1290 2043 52	-3013 4232 46	+2724 8863 43	-3823 5766 39	+3895 0427 55	-3791 3780 52
	3800 - 4400	+1292 8751 52	-1886 0004 46	+1451 7234 43	-7752 0000 38	+3889 1827 55	-3812 2942 52
	4400 - 5000	+1294 5807 52	-1253 5153 46	+8422 0090 42	-8623 9152 38	+3884 8198 55	-3825 9243 52
5000 - 6000	+1296 2205 52	-6498 6420 45	+3820 8266 42	-3347 9564 38	+3879 6914 55	-3839 4390 52	
CF	150 - 300	+3640 0200 51	+8085 8640 47	-1026 9011 46	+2438 4900 43	+1940 6783 56	+4867 6076 51
	300 - 500	+3498 5413 51	-4528 6370 47	+3399 6376 45	-1921 1982 42	+1940 9729 56	+5674 6721 51
	500 - 700	+3597 7497 51	-8040 8130 47	+4156 7731 45	-2824 2658 42	+1940 7415 56	+5176 7255 51
	700 - 1000	+3810 1072 51	-6268 2490 47	+2385 5288 45	-1274 7825 42	+1940 9158 56	+4918 2736 51
	1000 - 1300	+4048 2657 51	-3885 1238 47	+1061 8631 45	-4275 8782 41	+1940 6368 56	+2414 2551 51
	1300 - 1700	+4225 0270 51	-2089 1357 47	+4374 3033 44	-1339 8215 41	+1940 2978 56	+1226 0050 51
	1700 - 2100	+4334 2200 51	-1335 6403 47	+2161 7485 44	-5212 2758 40	+1940 2672 56	+4713 8170 50
	2100 - 2600	+4441 7942 51	-8377 5910 46	+1084 3361 44	-2048 7978 40	+1940 3278 56	-8671 8950 49
	2600 - 3200	+4467 8185 51	-5822 8670 46	+6020 0162 43	-8903 5200 39	+1940 5100 56	-4985 2010 50
	3200 - 3800	+4508 2460 51	-4630 6640 46	+3870 6023 43	-6584 6109 39	+1940 5100 56	-8000 8070 50
	3800 - 4400	+4541 0295 51	-3813 2379 46	+2644 8087 43	-2522 3761 39	+1940 1526 56	-1050 5867 51
	4400 - 5000	+4569 6116 51	-3184 7846 46	+1851 2604 43	-1379 0052 39	+1940 4685 56	-1273 6745 51
5000 - 6000	+4608 1204 51	-2076 7807 46	+9178 6561 42	-2634 8774 38	+1940 3042 56	-1586 8660 51	
CF ₂	150 - 300	+4048 5275 51	-2616 5412 48	+2155 9933 46	-2058 6114 43	+6584 7865 55	+5829 4252 51
	300 - 500	+4074 4857 51	-2459 6320 48	+2064 6571 46	-1981 1983 43	+6584 1442 55	+5680 2914 51
	500 - 700	+4691 9175 51	-2394 9638 48	+1263 9499 46	-9151 9648 42	+6568 6792 55	+2347 8274 51
	700 - 1000	+5409 6786 51	-1408 4350 48	+5348 7413 45	-2842 5180 42	+6539 7513 55	+1879 9085 51
	1000 - 1300	+6025 9535 51	-7504 6540 48	+2030 6869 45	-7987 0809 41	+6504 7319 55	+5917 2859 51
	1300 - 1700	+6398 7799 51	-3929 7130 47	+8155 2021 44	-2451 9736 41	+6475 5249 55	-8433 7760 51
	1700 - 2100	+6662 6054 51	-2224 2198 47	+3543 7494 44	-8257 7665 40	+6450 9950 55	-1013 7338 52
	2100 - 2600	+6788 3007 51	-1372 2122 47	+1756 5186 44	-3252 3470 40	+6432 4476 55	-1119 1218 52
	2600 - 3200	+6891 2452 51	-9243 3170 46	+9493 4160 43	-6591 8731 39	+6416 6267 55	-1195 3073 52
	3200 - 3800	+6967 1014 51	-6796 6480 46	+5630 0065 43	-1396 0756 40	+6402 7074 55	-1252 6276 52
	3800 - 4400	+7021 0652 51	-5466 6732 46	+3777 3931 43	-3621 0579 39	+6390 9978 55	-1294 2206 52
	4400 - 5000	+7058 0449 51	-4920 3790 46	+2933 2725 43	-2418 8941 39	+6382 1426 55	-1322 8904 52
5000 - 6000	+7097 4438 51	-4178 3006 46	+2148 5733 43	-1461 5182 39	+6370 9039 55	-1354 3379 52	
CF ₃	150 - 300	+4415 9046 51	-1079 2001 49	+1028 9803 47	-1547 4411 44	+3294 5442 55	+6322 6310 51
	300 - 500	+6995 4769 51	+6890 2840 48	-6064 6113 46	+9838 4060 43	+3233 5181 55	-8614 0409 51
	500 - 700	+1340 4500 50	-2596 2896 49	+1511 2585 47	-1367 1095 44	+3485 6118 55	+3544 3864 52
	700 - 1000	+6412 2822 51	-5167 3100 48	+2151 1245 46	-1307 2694 43	+3257 6653 55	-4378 9501 51
	1000 - 1300	+7725 6912 51	-2967 7290 48	+8838 4890 45	-3912 9278 42	+3209 7765 55	-1236 8123 52
	1300 - 1700	+9068 6613 51	-1109 7817 48	+2576 9457 45	-8070 0746 41	+3114 9770 55	-2139 6277 52
	1700 - 2100	+9582 7034 51	-6851 8810 47	+1229 5950 45	-2863 4956 41	+3061 1725 55	-2559 1310 52
	2100 - 2600	+1013 8660 52	-4418 4184 47	+6387 7821 44	-1094 2288 41	+3008 1267 55	-2883 3689 52
	2600 - 3200	+1047 7649 52	-3606 9383 47	+4132 9340 44	-5398 9138 40	+2961 3360 55	-3127 2861 52
	3200 - 3800	+1076 8882 52	-3381 4409 47	+3076 1815 44	-3205 5653 40	+2914 5240 55	-3350 4045 52
	3800 - 4400	+1102 5318 52	-3277 2624 47	+2461 8412 44	-2128 3409 40	+2865 7705 55	-3530 0856 52
	4400 - 5000	+1125 0822 52	-3285 3329 47	+2101 1199 44	-1569 0770 40	+2817 3513 55	-3699 8762 52
5000 - 6000	+1150 6199 52	-3117 8637 47	+1722 3104 44	-1082 7473 40	+2750 5776 55	-3898 6721 52	
CF ₄	150 - 300	+4643 8961 51	-1683 7831 49	+1601 9450 47	-2396 9562 44	-1014 9484 54	+5178 0680 51
	300 - 500	+5623 0578 51	-8719 8704 48	+7316 1903 46	-7405 1763 43	-1222 0906 54	-3985 7300 50
	500 - 700	+7960 4636 51	-6242 2794 48	+3262 8202 46	-2359 3972 43	-1831 2412 54	-1328 2457 50

TABLE I. - Continued. COEFFICIENTS FOR OBTAINING THERMODYNAMIC DATA FOR SEVERAL SUBSTANCES

Coefficients for use in equations (105) to (107)

Sub- stance (a)	Temperature Interval, °K	Coefficients					
		A	B	C	D	E	F
CH	150 - 300	+3512 7827 51	+4636 0810 46	-5378 9030 44	-1346 7447 42	+1344 6458 56	+1985 4362 51
	300 - 500	+3518 9332 51	+8459 4710 46	-9090 7610 44	+1731 4444 42	+1344 6317 56	+1950 3265 51
	500 - 700	+3488 5177 51	+341 9700 46	-1474 4120 44	+9635 7372 41	+1344 7464 56	+2140 1459 51
	700 - 1000	+3400 5554 51	-5633 2938 47	+1934 0930 45	-6925 5161 41	+1345 2502 56	+2759 7067 51
	1000 - 1300	+3525 5707 51	-8199 6840 47	+2173 4717 45	-8003 0457 41	+1344 7547 56	+2069 0007 51
	1300 - 1700	+3837 6747 51	-6520 0620 47	+1371 1096 45	-4245 5102 41	+1342 4710 56	+1564 5000 49
	1700 - 2100	+4192 6268 51	-4067 2700 47	+6710 9154 44	-1698 9191 41	+1339 0392 56	-2447 1172 51
	2100 - 2600	+4465 9529 51	-2009 4469 47	+2655 2706 44	-3294 6864 40	+1335 5954 56	-4436 8745 51
	2600 - 3200	+4632 7107 51	-9757 7450 46	+9834 5740 43	-1342 4002 40	+1333 0453 56	-5683 3608 51
	3200 - 3800	+4698 1775 51	-7731 9680 46	+5967 1047 43	-5314 9447 39	+1332 0116 56	-6167 1269 51
	3800 - 4400	+4702 1190 51	-1030 5653 47	+7078 9557 43	-6530 3692 39	+1332 3200 56	-6159 8416 51
	4400 - 5000	+4683 7437 51	-1461 5449 47	+9345 2350 43	-9239 1545 39	+1333 4036 56	-6958 5943 51
	5000 - 6000	+4705 6474 51	-1610 6331 47	+9697 4750 43	-9522 1104 39	+1333 1471 56	-6102 7716 51
CH ₄	150 - 300	+4041 7634 51	+2256 4400 47	-8630 3440 45	+3562 1920 43	+1060 6422 56	-6347 7250 50
	300 - 500	+3771 6119 51	-1914 0720 48	+1386 0780 46	-5564 2687 42	+1061 2254 56	+0066 3870 50
	500 - 700	+4137 3746 51	-3824 2483 48	+1900 8319 46	-1114 4742 43	+1060 5115 56	-8222 8700 50
	700 - 1000	+4960 9077 51	-3993 5554 48	+1469 0695 46	-7032 1339 42	+1057 6295 56	-5511 1720 51
	1000 - 1300	+6265 1238 51	-3554 3046 48	+9493 8230 45	-3578 7489 42	+1051 0805 56	-1351 2328 52
	1300 - 1700	+7669 6463 51	-2559 0212 48	+5320 7298 45	-1596 8105 42	+1040 8233 56	-2280 0662 52
	1700 - 2100	+8940 9968 51	-1821 1267 48	+2963 0253 45	-7240 8212 41	+1028 9929 56	-3153 5615 52
	2100 - 2600	+9999 5267 51	-1151 4294 48	+1572 5193 45	-3042 8540 41	+1015 9947 56	-3915 9002 52
	2600 - 3200	+1082 7726 52	-7167 4950 47	+7704 7857 44	-1264 4178 41	+1003 5136 56	-4530 1437 52
	3200 - 3800	+1159 5575 52	-4744 1100 47	+4206 8772 44	-3793 1231 40	+9932 4942 55	-4961 4187 52
	3800 - 4400	+1178 8522 52	-2183 3398 47	+2393 0379 44	-2833 1861 40	+9846 8258 55	-5268 2486 52
	4400 - 5000	+1205 5418 52	-2229 3658 47	+1456 2454 44	-1310 1845 40	+9779 0774 55	-5481 0165 52
	5000 - 6000	+1232 4498 52	-1249 1856 47	+7039 3966 43	-6132 1844 39	+9695 2767 55	-5702 5529 52
CO	150 - 300	+3501 4842 51	+1087 8922 46	-2132 6547 44	+7176 7187 41	+3308 4242 55	+3809 0776 51
	300 - 500	+3504 8282 51	+5717 3880 46	-7717 9140 44	+1948 0969 42	+3308 3690 55	+3790 2032 51
	500 - 700	+3547 2625 51	-2833 6849 47	+1252 0307 45	-3548 5188 41	+3310 1729 55	+4099 1993 51
	700 - 1000	+3478 1473 51	-5369 0403 47	+1958 1791 45	-9091 0461 41	+3310 1638 55	+4029 9306 51
	1000 - 1300	+3651 5834 51	-5144 8902 47	+1380 4870 45	-5272 8366 41	+3301 4098 55	+2971 0270 51
	1300 - 1700	+3860 8374 51	-3546 9532 47	+7404 9426 44	-9678 6685 40	+3269 0418 55	+3411 6830 50
	1700 - 2100	+4040 9776 51	-2413 3244 47	+3930 0638 44	-1948 8754 40	+3251 7557 55	-6791 5710 50
	2100 - 2600	+4182 5494 51	-1491 5448 47	+1948 8754 40	-3880 7574 40	+3235 9292 55	-1463 2026 51
	2600 - 3200	+4288 4419 51	-9428 1210 46	+1001 4612 44	-1595 1818 40	+3222 2132 55	-2039 2716 51
	3200 - 3800	+4364 4008 51	-6326 1270 46	+5453 3767 43	-7027 3322 39	+3210 1502 55	-2466 3384 51
	3800 - 4400	+4419 2221 51	-4399 2938 46	+3153 4215 43	-3308 2674 39	+3200 9544 55	-2753 9920 51
	4400 - 5000	+4455 6250 51	-3418 0326 46	+2087 5301 43	-1819 9816 39	+3190 9734 55	-3024 6520 51
	5000 - 6000	+4489 0699 51	-2554 6512 46	+1323 6630 43	-9051 5936 38	+3190 9734 55	-3024 6520 51
CO ₂	150 - 300	+3563 7140 51	+4925 8570 48	+5440 0397 46	-6280 3430 43	+5747 4400 51	+5400 7202 51
	300 - 500	+3816 8846 51	-2963 9146 48	+2490 7914 46	-2567 1204 43	+4925 1570 52	+3956 7791 51
	500 - 700	+4442 4313 51	-2696 4402 48	+1430 5622 46	-1054 0891 43	+1901 0823 53	+6296 7070 50
	700 - 1000	+5077 4390 51	-1862 6330 48	+7097 4891 45	-3796 3466 42	+1495 9603 53	+3119 0925 51
	1000 - 1300	+5616 2514 51	-1446 4518 48	+3992 8749 45	-1646 2220 42	+1469 3300 53	-6421 4910 51
	1300 - 1700	+6233 4300 51	-7697 1330 47	+1624 9078 45	-5067 2175 41	+1123 1588 54	-1056 0477 52
	1700 - 2100	+6563 7140 51	-4526 7290 47	+7359 4847 44	-1790 7679 41	+1524 1600 54	-1347 7832 52
	2100 - 2600	+6946 1749 51	-2588 8848 47	+3382 8632 44	-6523 5648 40	+1891 5354 54	-1559 6591 52
	2600 - 3200	+7139 6491 51	-1643 2337 47	+1725 5138 44	-2650 3605 40	+2185 9376 54	-1703 0668 52
	3200 - 3800	+7296 9835 51	-1012 4495 47	+8494 4890 43	-1007 5645 40	+2485 6878 54	-1623 3039 52
	3800 - 4400	+7355 3715 51	-9492 3200 46	+5828 6345 43	-7193 5879 39	+2598 7416 54	-1867 0777 52
	4400 - 5000	+7412 7505 51	-8252 2950 46	+5117 7600 43	-4618 8168 39	+2726 6119 54	-1911 4164 52
	5000 - 6000	+7871 5782 51	+9909 4290 46	-6572 2870 43	+7825 5668 39	+4364 6730 54	-2298 7484 52
COF ₂	150 - 300	+4131 1379 51	-8226 1920 48	+7478 2778 46	-9970 5473 43	+2401 0874 54	+7645 5612 51
	300 - 500	+4500 8690 51	-5432 1224 48	+4581 6857 46	-4789 2317 43	+2320 2046 54	+5535 4142 51
	500 - 700	+3678 2507 51	-4772 8328 48	+2562 2177 46	-1955 9689 43	+2047 8396 54	+7674 1900 50
	700 - 1000	+4831 6009 51	-2985 8582 48	+1156 0805 46	-6481 0941 42	+1625 3541 54	-7624 2150 51
	1000 - 1300	+7879 7798 51	-1693 2846 48	+4684 2722 45	-1945 3137 42	+1089 1210 54	-1423 1012 52
	1300 - 1700	+8678 4190 51	-7904 5080 47	+1673 8397 45	-5273 3114 41	+4801 6047 53	-1962 3695 52
	1700 - 2100	+9108 8118 51	-4627 0080 47	+7630 8454 44	-1926 0389 41	+6748 8280 52	-2261 6387 52
	2100 - 2600	+9396 9763 51	-2546 8965 47	+3401 2225 44	-6947 7252 40	+5779 4560 53	-2612 2675 52
	2600 - 3200	+9587 4023 51	-1454 6465 47	+1576 5317 44	-2628 8817 40	+7897 2630 53	-2701 4363 52
	3200 - 3800	+9704 5646 51	-9199 5530 46	+8210 7660 43	-1147 7945 40	+9569 4820 53	-2761 5713 52
	3800 - 4400	+9781 4624 51	-5987 9330 46	+4538 2056 43	-5439 1950 39	+1646 6403 53	-2802 5647 52
	4400 - 5000	+9832 8204 51	-4061 2490 46	+2673 6624 43	-2799 4552 39	+1087 2569 54	-2844 2347 52
	5000 - 6000	+9883 5737 51	-2174 6468 46	+1235 8455 43	-1082 8883 39	+1244 9725 54	-2844 2347 52
Cl	150 - 300	+2499 7173 51	+5674 1480 47	+4632 7803 45	-4415 2433 42	+1633 2049 55	+5612 5486 51
	300 - 500	+2506 4788 51	-5929 4416 47	+5200 7614 45	-6227 5033 42	+1632 9938 55	+5573 8263 51
	500 - 700	+2636 4730 51	-2859 9690 47	+1486 3535 45	-1627 5100 42	+1629 1113 55	+4735 7792 51
	700 - 1000	+2743 3927 51	+6972 4500 45	+3294 7080 43	-1131 0739 41	+1625 6851 55	+4193 6441 51
	1000 - 1300	+2741 6558 51	+9775 6604 46	-2503 7621 44	+8246 8597 40	+1625 9067 55	+4191 7610 51
	1300 - 1700	+2710 4271 51	+9894 5520 46	-2052 2334 44	+6124 6450 40	+1628 0747 55	+4591 5167 51
	1700 - 2100	+2662 2371 51	+7245 6250 46	-1178 8354 44	+2884 4541 40	+1632 5570 55	+4721 8621 51
	2100 - 2600	+2620 6236 51	+4588 0250 46	-6064 0807 43	+1211 7404 40	+1637 6549 55	+5022 9170 51
	2600 - 3200	+2567 6175 51	+2858 2904 46	-3068 8116 43	+5031 4423 39	+1642 5883 55	+5266 1807 51
	3200 - 3800	+2585 1467 51	+1900 4820 46	-1679 7858 43	+2331 8500 39	+1646 6403 55	+5436 7772 51
	3800 - 4400	+2549 4787 51	+1280 0393 46	-9597 3450 42	+113 1857 39	+1650 0529 55	+5559 0897 51
	4400 - 5000	+2539 0046 51	+9115 8820 45	-5941 3944 42	+615 6189 38	+1652 6975 55	+5642 4806 51
	5000 - 6000	+2528 1946 51	+5179 8450 45	-2909 6748 42	+253 4032 38	+1656 0533 55	+5731 4370 51
Cl ₂	150 - 300	+3448 0294 51	-1658 5658 48	+2692 6483 46	-478 5249 43	+3934 6532 54	+6880 4000 51
	300 - 500	+3835 3499 51	-1188 8258 48	+1031 7245 46	-119 1520 43	+3873 9265 54	+4963 9378 51
	500 - 700	+4091 1205 51	-7711 9500 47	+4259 4980 45	-351 7128 42	+3815 0122 54	+3572 8781 51
	700 - 1000	+4269 0209 51	-3765 4088 47	+1485 0840 45	-873 1259 41	+3752 5719 54	+2509 1450 51
	1000 - 1300	+4388 1534 51	-1874 4198 47	+5195 4893 44	-215 2894 41	+3696 4574 54	+1760 9050 51
	1300 - 1700	+4478 1904 51	-7895 4060 46	+1610 2315 44	-453 1719 40	+3628 3890 54	+1152 1280 51
	1700 - 2100	+4529 1124 51	-4114 9154 46	+3753 0589 43	-790 8876 39	+3578 5248 54	+7973 3350 50
	2100 - 2600	+4610 0199 51	+3446 6630 46	-7130 3870 43	+275 3050 40	+3467 1576 54	+1942 1692 50
	2600 - 3200	+4760 6830 51	+1734 0760 47	-2492 1302 44	+668 4165 40	+3199 1333 54	+9806 5385 50
	3200 - 3800	+4874 2401 51	+2677 9490 47	-3503 0664 44	+857 2934 40	+2961 0183 54	-1888 1367 51
	3800 - 4400	+4707 9090 51	+1249 2260 47	-2466 4155 44	+714 8116 40	+3476 8067 54	-4600 9460 50
	4400 - 5000	+3900 2910 51	+4688 6050 47	+1508 8757 44	+212 2074 40	+6193 9315 54	+6505 1700 51
	5000 - 6000	+1847 5100 51	-1749 7481 48	+9091 4226 44	-627 1116 40	+1399 8920 55	+2441 5074 52
ClF	150 - 300	+3451 8575 51	-6195 0380 47	+8977 4934 45	-7664 4753 42	+1049 7334 55	+5684 2088 51
	300 - 500	+3579 0533 51	-1315 6216 48	+1125 5565 46	-1218 0078 43	+1047 9913 55	+5607 9032 51
	500 - 700	+3875 6488 51	-9742 9350 47	+1466 9790 45	-1248 9684 42	+1040 8878 55	+5496 6080 51
	700 - 1000	+4115 6129 51	-5105 3480 47	+1914 0981 45	-1115 8321 42	+1032 1081 55	+4761 0926 51
	1000 - 130						

TABLE I. - Continued. COEFFICIENTS FOR OBTAINING THERMODYNAMIC DATA FOR SEVERAL SUBSTANCES

[Coefficients for use in equations (105) to (107).]

Substance (a)	Temperature Interval, °K	Coefficients					
		A	B	C	D	E	F
ClF ₃	150 - 300	+5127 0429 51	-1749 4520 49	+1761 6464 47	-2976 1208 44	+2856 0159 55	+4659 5420 51
	300 - 500	+6457 5624 51	-5893 7083 48	+5115 6181 46	-5909 3643 43	+2828 1043 55	-2930 9810 51
	500 - 700	+7730 3861 51	-3819 8758 48	+2115 3958 46	-1756 7111 43	+2798 6643 55	-9857 9920 51
	700 - 1000	+8622 9749 51	-1802 3217 48	+7167 0960 45	-4305 6373 42	+2767 0675 55	-1520 7148 52
	1000 - 1300	+9203 6441 51	-8107 5540 47	+2291 6450 45	-1002 4218 42	+2739 3569 55	-1887 3181 52
	1300 - 1700	+9616 4642 51	-2539 0922 47	+5440 6701 44	-1755 2752 41	+2707 5754 55	-2168 5910 52
	1700 - 2100	+9764 0535 51	-1278 0686 47	+2126 0319 44	-5422 3408 40	+2693 2176 55	-2271 7800 52
	2100 - 2600	+9847 6403 51	-6517 8960 46	+8787 1110 43	-1805 4192 40	+2682 7742 55	-2332 5352 52
	2600 - 3200	+9897 9694 51	-3586 5496 46	+3936 3035 43	-6597 0677 39	+2675 1109 55	-2370 0484 52
	3200 - 3800	+9927 8564 51	-2207 8365 46	+2001 7247 43	-2809 9884 39	+2669 6912 55	-2392 8132 52
	3800 - 4400	+9946 9377 51	-1412 0292 46	+1092 2948 43	-1315 6062 39	+2665 5387 55	-2407 7328 52
	4400 - 5000	+9959 2224 51	-9559 0740 45	+6462 9910 42	-6817 9250 38	+2662 4430 55	-2417 5282 52
	5000 - 6000	+9971 6836 51	-4900 9530 45	+2907 6060 42	-2567 3024 38	+2658 5622 55	-2427 7976 52
F	300 - 500	+2774 1677 51	+1569 7918 47	-1219 8418 45	+8817 6073 41	+2448 1175 55	+3274 3817 51
	500 - 700	+2741 1306 51	+2447 1894 47	-1290 5400 45	+9364 9496 41	+2448 8816 55	+3442 3810 51
	700 - 1000	+2668 2300 51	+1435 7079 47	-5466 0762 44	+2926 9741 41	+2451 8215 55	+3882 1075 51
	1000 - 1300	+2606 1647 51	+7594 5950 46	-2066 6151 44	+8244 1470 40	+2455 3341 55	+4278 5777 51
	1300 - 1700	+2568 8565 51	+3901 3852 46	-8171 2274 43	+2516 1409 40	+2458 2444 55	+4530 4593 51
	1700 - 2100	+2543 7160 51	+1989 4083 46	-3203 1108 43	+7669 7618 39	+2460 7969 55	+4706 8085 51
	2100 - 2600	+2530 2137 51	+1158 2342 46	-1516 1312 43	+2979 4828 39	+2462 5383 55	+4804 8492 51
	2600 - 3200	+2520 8123 51	+6763 1070 45	-7187 4217 42	+1160 3925 39	+2464 0181 55	+4875 0108 51
	3200 - 3800	+2514 1282 51	+3904 6228 45	-3373 8858 42	+4456 9788 38	+2465 2647 55	+4924 7717 51
	3800 - 4400	+2510 0138 51	+2262 4946 45	-1637 1748 42	+1810 1580 38	+2466 2929 55	+4958 8764 51
F ₂	150 - 300	+3474 8807 51	-2479 3670 47	+2808 0384 45	+4516 8609 42	+3067 9524 55	+4488 2780 51
	300 - 500	+3499 3010 51	-1230 4361 48	+1038 5229 46	-1091 0390 43	+3067 9438 55	+4441 2399 51
	500 - 700	+3781 3514 51	-1031 1322 48	+5565 7851 45	-4317 1200 42	+3061 1457 55	+2916 9669 51
	700 - 1000	+4041 7357 51	-5868 2000 47	+2277 7137 45	-1285 7726 42	+3051 4311 55	+1359 1435 51
	1000 - 1300	+4247 3596 51	-3180 6992 47	+8736 8100 44	-3561 1383 41	+3040 9909 55	+6212 3900 49
	1300 - 1700	+4395 0680 51	-1548 4066 47	+3194 9833 44	-9363 6692 40	+3029 8990 55	+9330 9680 50
	1700 - 2100	+4473 0713 51	-1083 0146 47	+1705 8185 44	-3801 9221 40	+3022 6281 55	+1468 3319 51
	2100 - 2600	+4530 1221 51	-8004 6210 46	+1001 6324 44	-1705 3955 40	+3015 9621 55	+1873 5356 51
	2600 - 3200	+4577 2369 51	-4659 1418 46	+2852 3304 43	-5909 4373 39	+3009 4373 55	+2213 6134 51
	3200 - 3800	+4617 9447 51	-6168 3545 46	+4992 1151 43	-5319 2178 39	+3002 9324 55	+2510 8582 51
H	150 - 300	+4654 6023 51	-5845 5975 46	+3970 3472 43	-3521 4000 39	+2995 9930 55	+2784 3785 51
	300 - 500	+4686 8046 51	-5734 8144 46	+3364 9472 43	-2580 7455 39	+2989 1276 55	+3027 5170 51
	500 - 700	+4726 7301 51	-5239 8070 46	+2658 8548 43	-1685 9673 39	+2978 4168 55	+3341 3410 51
	700 - 1000	+2500 3116 51	+4852 8250 45	-6211 4920 43	+1415 8863 41	+4294 5264 55	+4609 6828 50
	1000 - 1300	+2499 6710 51	-2385 2015 45	+2047 2396 43	-2955 4273 40	+4294 5386 55	+4573 1922 50
	1300 - 1700	+2499 0717 51	-3432 3430 45	+1896 0083 43	-1754 6524 40	+4294 5692 55	+4533 8129 50
	1700 - 2100	+2499 5465 51	-1261 8040 45	+4772 2317 42	-3092 1566 39	+4294 5582 55	+4561 8786 50
	2100 - 2600	+2498 9933 51	-2095 0920 45	+6015 1654 42	-2948 5802 39	+4294 6101 55	+4522 0179 50
	2600 - 3200	+2499 9803 51	-1102 0773 44	+6488 9065 40	-4834 1707 36	+4294 5389 55	+4589 9392 50
	3200 - 3800	+2498 2764 51	-1021 2900 45	+1742 6965 42	-5235 9488 38	+4294 6258 55	+4537 6904 50
H ₂	150 - 300	+2989 2484 51	-4103 4770 48	+4407 7218 46	-8356 1287 43	+3401 1138 55	+1324 4021 51
	300 - 500	+3383 2407 51	-4324 5294 47	+3912 7728 45	-5061 2747 42	+3393 0261 55	+3572 0562 51
	500 - 700	+3459 0074 51	-1656 0656 47	+9153 4690 44	-7399 4236 41	+3391 6394 55	+3981 7170 51
	700 - 1000	+3480 7949 51	-8057 9160 46	+2316 5682 44	-2880 5124 38	+3391 4081 55	+4101 0320 51
	1000 - 1300	+3471 9964 51	-1811 4833 47	+4046 6752 44	-6393 1054 40	+3393 1405 55	+4004 9763 51
	1300 - 1700	+3478 9902 51	-3159 4629 47	+5167 8657 44	-1505 2076 41	+3394 2702 55	+3995 7133 51
	1700 - 2100	+3584 4555 51	-3452 5690 47	+5352 7626 44	-1138 9801 41	+3386 2783 55	+4672 5704 51
	2100 - 2600	+3759 4391 51	-2880 8338 47	+3648 3990 44	-6459 7043 40	+3365 5684 55	+5907 5858 51
	2600 - 3200	+3950 4361 51	-2214 0298 47	+2252 3788 44	-3163 7688 40	+3337 4923 55	+7304 4520 51
	3200 - 3800	+4015 1762 51	-2473 1652 47	+2122 3369 44	-2701 7643 40	+3332 1516 55	+7727 5210 51
HCl	150 - 300	+4253 9189 51	-1542 7069 47	+1065 7981 44	-1000 8309 40	+3278 8324 55	+9597 2790 51
	300 - 500	+4316 8247 51	-1611 9098 47	+9809 8240 43	-8461 6973 39	+3267 4437 55	+1005 6383 52
	500 - 700	+4413 8660 51	-6368 8580 46	+2766 2305 43	-6509 3656 38	+3168 4849 55	+1251 8853 52
	700 - 1000	+3507 7834 51	+3434 8560 46	-3783 9075 44	+7488 3407 41	+7840 0952 54	+2478 6303 51
	1000 - 1300	+3496 6325 51	-8772 1500 45	-1483 8166 44	+5505 0572 41	+7844 5758 54	+2549 0010 51
	1300 - 1700	+3455 5431 51	-2524 1094 47	+8256 9265 44	-2240 1276 41	+7868 1516 54	+2838 6335 51
	1700 - 2100	+3497 7739 51	-4336 2524 47	+1120 6186 45	-3799 5512 41	+7857 2051 54	+2632 6456 51
	2100 - 2600	+3637 7472 51	-4092 2196 47	+8387 1455 44	-2412 5676 41	+7762 0326 54	+1733 9321 51
	2600 - 3200	+3828 5869 51	-3262 2034 47	+5240 1857 44	-1237 0559 41	+7587 5851 54	+4355 1680 50
	3200 - 3800	+4008 0692 51	-2269 0376 47	+2958 7010 44	-5696 4676 40	+7371 4782 54	+4849 9400 50
HF	150 - 300	+4163 1444 51	-1552 5681 47	+1637 7004 44	-2558 9129 40	+7141 4411 54	+1992 0853 51
	300 - 500	+4278 2700 51	-1136 3225 47	+9795 8780 43	-1262 3444 40	+6935 9632 54	+2867 0492 51
	500 - 700	+4365 4707 51	-8607 3540 46	+6238 6255 43	-6741 6929 39	+6753 4656 54	+3533 0504 51
	700 - 1000	+4428 6165 51	-6932 3370 46	+4323 4380 43	-3995 4750 39	+6599 9666 54	+4029 0913 51
	1000 - 1300	+4496 5332 51	-4983 7368 46	+2652 7672 43	-1976 9074 39	+6397 5200 54	+4580 2542 51
	1300 - 1700	+3502 9862 51	-5341 4090 45	+3907 3861 43	-1722 7617 40	+1026 8292 52	+9285 0538 50
	1700 - 2100	+3503 7414 51	-7163 1600 44	-5447 6980 42	+5181 9187 40	-1044 2091 52	+9241 9770 50
	2100 - 2600	+3510 6273 51	+3178 3340 46	-2370 2806 44	+3298 9392 41	-1264 3243 52	+8825 1182 50
	2600 - 3200	+3497 5136 51	-1383 0680 46	-5305 0300 43	+1983 9089 41	-5429 5120 51	+9703 1135 50
	3200 - 3800	+3459 5106 51	-2005 0034 47	+4630 1579 44	-9300 2525 40	+2673 4630 52	+1258 5941 51
H ₂ O	150 - 300	+3477 7106 51	-3196 6027 47	+6293 8357 44	-1587 5290 41	+2887 5590 52	+1190 5757 51
	300 - 500	+3595 2253 51	-3334 3110 47	+5229 6762 44	-1153 0942 41	+6743 7760 52	+4224 9140 50
	500 - 700	+3754 7551 51	-2772 2634 47	+3563 5125 44	-6593 9114 40	+2520 7695 53	+7005 1120 50
	700 - 1000	+3932 3426 51	-2104 1015 47	+2197 0853 44	-3337 2252 40	+5111 9610 53	+1999 9964 51
	1000 - 1300	+4085 7884 51	-1614 8342 47	+1377 0964 44	-1723 8858 40	+7813 6590 53	+3159 4638 51
	1300 - 1700	+4209 3672 51	-1252 4527 47	+8941 3920 43	-9272 9771 39	+1042 4966 54	+4104 5633 51
	1700 - 2100	+4301 3524 51	-1027 8717 47	+6265 6581 43	-5431 6307 39	+1264 8039 54	+4825 1389 51
	2100 - 2600	+4402 9214 51	-7489 6732 46	+3816 7579 43	-2461 9992 39	+1564 9097 54	+5647 2957 51
	2600 - 3200	+4012 7997 51	+4444 8300 46	-1184 6208 45	+4440 3590 42	+5696 5839 54	+1658 1832 50
	3200 - 3800	+3984 3281 51	-1560 3100 47	+8521 9880 44	+9334 5693 41	+5702 9188 54	+3361 4200 48
	3800 - 4400	+3995 7858 51	-5866 2548 47	+2772 9813 45	-1277 3920 42	+5705 5261 54	+7248 4000 48

*All substances in gaseous phase except water.

TABLE I. - Continued. COEFFICIENTS FOR OBTAINING THERMODYNAMIC DATA FOR SEVERAL SUBSTANCES
[Coefficients for use in equations (105) to (107).]

Sub- stance (a)	Temperature Interval, °K	Coefficients					
		A	B	C	D	E	F
N	300 - 500	+2499 6710 51	-2385 2015 45	+2047 2396 43	-2955 4273 40	+5707 9313 55	+4183 1808 51
	500 - 700	+2499 1136 51	-3267 4440 45	+1798 0743 43	-1659 2209 40	+5707 9603 55	+4186 8511 51
	700 - 1000	+2499 6036 51	-1131 0429 45	+4232 2090 42	-2736 5544 39	+5707 9478 55	+4183 9375 51
	1000 - 1300	+2499 0940 51	-1901 1726 45	+5442 2129 42	-2666 8173 39	+5707 9952 55	+4187 5999 51
	1300 - 1700	+2500 2204 51	+3456 2550 44	-5655 6710 41	+4200 6645 38	+5707 9078 55	+4179 7565 51
	1700 - 2100	+2501 6390 51	+2522 5800 45	-4789 7317 42	+1627 5565 39	+5707 7262 55	+4169 0222 51
	2100 - 2600	+2508 6192 51	+1107 6049 46	-1756 3079 43	+5016 8252 39	+5706 6696 55	+4115 3955 51
	2600 - 3200	+2517 3414 51	+2174 0230 46	-3034 2712 43	+7858 2646 39	+5705 0383 55	+4045 6309 51
	3200 - 3800	+2512 6964 51	+1967 0040 46	-2871 8071 43	+7694 4866 39	+5706 2395 55	+4083 2154 51
	3800 - 4400	+2482 1655 51	-6399 2200 45	-8908 3900 42	+4843 1658 39	+5715 2935 55	+4343 0639 51
	4400 - 5000	+2434 6193 51	-5054 2730 46	+1913 3373 43	+1308 3373 39	+5732 4433 55	+4765 1025 51
	5000 - 6000	+2351 2887 51	-1171 7309 47	+5608 4591 43	-2764 8502 39	+5766 8718 55	+5513 9770 51
N ₂	150 - 300	+3501 6234 51	+1419 9930 46	-2221 4814 44	+6337 0257 41	+8539 5697 53	+3078 0353 51
	300 - 500	+3507 3207 51	+6478 8790 46	-7700 5600 44	+1686 9531 42	+8527 6963 53	+3045 5391 51
	500 - 700	+3468 1570 51	-1742 8035 47	+6732 6921 44	+6988 8312 40	+8673 6314 53	+3295 4226 51
	700 - 1000	+3462 1286 51	-4539 6402 47	+1622 1534 45	-6973 0151 41	+8776 6703 53	+3385 9355 51
	1000 - 1300	+3600 4480 51	-4968 5174 47	+1321 7619 45	-4923 4174 41	+8096 8196 53	+2555 2204 51
	1300 - 1700	+3793 9348 51	-3715 9604 47	+7731 5595 44	-2325 2167 41	+6485 5239 53	+1278 3593 51
	1700 - 2100	+3979 4426 51	-2618 0633 47	+4257 4284 44	-1039 0909 41	+4949 4356 53	+3226 6000 48
	2100 - 2600	+4131 6527 51	-1645 9670 47	+2167 0242 44	-4284 4626 40	+3093 6592 53	-1092 8453 51
	2600 - 3200	+4249 0997 51	-1039 9359 47	+1106 6286 44	-1770 7380 40	+1332 3679 53	-1962 7879 51
	3200 - 3800	+4327 0196 51	-7332 7190 46	+6383 0855 43	-8445 0756 39	+4394 6700 51	-2551 1939 51
	3800 - 4400	+4383 7162 51	-5322 6420 46	+3896 3172 43	-4326 2187 39	-1248 3259 53	-2990 7057 51
	4400 - 5000	+4426 8870 51	-3934 9468 46	+2455 1316 43	-2274 3750 39	-2321 5622 51	-1332 6990 51
5000 - 6000	+4822 3937 51	+1235 5686 47	-7763 4410 43	+8482 4648 39	-1669 0365 54	-6686 7119 51	
NH ₃	150 - 300	+3501 4877 51	-1135 4880 46	+3492 4950 43	+1605 9661 41	+5707 5674 55	+1837 3594 51
	300 - 500	+3506 9044 51	+1658 8050 46	-1893 7787 44	+3971 7660 41	+5707 4332 55	+1806 0451 51
	500 - 700	+3507 6770 51	+2796 6700 46	-3019 6472 44	+5706 5528 41	+5707 4505 55	+1802 3997 51
	700 - 1000	+3467 4923 51	-1587 8517 47	+4682 2623 44	-3133 4757 40	+5709 6465 55	+2076 5108 51
	1000 - 1300	+3476 0496 51	-3595 9897 47	+8992 4746 44	-2700 0943 41	+5710 4331 55	+2082 2903 51
	1300 - 1700	+3578 3151 51	-3917 3724 47	+7834 3879 44	-2085 4695 41	+5703 9404 55	+1443 5951 51
	1700 - 2100	+3753 2238 51	-3437 2875 47	+5329 0472 44	-1133 8710 41	+5688 4282 55	+2671 2430 50
	2100 - 2600	+3924 7695 51	-2774 1647 47	+3440 1817 44	-5700 1390 40	+5668 6761 55	-9419 7230 50
	2600 - 3200	+4082 2543 51	-2416 9060 47	+2402 2699 44	-3132 6809 40	+5647 1309 55	-2072 8080 51
	3200 - 3800	+4226 3537 51	-2291 3941 47	+1856 8495 44	-1990 5685 40	+5624 2276 55	-3121 4787 51
	3800 - 4400	-9768 5140 52	-6242 7160 49	+5044 9155 46	-7082 5339 42	+3413 8680 56	+8395 4054 53
	4400 - 5000	-1813 5084 52	-8906 1750 49	+6213 1583 46	-7379 7014 42	+6634 4534 56	+1553 9865 54
5000 - 6000	-2323 8668 52	-1115 6880 49	+6734 9310 45	-6814 6304 41	+1606 8773 56	+2311 5519 53	
NH ₃	150 - 300	+4016 0739 51	-5921 7280 47	+2172 9700 45	+8870 2067 42	+4660 2050 55	+2676 3530 50
	300 - 500	+3929 2082 51	-1358 1227 48	+1045 1508 46	-6997 1157 42	+4662 0202 55	+7631 5510 50
	500 - 700	+4204 7432 51	-2082 9945 48	+1039 4443 46	-6167 7796 42	+4656 2775 55	-6133 4010 50
	700 - 1000	+4643 7799 51	-2103 0362 48	+7635 1643 45	-3465 0380 42	+4641 3606 55	-3108 4650 51
	1000 - 1300	+5267 2607 51	-2084 8879 48	+5491 9755 45	-1983 4803 42	+4612 0057 55	-6862 3930 51
	1300 - 1700	+6020 3398 51	-1698 3392 48	+3497 6990 45	-1020 9245 42	+4558 7608 55	-1178 4321 52
	1700 - 2100	+6822 7353 51	-1316 2876 48	+2126 1664 45	-5097 7779 41	+4484 9963 55	-1725 7876 52
	2100 - 2600	+7558 4148 51	-8904 3840 47	+1171 7555 45	-2312 0365 41	+4395 8496 55	-2253 4893 52
	2600 - 3200	+8185 0643 51	-5794 8770 47	+6205 9477 44	-1009 0955 41	+4301 8144 55	-2717 1642 52
	3200 - 3800	+8640 1560 51	-3931 9340 47	+3470 3306 44	-4747 1369 40	+4219 6290 55	-3062 3226 52
	3800 - 4400	+8962 9398 51	-2692 3262 47	+2017 9453 44	-2371 7716 40	+4149 2986 55	-3314 0852 52
	4400 - 5000	+9187 2759 51	-1912 4119 47	+1245 5081 44	-1282 4365 40	+4002 3525 55	-3492 7645 52
5000 - 6000	+9414 7085 51	-1099 4602 47	+6180 2898 43	-5346 0492 39	+4021 6182 55	-3679 8456 52	
NO	300 - 500	+3629 9914 51	+2657 5880 47	-2717 2093 45	+4701 8630 42	+1177 3583 55	+4650 8256 51
	500 - 700	+3526 2159 51	-3327 2407 47	+1496 6665 45	-5017 5332 41	+1180 6009 55	+5285 0742 51
	700 - 1000	+3571 2043 51	-5722 3794 47	+2111 9083 45	-1023 0275 42	+1179 4145 55	+5066 8759 51
	1000 - 1300	+3769 9172 51	-4896 8460 47	+1322 3357 45	-5147 2119 41	+1169 0270 55	+3897 0127 51
	1300 - 1700	+3976 2131 51	-3140 6382 47	+6575 7561 44	-2009 1463 41	+1153 6702 55	+2461 7464 51
	1700 - 2100	+4137 1746 51	-2076 7231 47	+3380 3599 44	-8273 2029 40	+1138 5290 55	+1351 2723 51
	2100 - 2600	+4259 7731 51	-1265 1294 47	+1656 3960 44	-3228 0166 40	+1123 5766 55	+4673 8600 50
	2600 - 3200	+4349 0587 51	-8120 9610 46	+8518 4400 43	-1311 7501 40	+1110 2937 55	-1928 0800 50
	3200 - 3800	+4413 5660 51	-5677 9250 46	+4786 5005 43	-5809 5741 39	+1098 7485 55	-6803 6460 50
	3800 - 4400	+4459 4771 51	-4305 6534 46	+2995 3452 43	-2883 0271 39	+1088 9003 55	-1035 1524 51
	4400 - 5000	+4489 7869 51	-3762 9549 46	+2235 0024 43	-1791 0895 39	+1081 6691 55	-1270 7127 51
	5000 - 5500	+4509 2548 51	-3739 5470 46	+1972 1171 43	-1430 4410 39	+1076 9605 55	-1419 8637 51
5500 - 6000	+4525 5565 51	-3723 0352 46	+1802 9307 43	-1226 2702 39	+1072 4569 55	-1546 9048 51	
O	150 - 300	+2832 8173 51	+1431 7687 48	-1468 4834 46	+2566 9894 43	+3017 4976 55	+3217 0845 51
	300 - 500	+2714 6413 51	+3870 4329 47	-3379 2646 45	+3969 6103 42	+3019 9635 55	+3891 1039 51
	500 - 700	+2629 9259 51	+2286 8597 47	-1271 4552 45	+1065 1442 42	+3021 9345 55	+4354 2996 51
	700 - 1000	+2576 2890 51	+1028 8519 47	-4106 0040 44	+2484 6390 41	+3023 8309 55	+4676 2053 51
	1000 - 1300	+2547 0979 51	+5221 5330 46	-1496 6858 44	+6739 3093 40	+3025 1125 55	+4458 4101 51
	1300 - 1700	+2519 3465 51	+1151 2610 46	-2514 3283 43	+8031 2904 39	+3027 2774 55	+5048 9417 51
	1700 - 2100	+2514 1793 51	+5680 0900 45	-1678 4195 43	+4800 0132 39	+3027 7264 55	+5083 3051 51
	2100 - 2600	+2508 6997 51	+6151 5400 45	-9959 5160 42	+2941 9744 39	+3028 4518 55	+5123 3201 51
	2600 - 3200	+2506 8516 51	+6191 4720 45	-1014 7413 43	+3113 4905 39	+3028 8330 55	+5137 3787 51
	3200 - 3800	+2496 0645 51	-4318 7660 45	-1785 1200 41	+1353 7926 39	+3031 3904 55	+5226 2535 51
	3800 - 4400	+2484 1660 51	-1828 7300 46	+9952 7176 42	-1281 2973 38	+3035 1914 55	+5391 3688 51
	4400 - 5000	+2461 6602 51	-3966 3519 46	+2327 9192 42	-1788 5282 39	+3043 5044 55	+5532 3795 51
O ₂	150 - 300	+3507 8622 51	+7336 8300 46	-1566 0917 45	+5367 9823 42	+1022 7365 54	+3678 3884 51
	300 - 500	+3468 1122 51	-2094 4310 47	+1311 3020 45	+4112 4133 41	+1031 5694 54	+4905 2651 51
	500 - 700	+3491 8904 51	-6759 0190 47	+3398 6627 45	-2087 8706 42	+1030 0629 54	+4833 9511 51
	700 - 1000	+3655 2327 51	-6543 3148 47	+2462 0346 45	-1270 0679 42	+9684 3794 53	+3884 7554 51
	1000 - 1300	+3904 0901 51	-4442 4078 47	+1199 2093 45	-4661 9082 41	+8345 0760 53	+2319 0523 51
	1300 - 1700	+4104 9900 51	-2517 0318 47	+5093 9020 44	-1409 5115 41	+6895 7755 53	+0729 7660 50
	1700 - 2100	+4222 7020 51	-1953 0831 47	+2975 1070 44	-5976 9259 40	+5794 9642 53	+1747 6760 50
	2100 - 2600	+4302 7917 51	-1791 1603 47	+2194 9064 44	-3493 6626 40	+4957 1490 53	+1763 2250 50
	2600 - 3200	+4378 2138 51	-1859 5901 47	+1888 4516 44	-2642 8824 40	+4050 9189 53	-8980 5550 50
	3200 - 3800	+4481 6232 51	-1804 0341 47	+1533 7064 44	-1904 1376 40	+2395 5642 53	-1649 5016 51
	3800 - 4400	+4595 4599 51	-1604 0929 47	+1175 2869 44	-1306 8504 40	+6835 3000 51	-2514 2771 51
	4400 - 5000	+4700 9554 51	-1392 3351 47	+9033 6640 44	-9220 7268 39	+2507 6420 53	-3338 5270 51
OH	150 - 300	+3764 1804 51	+1330 9369 48	-1397 7859 44	+2549 9846 43	+2208 6061 55	+6394 1790 50
	300 - 500	+3650 7552 51	+2767 0068 47	-2437 5563 44	+2946 8393 42	+2210 9337 55	+1286 1048 51
	500 - 700	+3583 7943 51	+1516 8258 47	-9296 1300 44	+9667 5264 41	+2212 6553 55	+1658 9638 51
	700 - 1000	+3516 1720 51	-4302 4030 46	+4112 6890 44	+1744 5983 41	+2215 8159 55	+2091 0667 51

TABLE II. - INPUT TO VECTOR
AND PROPELLANT DECK*

Product code	Card column	
44-47	48-50	51-60
0037	BOP	
0054	ATM	H
0061	ATM	N
0450	ATM	O
0451	MOL	H2
0650	MOL	H2O1
0651	MOL	N2
0750	MOL	N1O1
0751	MOL	O2
	MOL	O1H1
	F1	N2H4
	EF1	1547029756
	PF1	1000000053
	X1	H2O2
	EX1	2868162655
	PX1	1000000053

*The symbol \bar{O} is used to indicate the alphabetic letter; the symbol 0 is used for zero.

TABLE III. - OUTPUT OF VECTOR AND PROPELLANT DECK

Type of card	Product code	Packed vector	Product code		
	Card column				
	17-20	31-40	44-47	48-50	51-60
Packed vectors	0037	0000000001	0037	ATM	H
	0054	0000000011	0054	ATM	N
	0061	0000000021	0061	ATM	O
	0450	0000000002	0450	MOL	H2
	0451	0000000021	0451	MOL	H2O1
	0650	0000000012	0650	MOL	N2
	0651	0000001121	0651	MOL	N1O1
	0750	0000000022	0750	MOL	O2
	0751	0000002101	0751	MOL	O1H1
Cards for listing only to check input				F1	N2H4
				EF1	1547029756
				PF1	1000000053
				X1	H2O2
				EX1	2868162655
				PX1	1000000053

Type of card	Drum location	Contents	Drum location	Contents	Drum location	Contents
	Card column					
	1-4	5-15	16-19	20-30	31-34	35-45
a_f (hydrogen)	0587	1248127850+	0588	6240639049+		
b_f (nitrogen)						
Fuel enthalpy, h_f	0597	4827226954+	0598	1248127850+		
Fuel valence, v_f						
a_x (hydrogen)	0537	5879586049+	0539	5379586049+		
c_x (oxygen)						
Oxidant enthalpy, h_x	0547	8431804353+	0548	5879586049+	0549	1175917250-
Oxidant valence, v_x^+						
Oxidant valence, v_x^-						

TABLE IV. - INPUT TO MAIN OPERATING DECK

[illegible]

TABLE V. - OUTPUT OF MAIN OPERATING DECK

		EQUIV RATO R		O/F	PRCNT FUEL	PC PSIA	ENTH CAL/ GM	IDENT FICA TN		
9005	6	+8571	4286	50	+1592 1118 51	+3857 8583 52	+6000 0000 53	+2380 1691 54	+0857 0208 63	1
9005	6	A SUB F	B SUB F	C SUB F	D SUB F	E SUB F				2
9005	6	+1248 1278 50	+6240 6390 49						+0857 0208 63	3
9005	6	F SUB F	G SUB F	H SUB F	I SUB F	J SUB F				4
9005	6									5
9005	6	FUEL ENTH HF	FUEL +VAL VF ⁺	FUEL -VAL VF ⁻						6
9005	6	+4827 2269 54	+1248 1278 50						+0857 0208 63	7
9005	6	A SUB X	B SUB X	C SUB X	D SUB X	E SUB X				8
9005	6	+5879 5860 49		+5879 5860 49					+0857 0208 63	9
9005	6	F SUB X	G SUB X	H SUB X	I SUB X	J SUB X				10
9005	6									11
9005	6	OXID ENTH HX	OXID +VAL VX ⁺	OXID -VAL VX ⁻						12
9005	6	+8431 8043 53	+5879 5860 49	-1175 9172 50					+0857 0208 63	13
										14
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										100

Type of equation	Equation number in text	Gaseous molecules					Gaseous atoms				Condensed phases			
		$\Delta \ln n_1$	$\Delta \ln n_2$	$\Delta \ln n_3$	---	$\Delta \ln n_Z$	$\Delta \ln n_Y$	$\Delta \ln n_X$	---	$\Delta \ln n_M$	$\Delta \ln n_N$	$-\Delta \ln A$	$\Delta \ln T$	Constant
Gaseous equilibria	(29)	1	0	0	0	-a ₁	-b ₁	-c ₁	---	0	0	0	-q ₁	-s ₁
		0	1	0	0	-a ₂	-b ₂	-c ₂	---	0	0	0	-q ₂	-s ₂
		0	0	1	0	-a ₃	-b ₃	-c ₃	---	0	0	0	-q ₃	-s ₃
		0	0	0	---	---	---	---	---	0	0	0	---	---
Mass balance	(28)	a ₁ n ₁	a ₂ n ₂	a ₃ n ₃	---	r _Z	0	0	0	---	a _N n _N	$\sum a_i n_i$	0	AAa
		b ₁ n ₁	b ₂ n ₂	b ₃ n ₃	---	0	n _Y	0	0	---	b _N n _N	$\sum b_i n_i$	0	ABa
		c ₁ n ₁	c ₂ n ₂	c ₃ n ₃	---	0	0	n _X	0	---	c _N n _N	$\sum c_i n_i$	0	ACa
		----	----	----	---	0	0	0	---	---	---	---	0	---
Condensed-phase equilibria	(30)	0	0	0	0	---	---	---	---	0	0	0	---	---
		0	0	0	0	a _M	b _M	c _M	---	0	0	0	q _M	s _M
		0	0	0	0	a _N	b _N	c _N	---	0	0	0	q _N	s _N
Pressure	(31)	p ₁	p ₂	p ₃	---	p _Z	p _Y	p _X	---	0	0	0	0	ΔP
Enthalpy*	(32)	(H _T ⁰) ₁ n ₁	(H _T ⁰) ₂ n ₂	(H _T ⁰) ₃ n ₃	---	(H _T ⁰) _Z n _Z	(H _T ⁰) _Y n _Y	(H _T ⁰) _X n _X	---	(H _T ⁰) _M n _M	(H _T ⁰) _N n _N	$\sum (H_T^0)_i n_i$	$\sum (C_p^0)_i n_i$	ΔH

*Row vector to be substituted in place of enthalpy row for isentropic expansion to assigned pressure:

Entropy	(33)	(S _T) ₁ n ₁	(S _T) ₂ n ₂	(S _T) ₃ n ₃	---	(S _T) _Z n _Z	(S _T) _Y n _Y	(S _T) _X n _X	---	(S _T) _M n _M	(S _T) _N n _N	$\sum (S_T)_i n_i$	$\sum (C_p^0)_i n_i$	ΔS
---------	------	---	---	---	-----	---	---	---	-----	---	---	--------------------	----------------------	----

Figure 1. - General matrix of correction equations for adiabatic combustion at assigned pressure.

Type of equation	Gaseous atoms				Condensed phases			
	$\left(\frac{\partial \ln p_Z}{\partial \ln T}\right)_P$	$\left(\frac{\partial \ln p_Y}{\partial \ln T}\right)_P$	$\left(\frac{\partial \ln p_X}{\partial \ln T}\right)_P$		$\left(\frac{\partial n_M}{\partial \ln T}\right)_P$	$\left(\frac{\partial n_N}{\partial \ln T}\right)_P$	$-\left(\frac{\partial \ln A}{\partial \ln T}\right)_P$	Constant
Mass balance	$\sum a_i^2 p_i$	$\sum a_i b_i p_i$	$\sum a_i c_i p_i$	---	a_M	a_N	$\sum a_i n_i$	$\sum a_i q_i p_i$
	$\sum a_i b_i p_i$	$\sum b_i^2 p_i$	$\sum b_i c_i p_i$	---	b_M	b_N	$\sum b_i n_i$	$\sum b_i q_i p_i$
	$\sum a_i c_i p_i$	$\sum b_i c_i p_i$	$\sum c_i^2 p_i$		c_M	c_N	$\sum c_i n_i$	$\sum c_i q_i p_i$
	-----	-----	-----	---	---	---	---	-----
Condensed-phase equilibria	-----	-----	-----	---	0	0	0	-----
	a_M	b_M	c_M	---	0	0	0	q_M
	a_N	b_N	c_N	---	0	0	0	q_N
Pressure	$\sum a_i p_i$	$\sum b_i p_i$	$\sum c_i p_i$	---	0	0	0	$\sum q_i p_i$

Figure 3. - General reduced augmented matrix for partial derivatives at constant pressure. (Summations in terms of p_i for gaseous products only. Summations in terms of n_i for all products.)

Type of equation	Gaseous atoms				Condensed phases		
	$\left(\frac{\partial \ln p_Z}{\partial \ln A}\right)_T$	$\left(\frac{\partial \ln p_Y}{\partial \ln A}\right)_T$	$\left(\frac{\partial \ln p_X}{\partial \ln A}\right)_T$		$\left(\frac{\partial n_M}{\partial \ln A}\right)_T$	$\left(\frac{\partial n_N}{\partial \ln A}\right)_T$	Constant
Mass balance	$\sum a_i^2 p_i$	$\sum a_i b_i p_i$	$\sum a_i c_i p_i$	---	a_M	a_N	$\sum a_i n_i$
	$\sum a_i b_i p_i$	$\sum b_i^2 p_i$	$\sum b_i c_i p_i$	---	b_M	b_N	$\sum b_i n_i$
	$\sum a_i c_i p_i$	$\sum b_i c_i p_i$	$\sum c_i^2 p_i$	---	c_M	c_N	$\sum c_i n_i$
	----	-----	-----	---	--	--	----
Condensed-phase equilibria	--	--	--	---	0	0	0
	a_M	b_M	c_M	---	0	0	0
	a_N	b_N	c_N	---	0	0	0

Figure 4. - General reduced augmented matrix for partial derivatives at constant temperature. (Summations in terms of p_i for gaseous products only. Summations in terms of n_i for all products.)

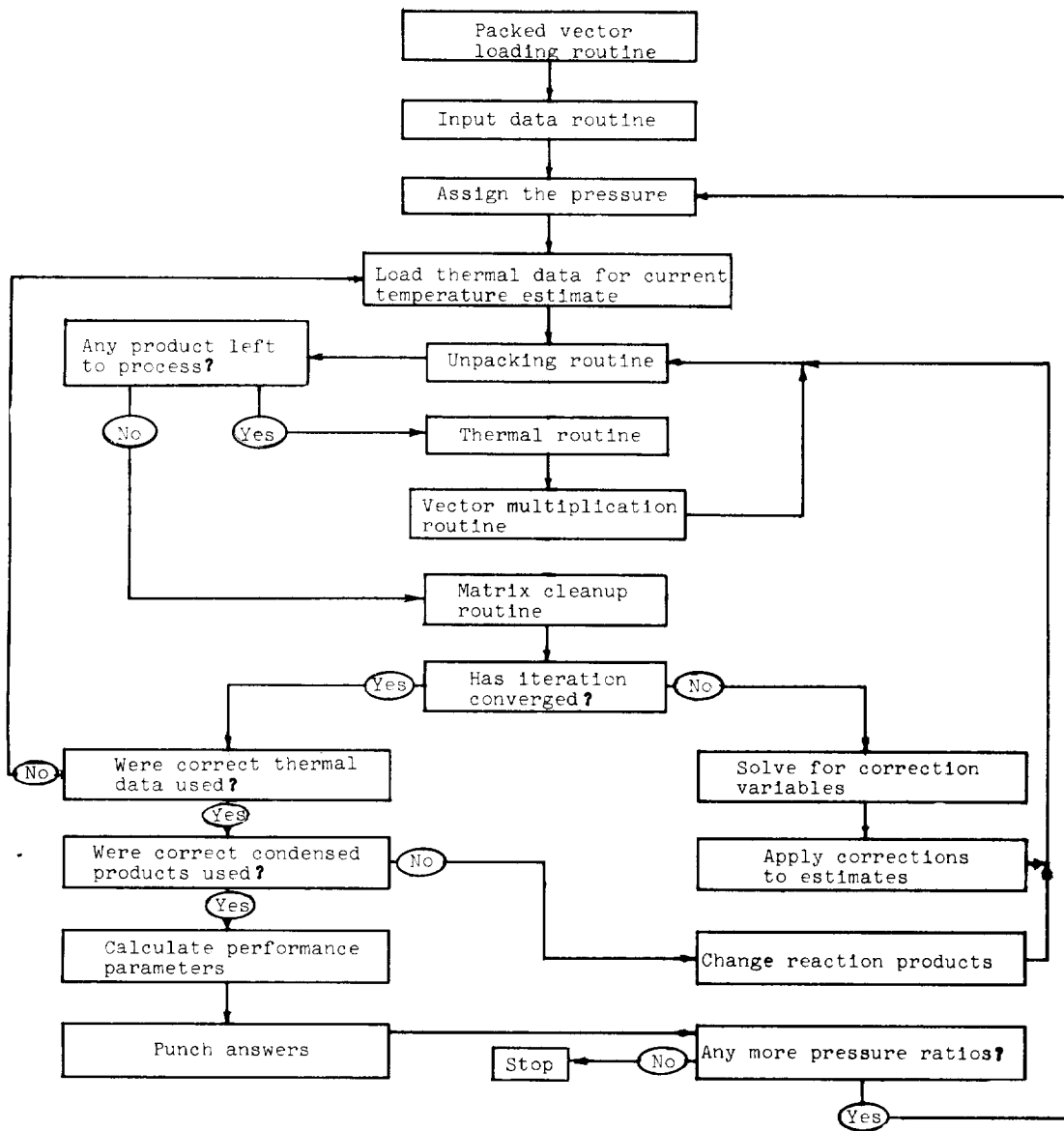


Figure 5. - Flow chart for Main Calculating Program.

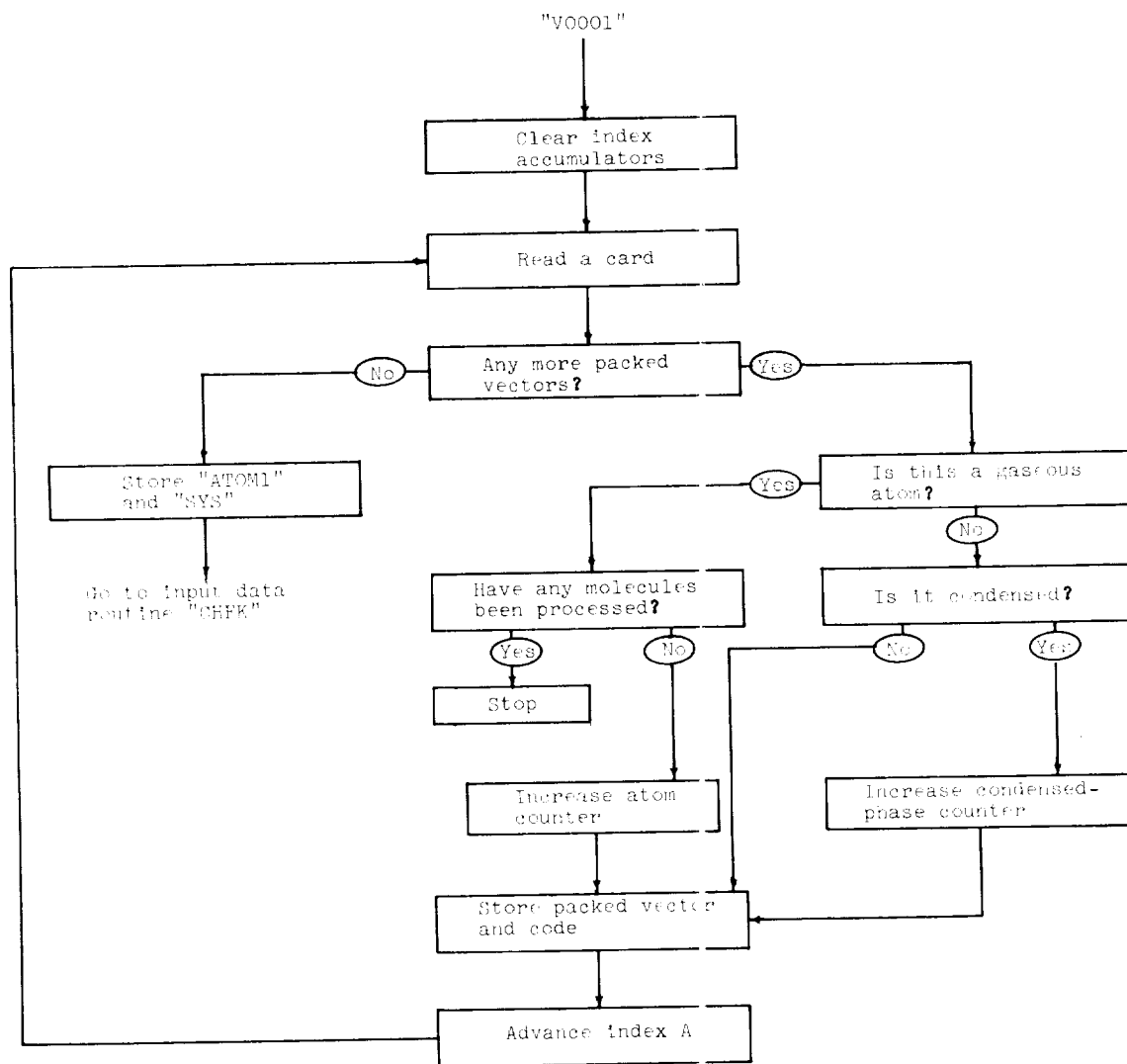


Figure 6. - Flow chart for packed vector loading.

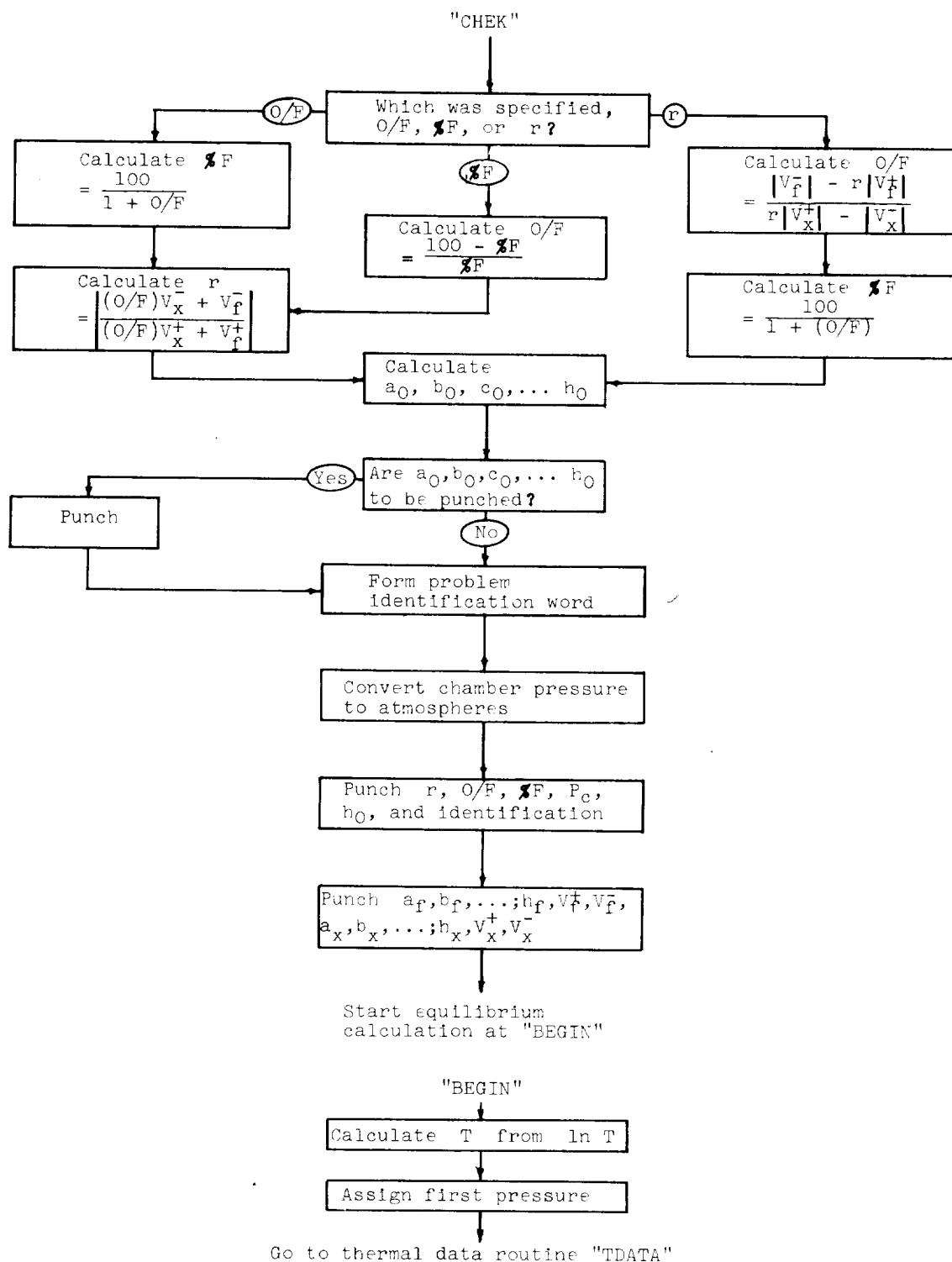


Figure 7. - Flow chart for input data routine.

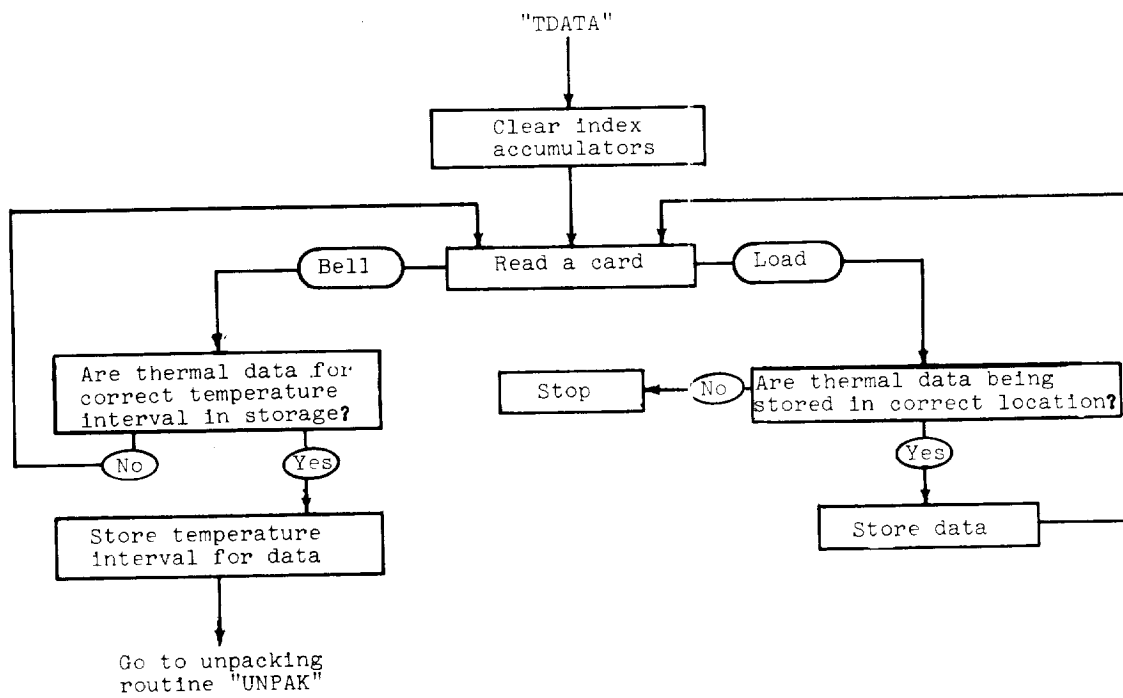


Figure 8. - Flow chart for load thermal data.

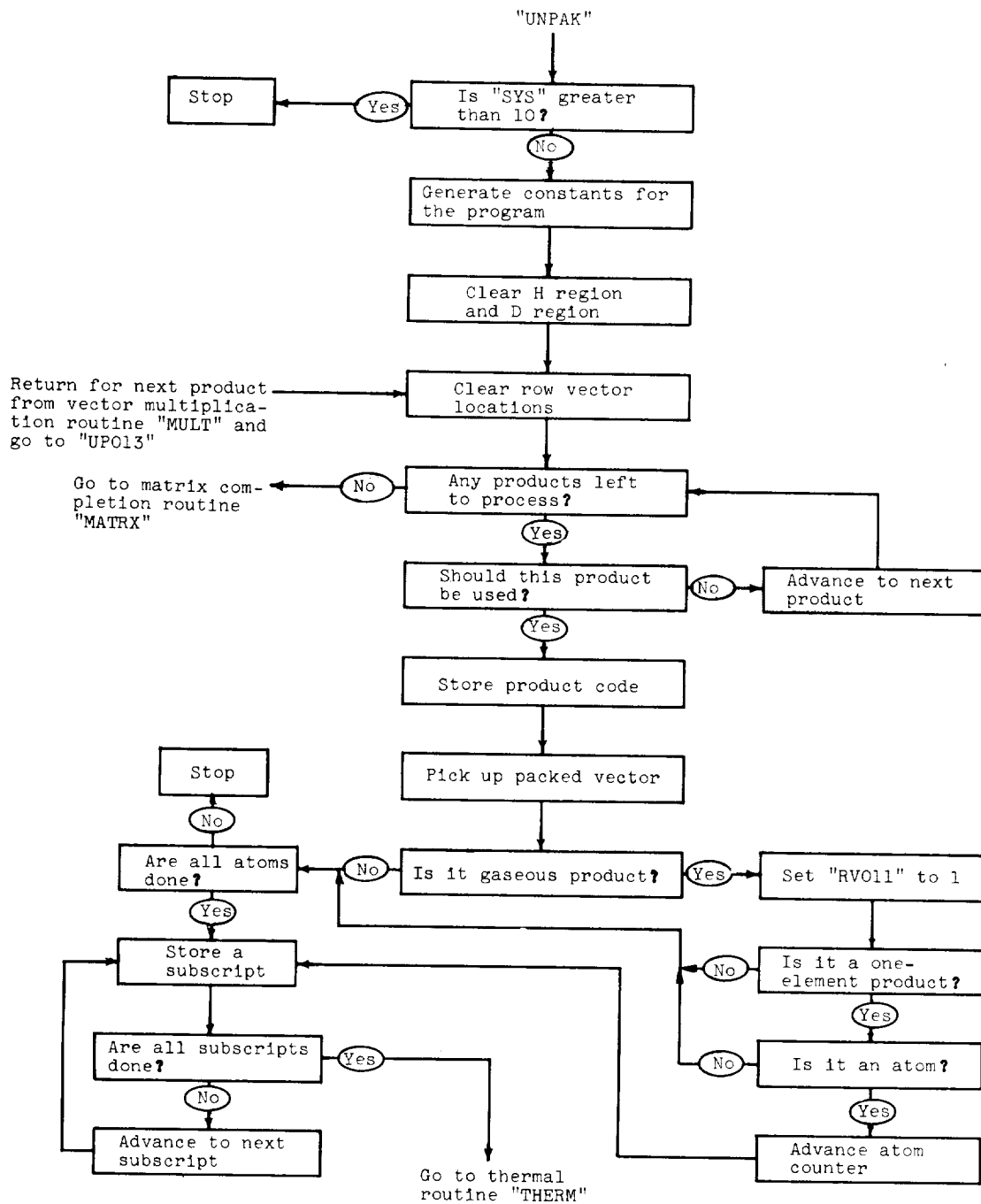


Figure 9. - Flow chart for unpacking routine.

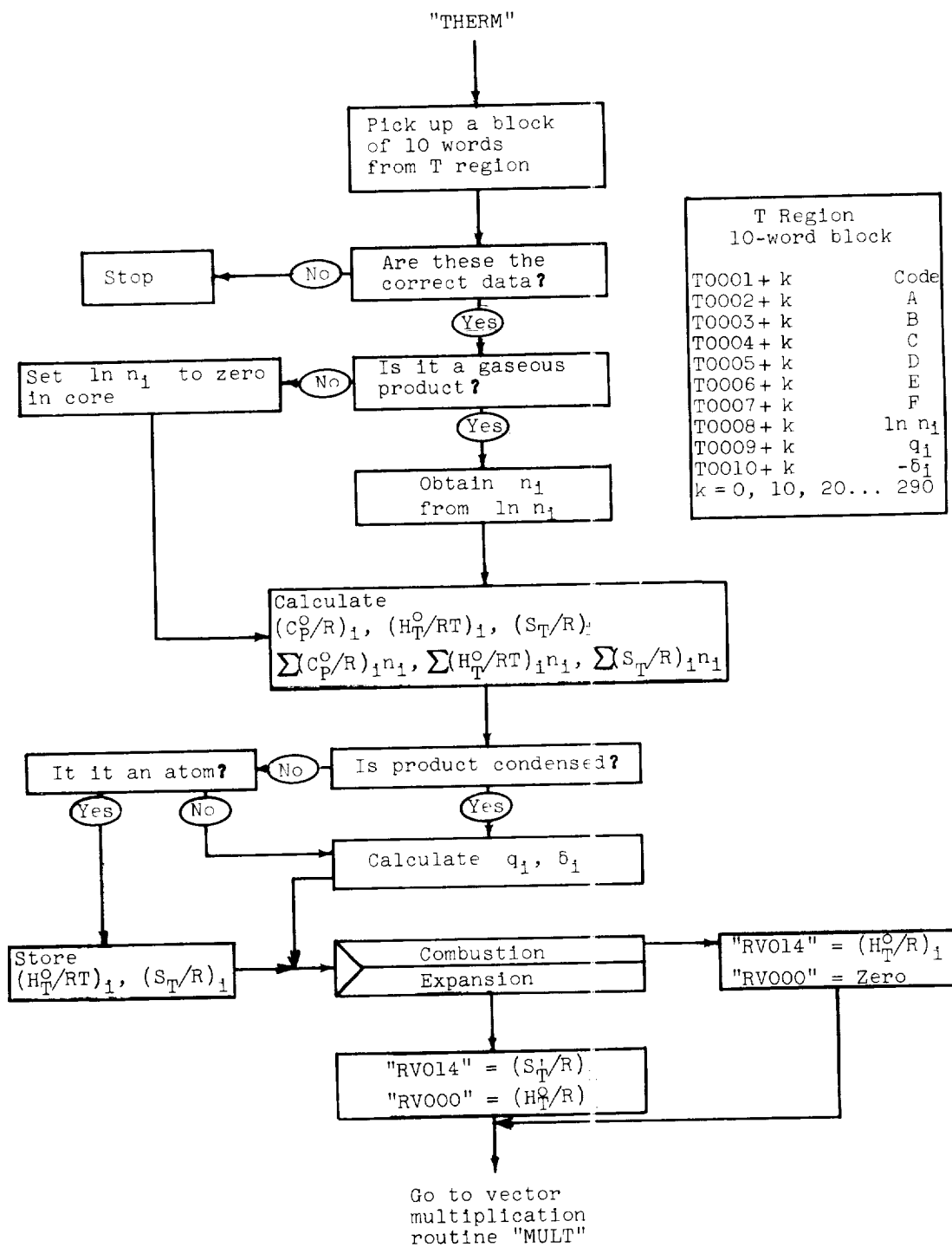


Figure 10. - Flow chart for thermal routine.

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CA-19 back

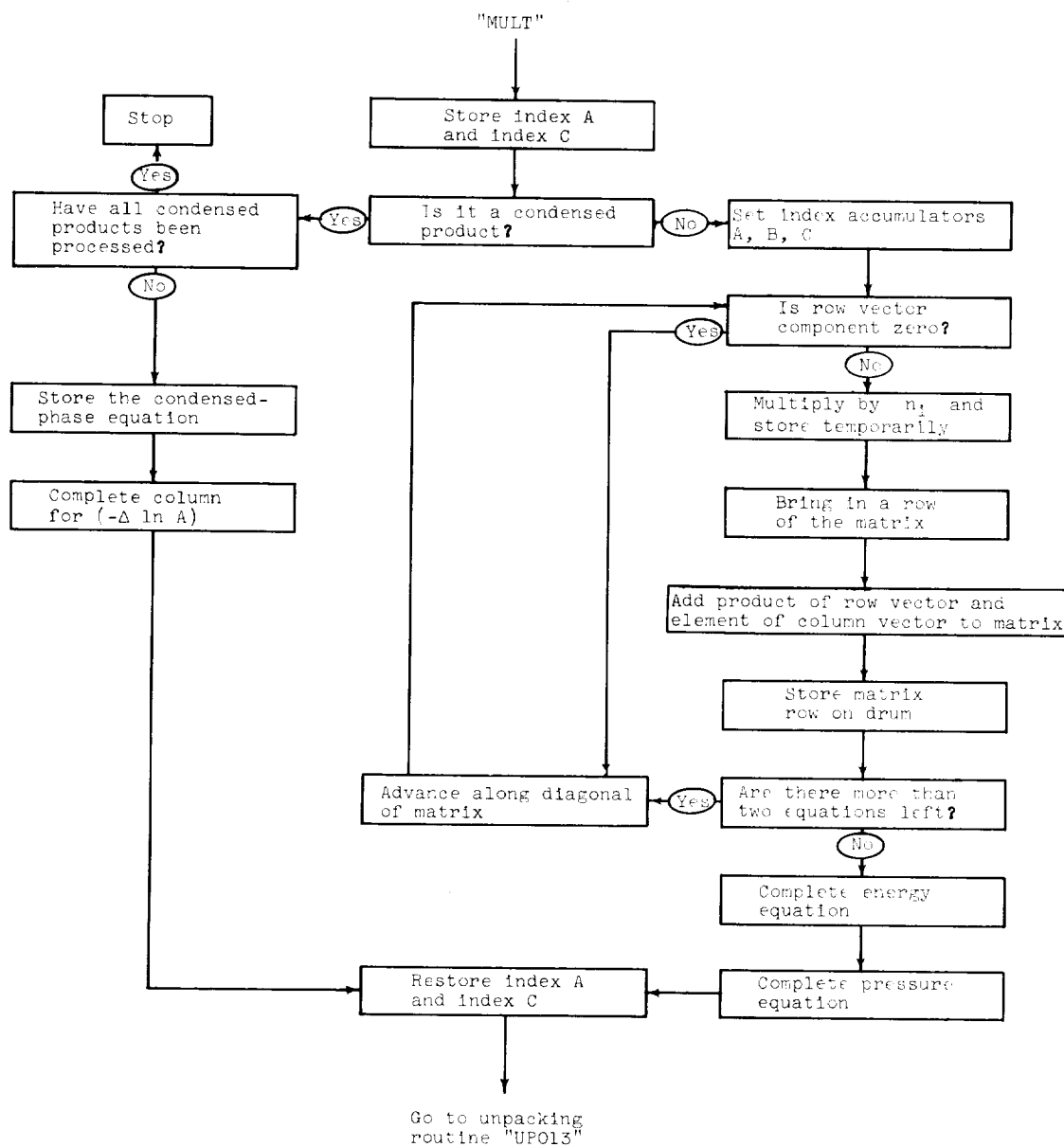


Figure 11. - Flow chart for vector multiplication routine.

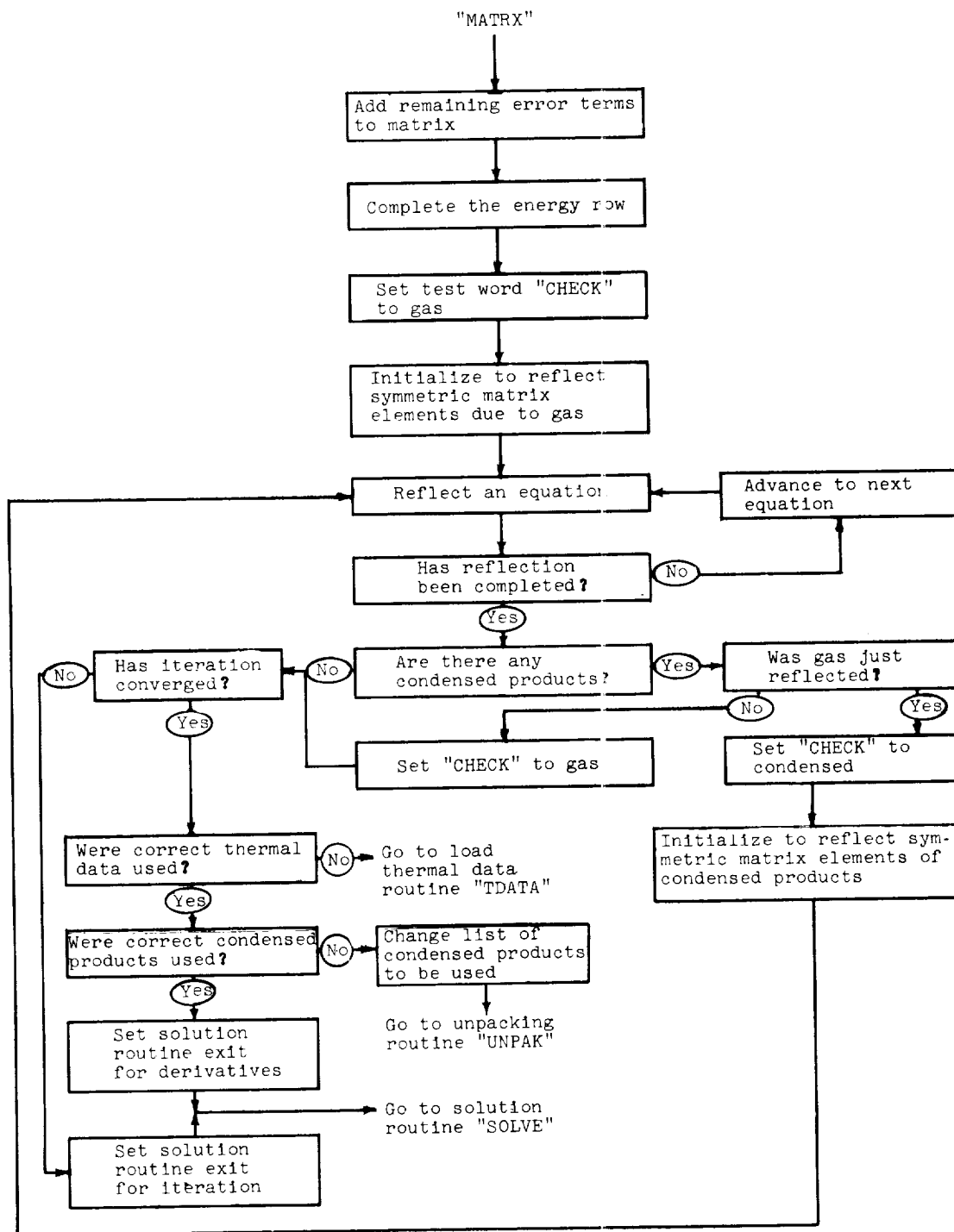


Figure 12. - Flow chart for matrix completion routine.

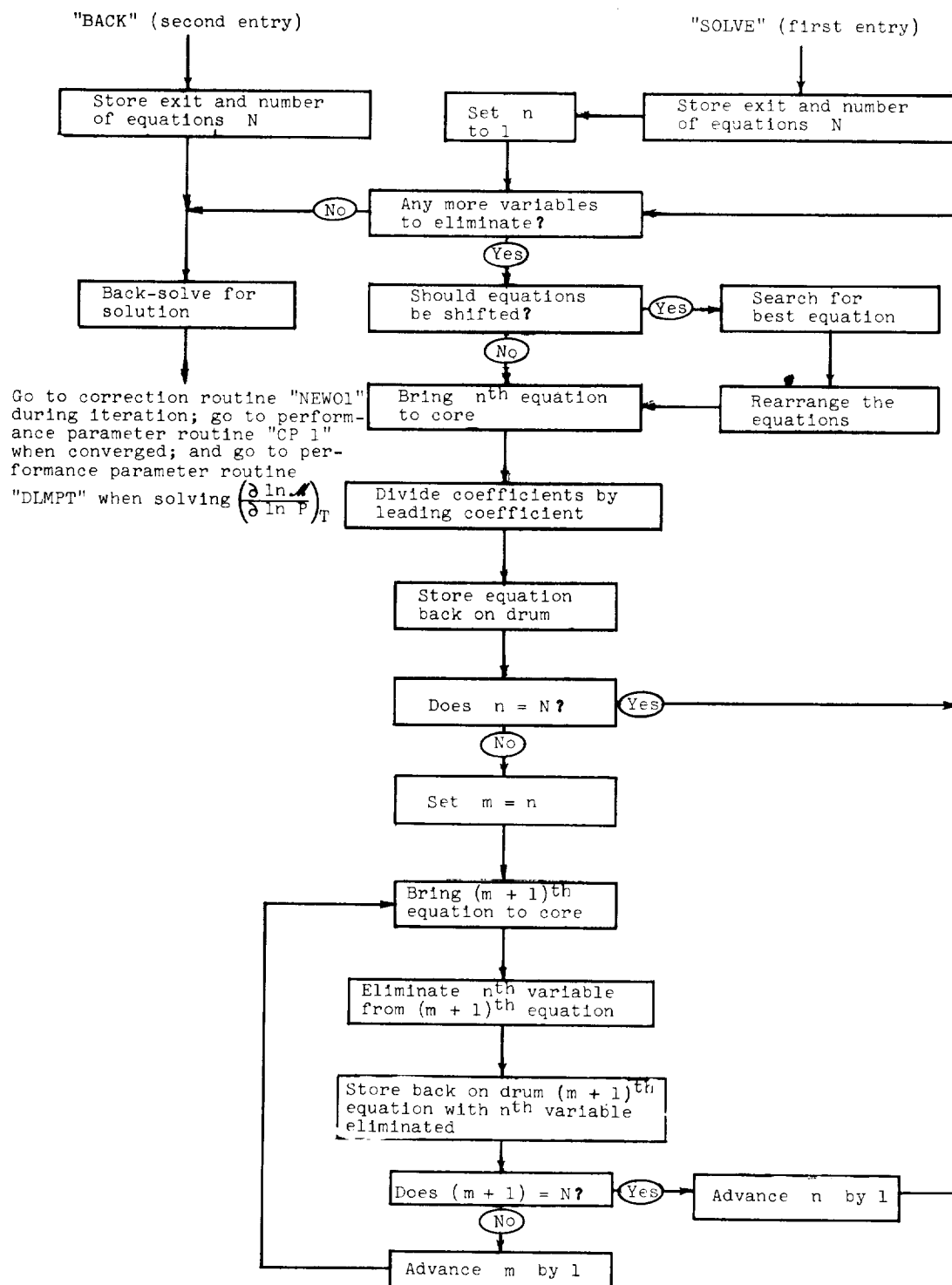


Figure 13. - Flow chart for matrix solution routine.

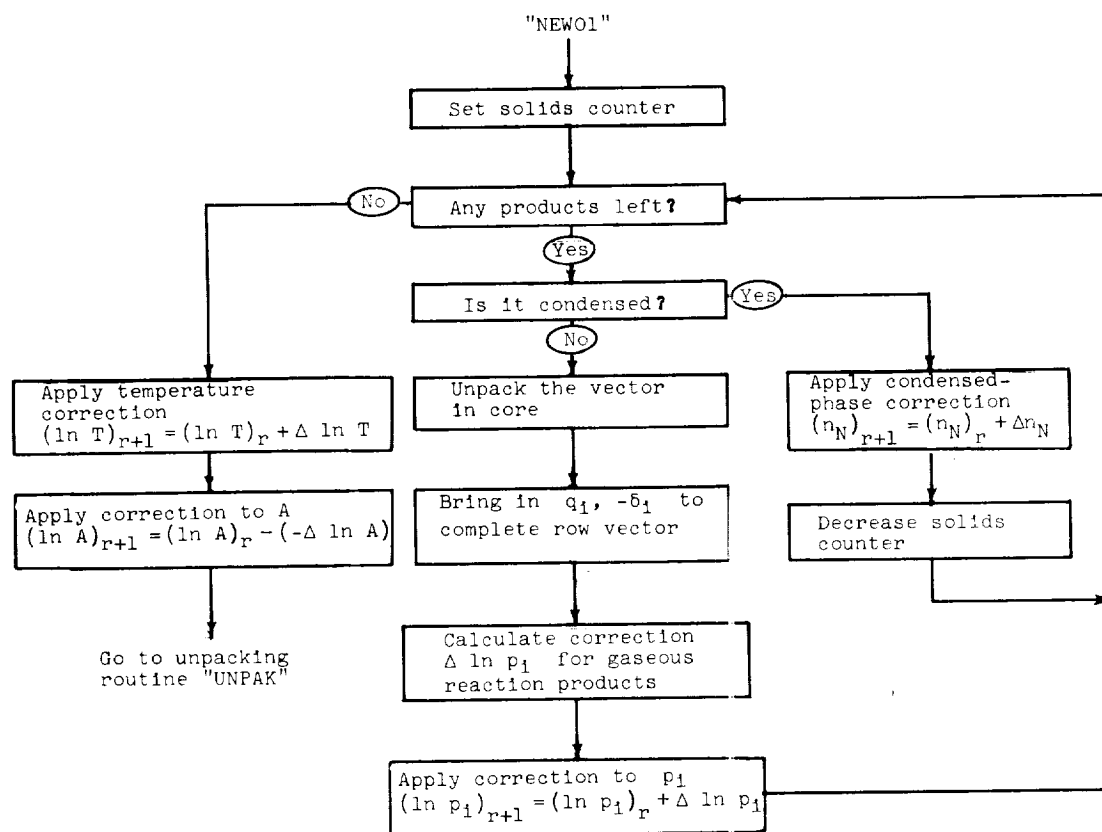
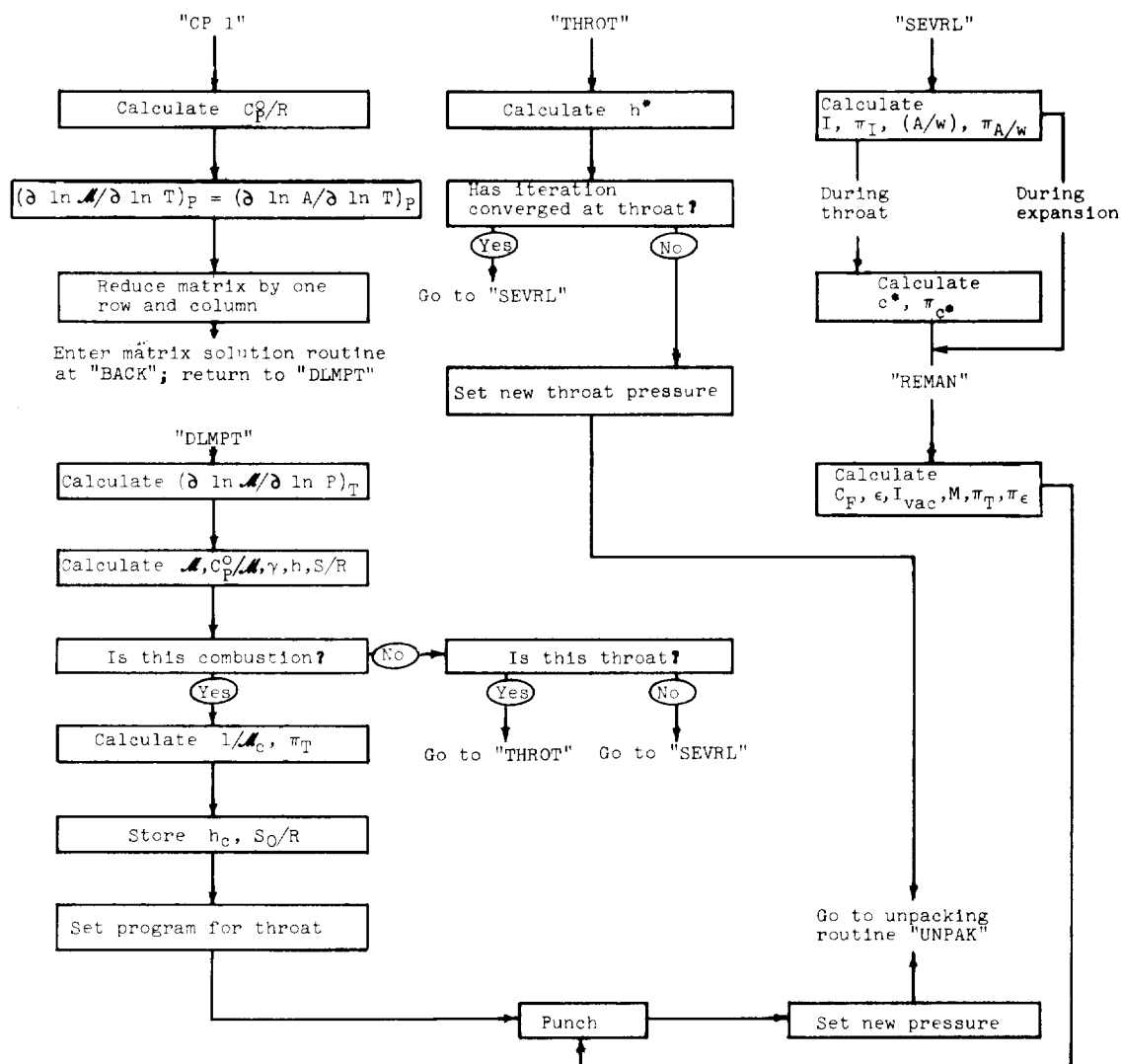


Figure 14. - Flow chart for correction routine.



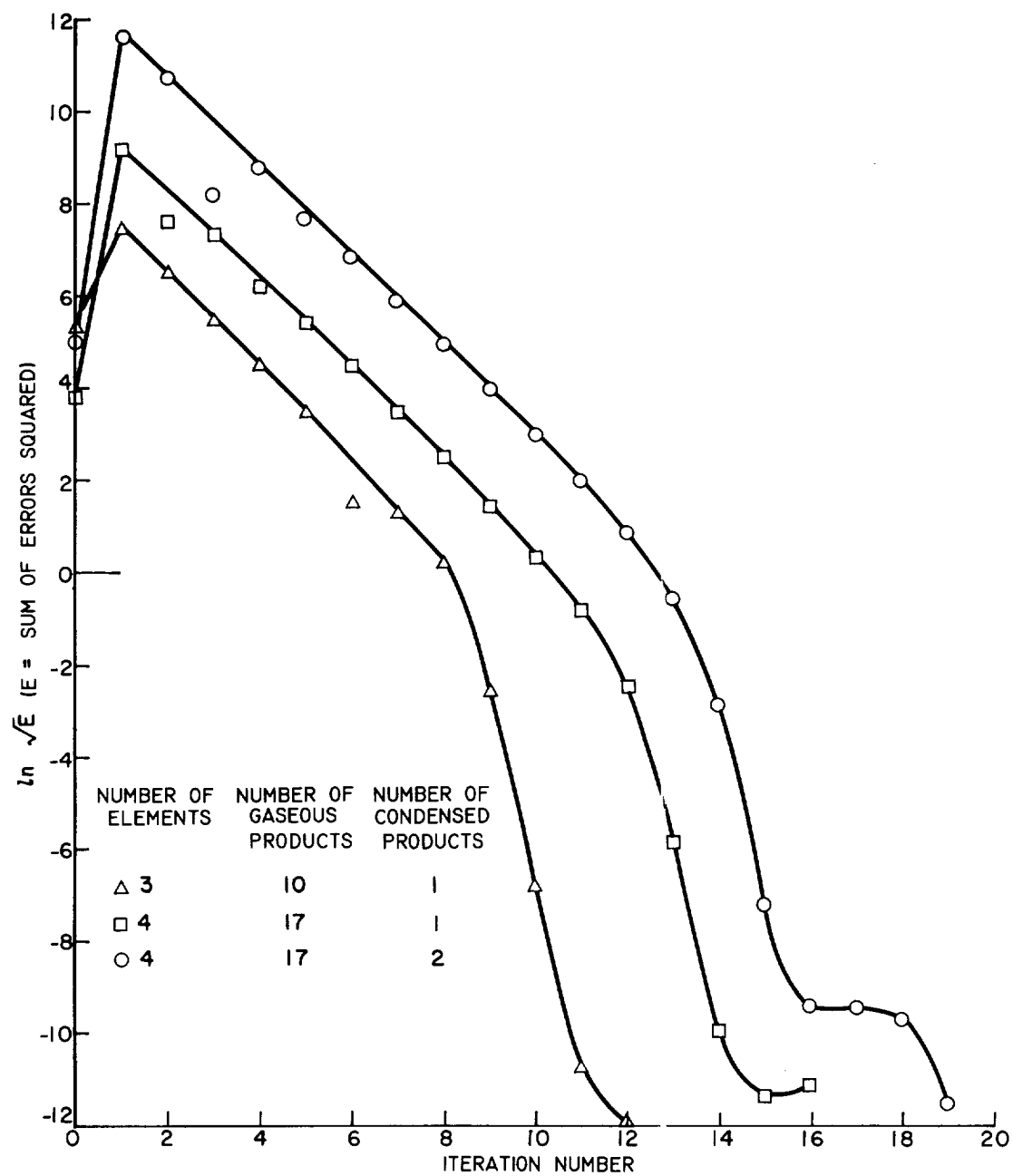


Figure 16. - Rate of convergence for several propellants.

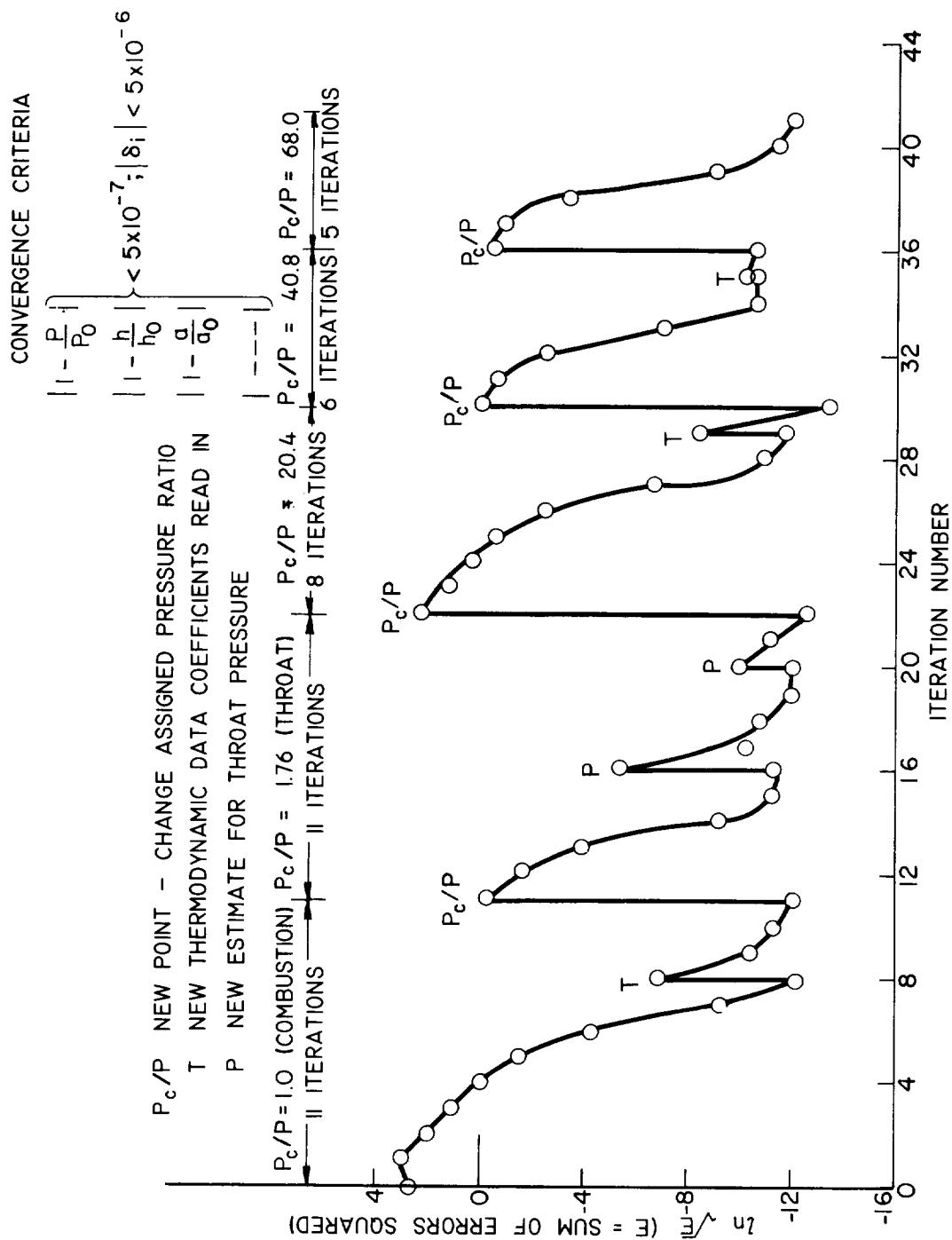


Figure 10 - Convergence for reaction $N_2H_4 + \frac{5}{2} H_2O$.

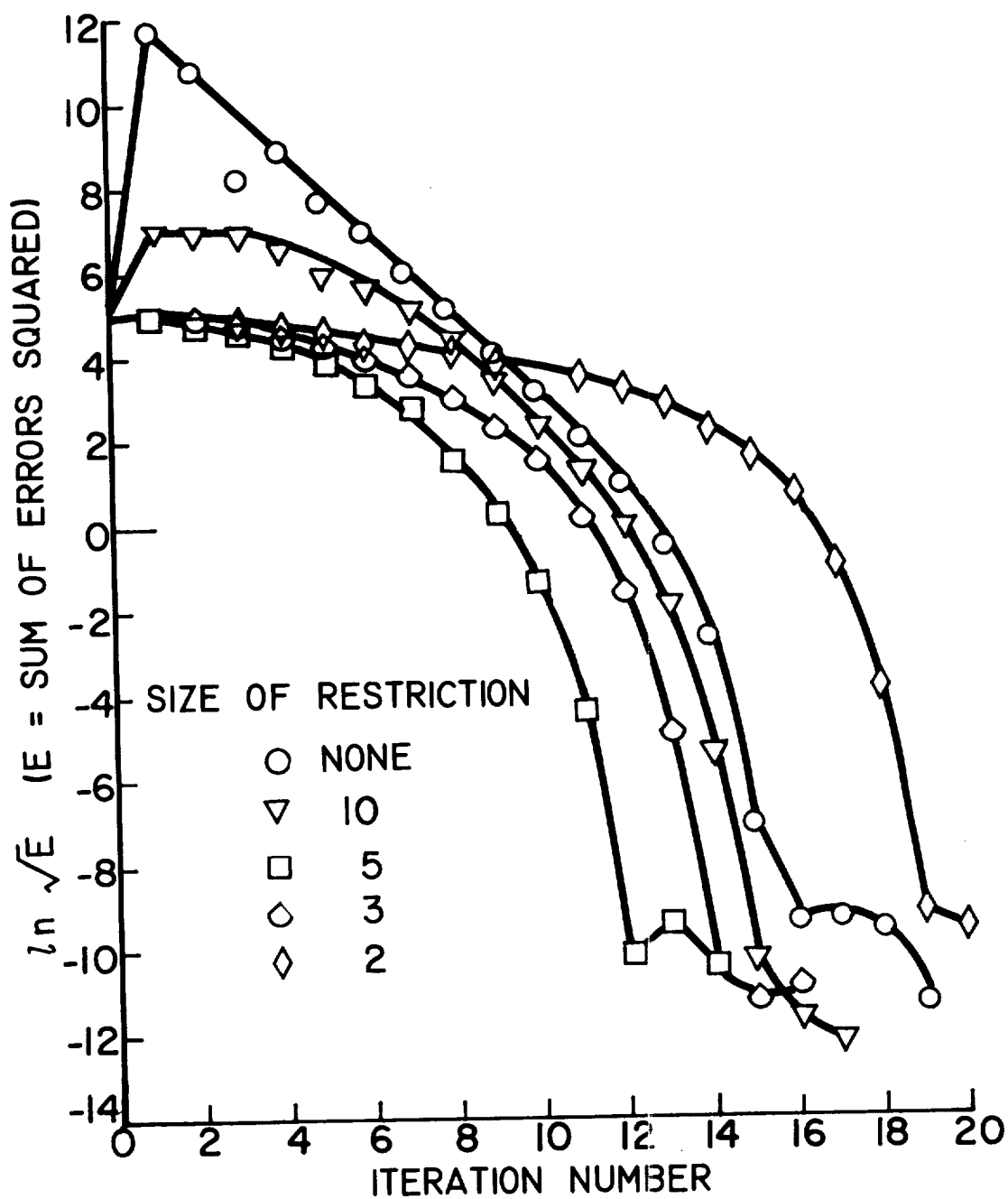


Figure 18. - Solution vector control and convergence;
4 elements, 17 gaseous products, 2 condensed products.

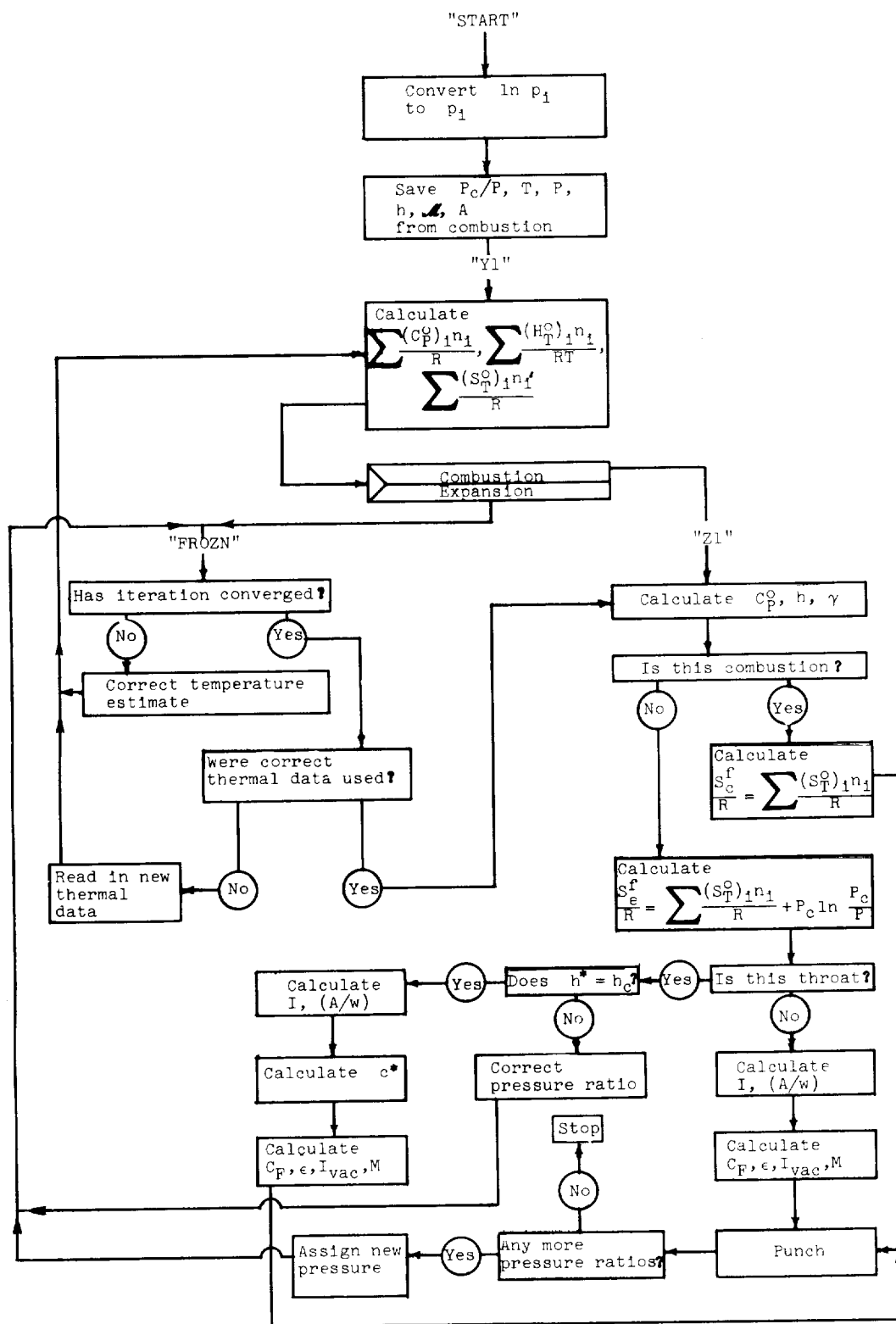


Figure 19. - Flow chart for frozen-composition routine.

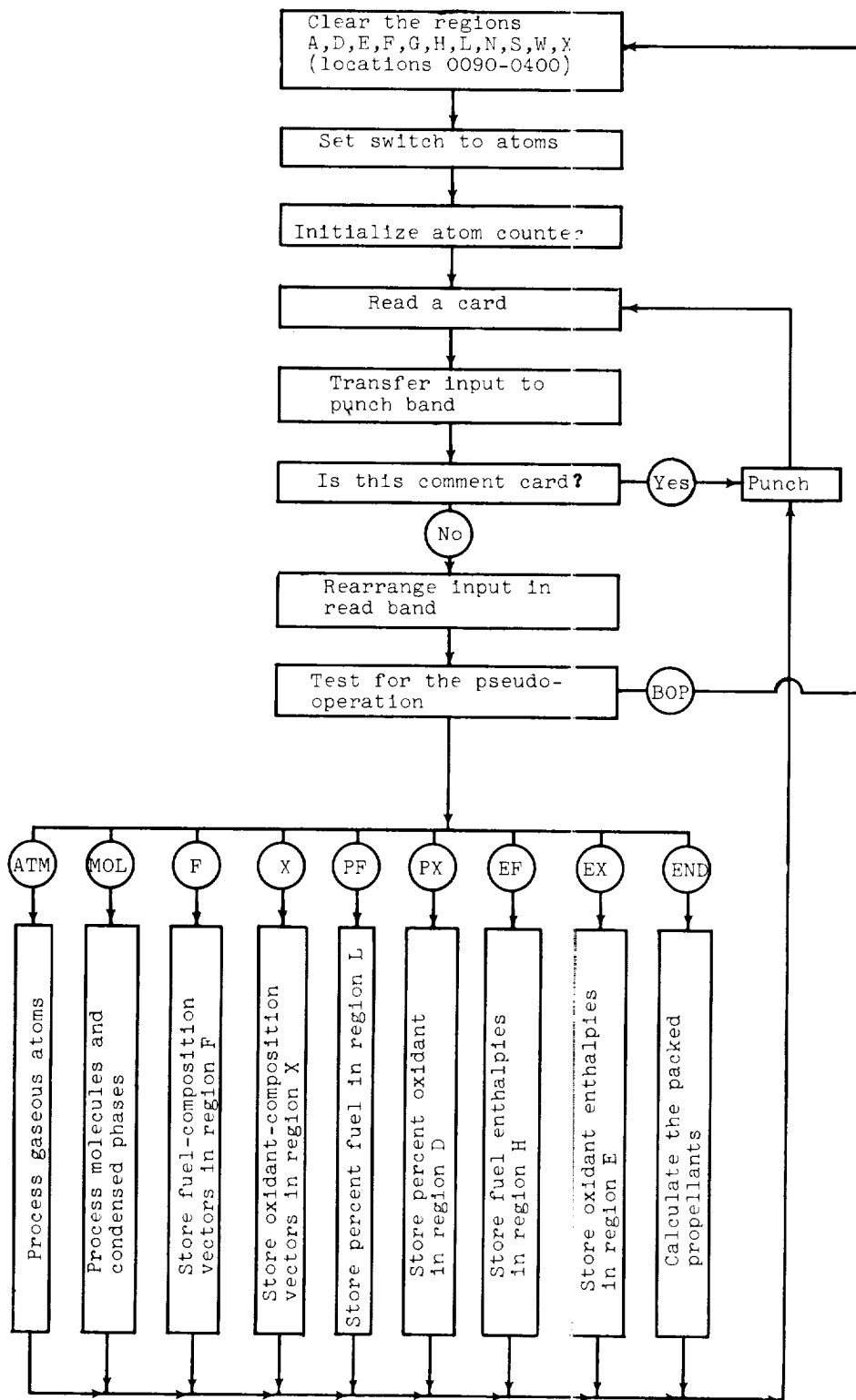


Figure 20. - Flow chart for Vector and Propellant Program.

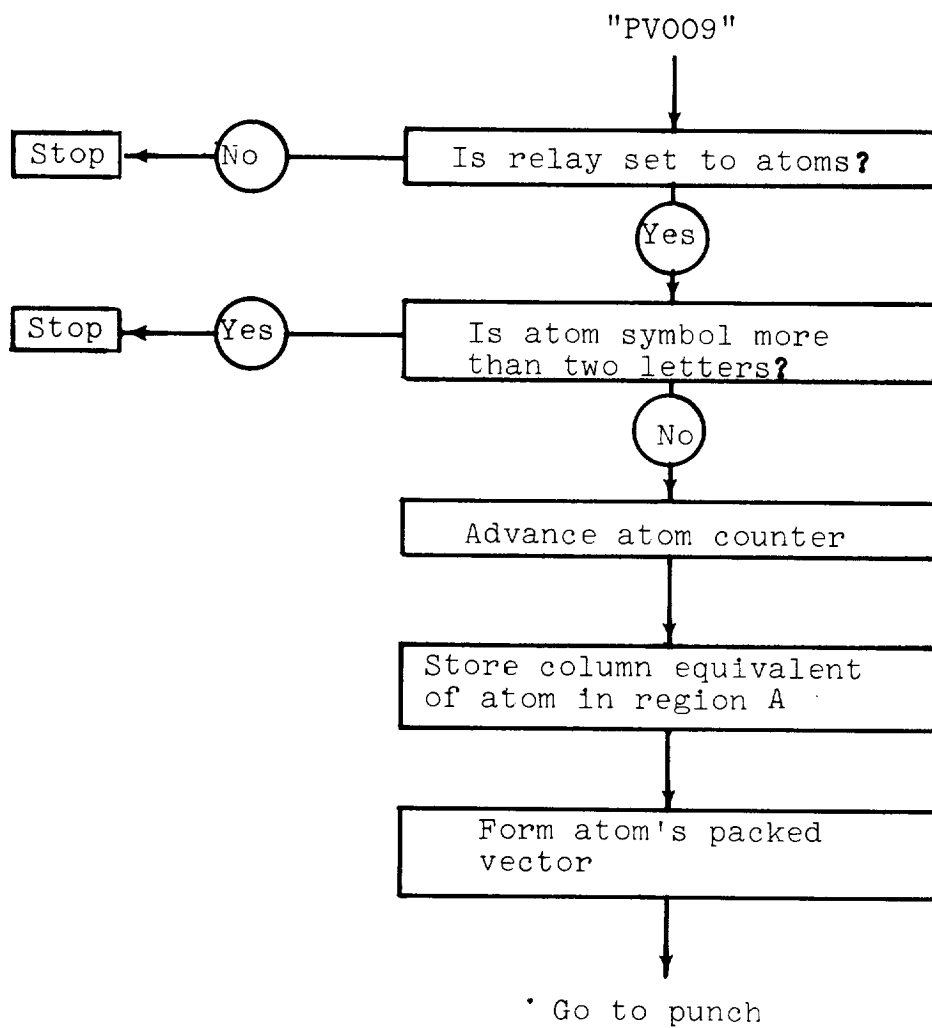


Figure 21. - Flow chart for ATM (pseudo-operation).

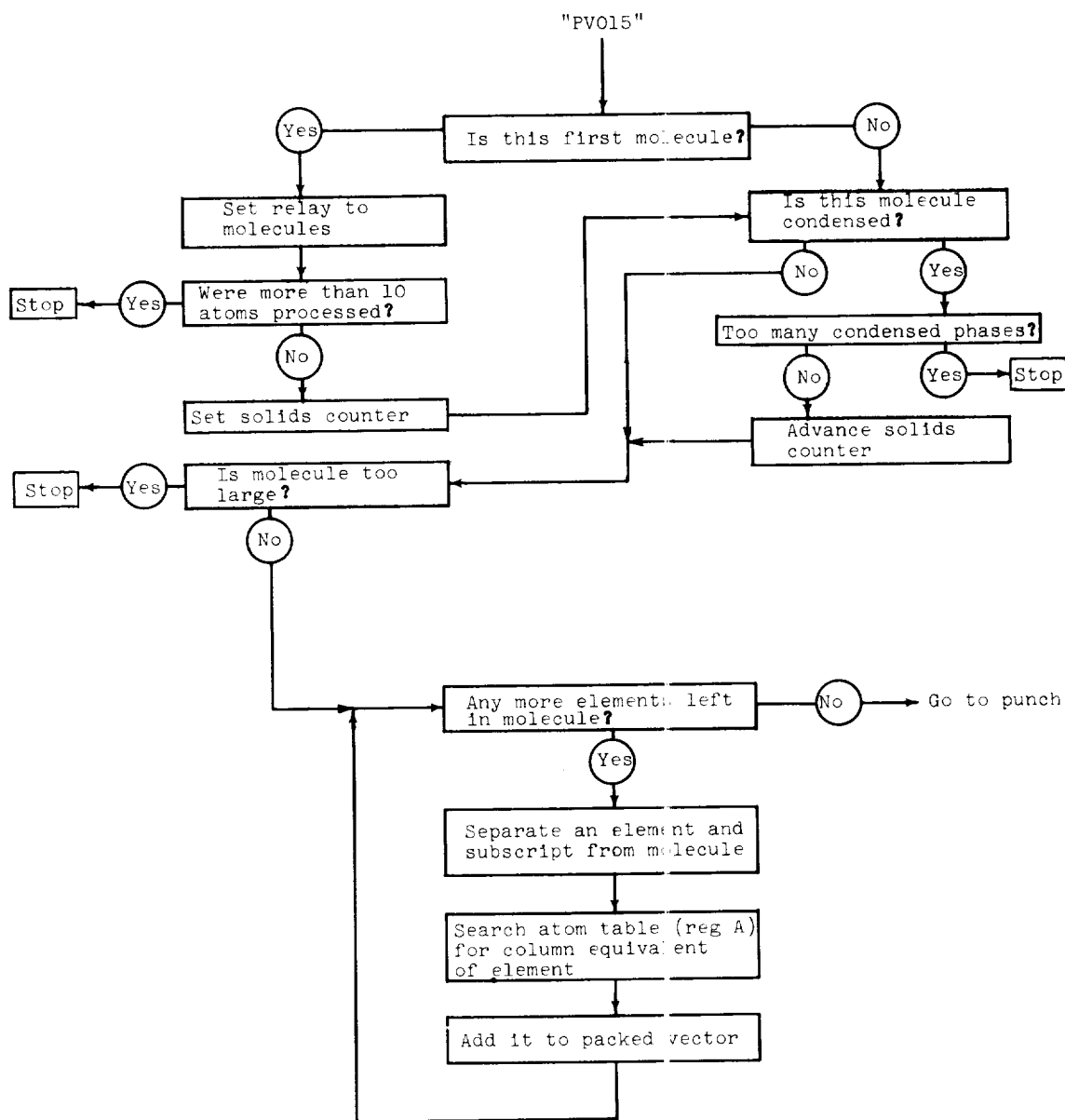
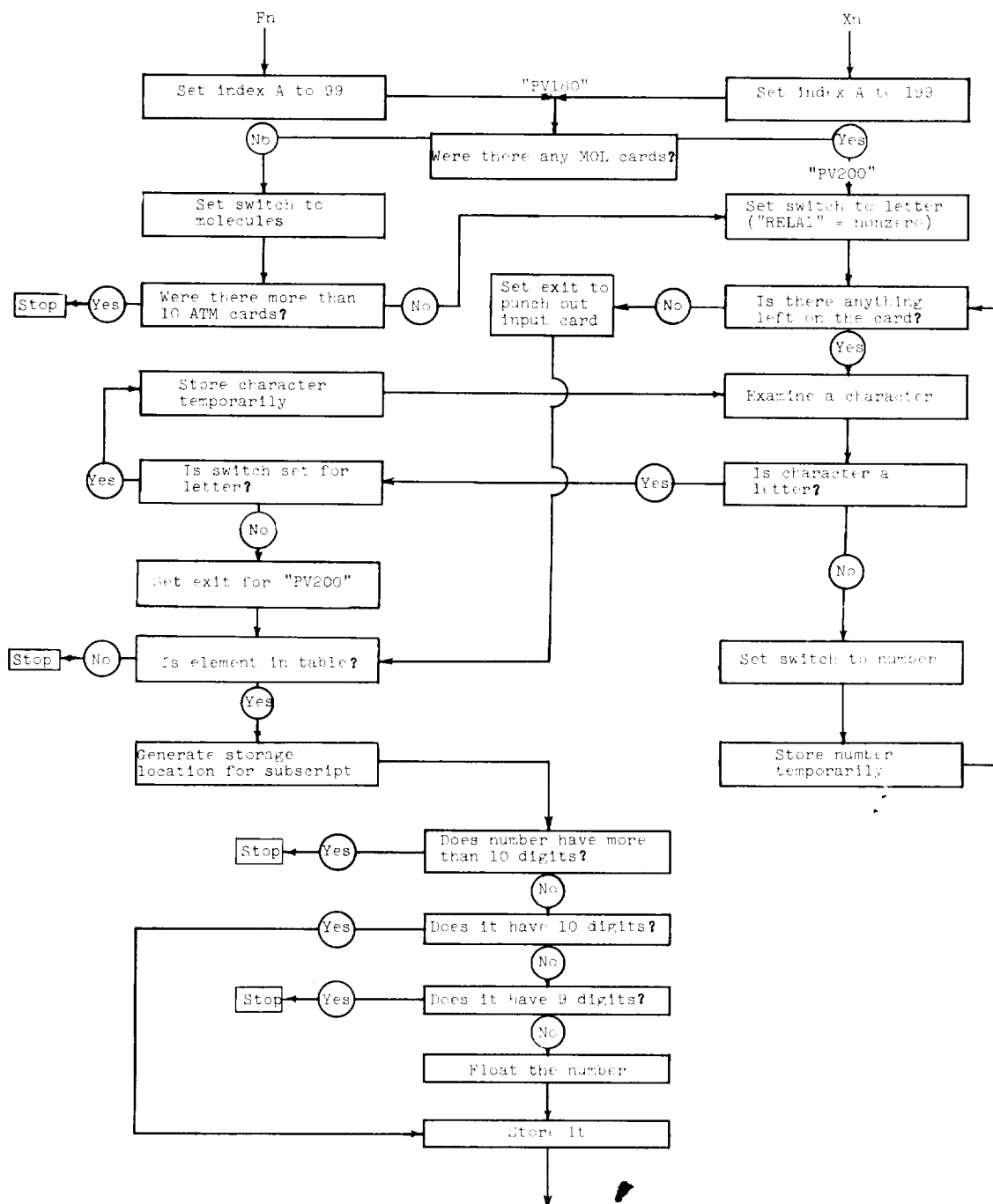


Figure 22. - Flow chart for MML (pseudo-operation).

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To to exit
 (1) "PV200" - continue processing fuel or oxidant
 (2) Punch out input card

Figure 23. - Flow chart for F and X (pseudo-operations).

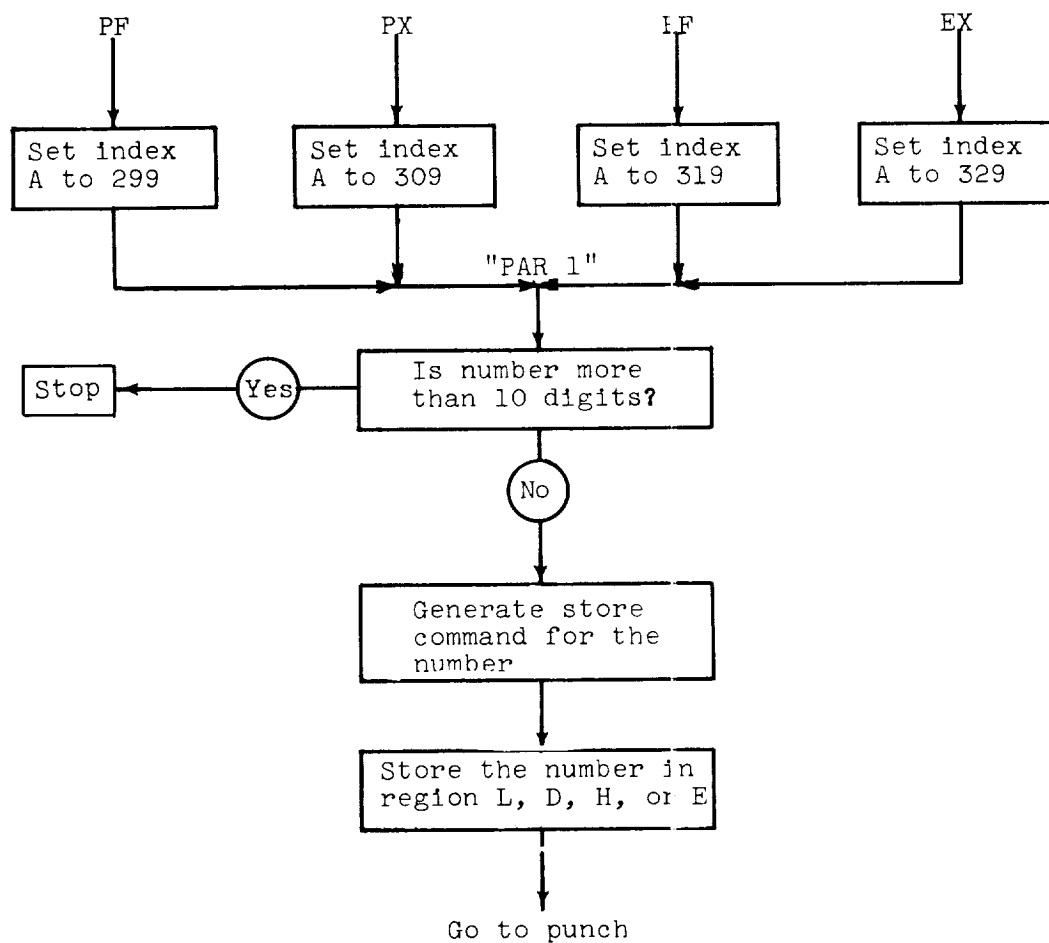


Figure 24. - Flow chart for percent fuel or oxidant and enthalpy of fuel or oxidant (pseudo-operations).

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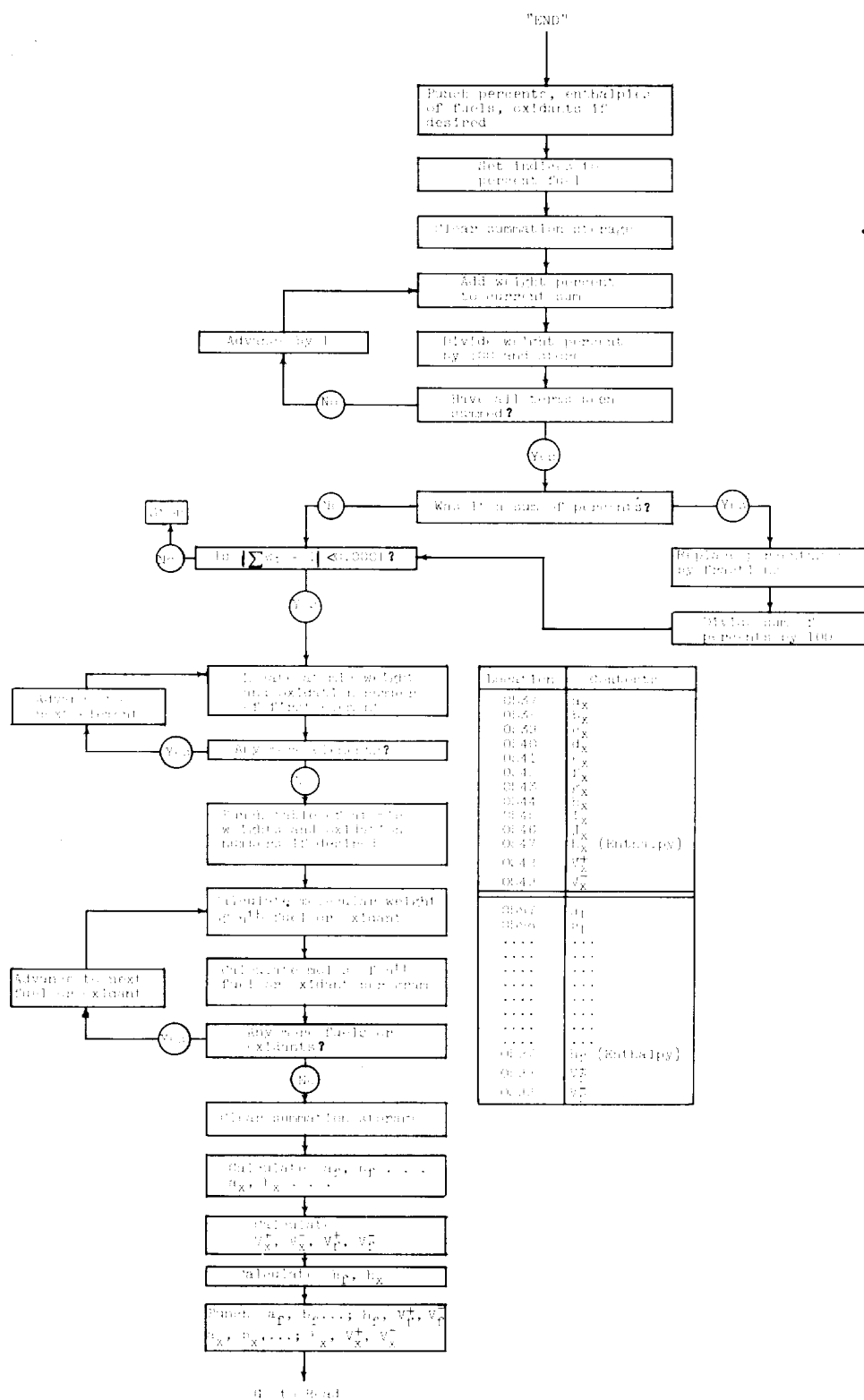


Figure 10. - Flow chart for propellant analysis.

<p>NASA TN D-132</p> <p>National Aeronautics and Space Administration.</p> <p>A GENERAL METHOD FOR AUTOMATIC COMPUTATION OF EQUILIBRIUM COMPOSITIONS AND THEORETICAL ROCKET PERFORMANCE OF PROPELLANTS. Sanford Gordon, Frank J. Zeleznik, and Vearl N. Huff. October 1959. 161p. diagrs., tabs. OTS price, \$3.00.</p> <p>(NASA TECHNICAL NOTE D-132)</p> <p>A general computer program for chemical equilibrium and rocket performance calculations was written for the IBM 650 computer with 2000 words of drum storage, 60 words of high-speed core storage, indexing registers, and floating point attachments. The program can carry out combustion and isentropic-expansion calculations on a chemical system that may include as many as 10 different chemical elements, 30 reaction products, and 25 pressure ratios. It calculates composition, temperature, pressure, specific impulse, specific impulse in vacuum, characteristic velocity, thrust coefficient, area ratio, molecular weight, Mach</p> <p>Copies obtainable from NASA, Washington (over)</p>	<ol style="list-style-type: none"> Engines, Rocket (3.1.8) Fuels - Rockets (Includes Fuel and Oxidant) (3.4.3.3) Combustion - Rocket Engines (3.5.2.5) <ol style="list-style-type: none"> Gordon, Sanford Zeleznik, Frank J. Huff, Vearl N. NASA TN D-132 <p>NASA</p>
<p>NASA TN D-132</p> <p>National Aeronautics and Space Administration.</p> <p>A GENERAL METHOD FOR AUTOMATIC COMPUTATION OF EQUILIBRIUM COMPOSITIONS AND THEORETICAL ROCKET PERFORMANCE OF PROPELLANTS. Sanford Gordon, Frank J. Zeleznik, and Vearl N. Huff. October 1959. 161p. diagrs., tabs. OTS price, \$3.00.</p> <p>(NASA TECHNICAL NOTE D-132)</p> <p>A general computer program for chemical equilibrium and rocket performance calculations was written for the IBM 650 computer with 2000 words of drum storage, 60 words of high-speed core storage, indexing registers, and floating point attachments. The program can carry out combustion and isentropic-expansion calculations on a chemical system that may include as many as 10 different chemical elements, 30 reaction products, and 25 pressure ratios. It calculates composition, temperature, pressure, specific impulse, specific impulse in vacuum, characteristic velocity, thrust coefficient, area ratio, molecular weight, Mach</p> <p>Copies obtainable from NASA, Washington (over)</p>	<ol style="list-style-type: none"> Engines, Rocket (3.1.8) Fuels - Rockets (Includes Fuel and Oxidant) (3.4.3.3) Combustion - Rocket Engines (3.5.2.5) <ol style="list-style-type: none"> Gordon, Sanford Zeleznik, Frank J. Huff, Vearl N. NASA TN D-132 <p>NASA</p>
<p>NASA TN D-132</p> <p>National Aeronautics and Space Administration.</p> <p>A GENERAL METHOD FOR AUTOMATIC COMPUTATION OF EQUILIBRIUM COMPOSITIONS AND THEORETICAL ROCKET PERFORMANCE OF PROPELLANTS. Sanford Gordon, Frank J. Zeleznik, and Vearl N. Huff. October 1959. 161p. diagrs., tabs. OTS price, \$3.00.</p> <p>(NASA TECHNICAL NOTE D-132)</p> <p>A general computer program for chemical equilibrium and rocket performance calculations was written for the IBM 650 computer with 2000 words of drum storage, 60 words of high-speed core storage, indexing registers, and floating point attachments. The program can carry out combustion and isentropic-expansion calculations on a chemical system that may include as many as 10 different chemical elements, 30 reaction products, and 25 pressure ratios. It calculates composition, temperature, pressure, specific impulse, specific impulse in vacuum, characteristic velocity, thrust coefficient, area ratio, molecular weight, Mach</p> <p>Copies obtainable from NASA, Washington (over)</p>	<ol style="list-style-type: none"> Engines, Rocket (3.1.8) Fuels - Rockets (Includes Fuel and Oxidant) (3.4.3.3) Combustion - Rocket Engines (3.5.2.5) <ol style="list-style-type: none"> Gordon, Sanford Zeleznik, Frank J. Huff, Vearl N. NASA TN D-132 <p>NASA</p>
<p>NASA TN D-132</p> <p>National Aeronautics and Space Administration.</p> <p>A GENERAL METHOD FOR AUTOMATIC COMPUTATION OF EQUILIBRIUM COMPOSITIONS AND THEORETICAL ROCKET PERFORMANCE OF PROPELLANTS. Sanford Gordon, Frank J. Zeleznik, and Vearl N. Huff. October 1959. 161p. diagrs., tabs. OTS price, \$3.00.</p> <p>(NASA TECHNICAL NOTE D-132)</p> <p>A general computer program for chemical equilibrium and rocket performance calculations was written for the IBM 650 computer with 2000 words of drum storage, 60 words of high-speed core storage, indexing registers, and floating point attachments. The program can carry out combustion and isentropic-expansion calculations on a chemical system that may include as many as 10 different chemical elements, 30 reaction products, and 25 pressure ratios. It calculates composition, temperature, pressure, specific impulse, specific impulse in vacuum, characteristic velocity, thrust coefficient, area ratio, molecular weight, Mach</p> <p>Copies obtainable from NASA, Washington (over)</p>	<ol style="list-style-type: none"> Engines, Rocket (3.1.8) Fuels - Rockets (Includes Fuel and Oxidant) (3.4.3.3) Combustion - Rocket Engines (3.5.2.5) <ol style="list-style-type: none"> Gordon, Sanford Zeleznik, Frank J. Huff, Vearl N. NASA TN D-132 <p>NASA</p>

NASA TN D-132

number, specific heat, isentropic exponent, enthalpy, entropy, and several thermodynamic first derivatives.

NASA TN D-132

number, specific heat, isentropic exponent, enthalpy, entropy, and several thermodynamic first derivatives.

Copies obtainable from NASA, Washington

NASA TN D-132

number, specific heat, isentropic exponent, enthalpy, entropy, and several thermodynamic first derivatives.

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